

RESIDENTIAL DEVELOPMENT

12433 DILLON DRIVE

TECUMSEH, ON

TRAFFIC IMPACT STUDY

Prepared by:



RC SPENCER ASSOCIATES INC.
Consulting Engineers

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RESIDENTIAL DEVELOPMENT, 12433 DILLON DRIVE, TECUMSEH, ON

TRAFFIC IMPACT STUDY (MARCH 2021)

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INTRODUCTION AND BACKGROUND

A residential development has been proposed for lands situated at 12433 Dillon Drive in the Town of Tecumseh, Ontario. As may be noted on Figure 1 – Area Plan, the proposed development site is located on the south side of Dillon Drive, between Lacasse Boulevard to the east and Lesperance Road to the west. The area around the study intersections is fully built out, so it is unlikely that there would be significant land use changes in the near future. There is no public transportation available in the immediate area.

The following intersections were analyzed as part of this traffic impact study:

- Dillon Drive at Lesperance Road;
- Dillon Drive at St. Pierre Street;
- Dillon Drive at the proposed site access; and
- Dillon Drive at Lacasse Boulevard.

Lesperance Road is a north / south roadway with a three-lane cross-section (one lane in each direction and a two-way left-turn lane); it is part of the arterial grid system in Tecumseh and a principal means of external access to the area. Dillon Drive is an east / west collector road, and Lacasse Boulevard is a north / south collector road. St. Pierre Street, just west of the site, is a local north / south road. There are sidewalks on both sides of each section of the subject roadways, except for along the south side of Dillon Drive, west of St. Pierre Street. The intersection of Dillon Drive at Lesperance Road is controlled by a two-way stop sign on the minor street, Dillon Drive. The intersection of Dillon Drive at Lacasse Boulevard is all-way stop-controlled, as is Dillon Drive at St. Pierre Street.

For AM and PM peak hours, detailed analysis was carried out for all of the above-noted intersections with respect to the following scenarios:

- Existing Traffic;
- Existing + Site Generated Traffic;
- 2025 Background Traffic;
- 2025 Background Traffic + Site Generated Traffic (Total Traffic 2025);
- 2030 Background Traffic; and
- 2030 Background Traffic + Site Generated Traffic (Total Traffic 2030).

The proposed site plan (Figure 2 – Site Plan) includes low-rise multifamily housing units consisting of 63 units in eight buildings. Two of the buildings are stacked townhouses consisting of twenty-four and sixteen units with a total of sixty-eight parking spaces proposed to be developed to service these two buildings. The remaining 23 units are part of three-section and four-section row houses, each unit will have its own driveway. The developer is proposing only one driveway access at Dillon Drive, which is located to the north of the subject lands.



The purpose of this study is to examine the traffic implications of the proposed development on traffic operations in the area, particularly on the above-noted intersections along Dillon Drive. The study will also identify potential traffic operations impact on area intersections experiencing a direct impact as a result of this proposed development.

TRAFFIC DATA COLLECTION

Turning movement counts were obtained by RC Spencer Associates Inc. on 25 April 2019 for the intersection of Dillon Drive at Lesperance Road, on 30 April 2019 for the Dillon Drive at Lacasse Boulevard intersection, and on 2 May 2019 for the Dillon Drive at St. Pierre Street intersection. All turning movement counts are provided in Appendix A.

METHODOLOGY

The aforementioned turning movement counts provided the basis for industry-standard traffic operations analysis; the software package utilized for the analysis (Synchro 10) calculates various parameters of intersection performance, such as level of service (LOS), intersection capacity utilization (ICU), control delay, and queue lengths on individual approaches. HCM 6th Edition methodology was used to generate the performance metrics.

Signalized level of service results are reported based on the following industry standard:

| Level of Service | Average Control Delay (sec/veh) | General Description (Signalized Intersections) |
|------------------|---------------------------------|---|
| A | ≤10 | Free Flow |
| B | >10 - 20 | Stable Flow (slight delays) |
| C | >20 - 35 | Stable flow (acceptable delays) |
| D | >35 - 55 | Approaching unstable flow (tolerable delay, occasionally wait through more than one signal cycle before proceeding) |
| E | >55 - 80 | Unstable flow (intolerable delay) |
| F | >80 | Forced flow (jammed) |

Unsignalized level of service results are reported based on the following industry standard:

| Level of Service | Average Control Delay (sec/veh) |
|------------------|---------------------------------|
| A | 0 - 10 |
| B | >10 - 15 |
| C | >15 - 25 |
| D | >25 - 35 |
| E | >35 - 50 |
| F | >50 |

TRIP GENERATION AND DISTRIBUTION

Trip generation for the proposed development was estimated from the Institute of Transportation Engineers Trip Generation Manual (10th Edition). ITE Land Use Code 220 (Low-Rise Multifamily Housing) is the most appropriate code for this use. Land Use Code 220 provides average generation rates of 0.46 trips per unit in the AM peak hour, with 23% entering and 77% exiting, and 0.56 trips per unit in the PM peak hour, with 63% entering and 37% exiting.

The details of the trip generation analysis are contained in Appendix B, noting that separate estimates were developed for AM and PM peak hours. When combined, the total trips generated by the proposed development are estimated to be 7 entering and 22 exiting during the AM peak hour, and 22 entering and 13 exiting during the PM peak hour. Average rates were used instead of regression equations because the results are always identical in this application.

To be conservative, the analysis was carried out assuming full build-out in 2020 and projected horizon years of 2025 and 2030. Background traffic was increased by 2% per year for the 2025 and 2030 horizon forecasts, which provides for very conservative increases to background traffic.

Site generated traffic was distributed to the proposed site access in accordance with the existing origin-destination matrices contained within the obtained turning movement counts. When the estimated trip distribution percentages were applied to the trip generation results from Appendix B, the turning movements which resulted at the surrounding intersections are illustrated on Figure 3. Figure 4 illustrates the existing traffic volumes, and Figures 5 to 9 summarize total traffic estimates that result from the summation of site generated traffic and the existing, projected 2025, and projected 2030 background traffic volumes.

CAPACITY AND LEVEL OF SERVICE ANALYSIS

Detailed Synchro 10 analysis was carried out for all intersections with respect to the following scenarios:

- Existing Traffic;
- Existing + Site Generated Traffic;
- 2025 Background Traffic;
- 2025 Background Traffic + Site Generated Traffic (Total Traffic 2025);
- 2030 Background Traffic; and
- 2030 Background Traffic + Site Generated Traffic (Total Traffic 2030).

The effect of adding site generated traffic to existing and future volumes at each specific intersection can be found in Appendix C. The data from Figures 4 to 9 was used in the Synchro analysis of intersection performance. The proposed site access was modelled based on a single lane for ingress and a single lane for egress.

The heavy vehicles percentages used for each intersection were determined from the values observed for the entire count duration, as taken from the turning movement counts. They are as follows:

| Intersection | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Dillon / Lesperance | 0 | 0 | 6 | 9 | 0 | 2 | 0 | 2 | 2 | 0 | 4 | 0 |
| Dillon / St. Pierre | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 22 | 40 | 0 | 4 | 0 |
| Dillon / Lacasse | 60 | 0 | 0 | 25 | 5 | 0 | 8 | 1 | 29 | 0 | 0 | 0 |

At the Dillon Drive site access, the default 2% was used for through heavy vehicle traffic, as this is a standard conservative value built into the Synchro 10 analysis software. This development is not expected to generate significant heavy vehicle traffic; therefore, all turning movements into and out of the site are assumed to be 0% heavy vehicles.

The peak hour factors for the overall intersection levels used in the Synchro analysis were obtained from the turning movement counts, except for the Dillon Drive site access, where the default 0.92 peak hour factor was used. The inputted peak hour factors are as follows:

| Intersection | AM PHF | PM PHF |
|---------------------|--------|--------|
| Dillon / Lesperance | 0.92 | 0.83 |
| Dillon / St. Pierre | 0.73 | 0.74 |
| Dillon / Lacasse | 0.65 | 0.91 |

Peak hour pedestrian volumes were very low, so the impact of pedestrians on intersection operations is expected to be nominal; regardless, conservative pedestrian volumes were inputted into the Synchro 10 analysis software.

By applying the above parameters, detailed Synchro reports were generated for evaluation and comparison; they are provided in Appendix D. To quantify and qualify the effect of traffic growth on individual intersections within the study area, and to assess the need for geometric or traffic infrastructure improvements, the detailed Synchro results were summarized as follows:

Dillon Drive at Lesperance Road

The intersection of Dillon Drive at Lesperance Road is an eastbound / westbound stop-controlled intersection. Currently, there are dedicated left turn lanes and shared through / right turn lanes on the northbound and southbound approaches. Dillon Drive is comprised of a two-lane cross-section, and it is slightly skewed at its intersection with Lesperance Road; this geometry forces through traffic to veer slightly to the right to proceed through the intersection. There are sidewalks on the east / west sides of Lesperance Road and on the north side of Dillon Drive.

From the level of service results provided in Table 1, it is observed that the intersection of Dillon Drive at Lesperance Road will be nominally affected by distribution of the site generated traffic; the change in level of service will be effectively imperceptible. It is the engineers' expectation that the intersection will continue to operate favourably in all horizon traffic scenarios.

Table 1: Level of Service by Approach – Dillon Drive at Lesperance Road

| Scenario | Dillon Drive at Lesperance Road | | | | | | | |
|---------------------------|---------------------------------|-----|-----|-----|--------------|-----|-----|-----|
| | AM Peak Hour | | | | PM Peak Hour | | | |
| | E/B | W/B | N/B | S/B | E/B | W/B | N/B | S/B |
| Existing Traffic | A | B | A | A | B | B | A | A |
| Existing + Site Generated | A | B | A | A | B | B | A | A |
| Background Traffic 2025 | A | B | A | A | B | B | A | A |
| Total Traffic 2025 | A | B | A | A | B | B | A | A |
| Background Traffic 2030 | A | B | A | A | B | B | A | A |
| Total Traffic 2030 | A | B | A | A | B | B | A | A |

Dillon Drive at St. Pierre Street

The intersection of Dillon Drive at St. Pierre Street is a four-way stop-controlled intersection. Both streets are comprised of two-lane cross-sections. There are sidewalks on the east and west sides of St. Pierre Street and on the north side of Dillon Drive. From the results provided in Table 2, it is observed that the intersection of Dillon Drive at St. Pierre Street will be nominally affected by distribution of the site generated traffic; the change in level of service will be effectively imperceptible. It is the engineers' expectation that the intersection will continue to operate favourably in all horizon traffic scenarios.

Table 2: Level of Service by Approach – Dillon Drive at St. Pierre Street

| Scenario | Dillon Drive at St. Pierre Street | | | | | | | |
|---------------------------|-----------------------------------|-----|-----|-----|--------------|-----|-----|-----|
| | AM Peak Hour | | | | PM Peak Hour | | | |
| | E/B | W/B | N/B | S/B | E/B | W/B | N/B | S/B |
| Existing Traffic | A | A | A | A | A | A | A | A |
| Existing + Site Generated | A | A | A | A | A | A | A | A |
| Background Traffic 2025 | A | A | A | A | A | A | A | A |
| Total Traffic 2025 | A | A | A | A | A | A | A | A |
| Background Traffic 2030 | A | A | A | A | A | A | A | A |
| Total Traffic 2030 | A | A | A | A | A | A | A | A |

Dillon Drive at Site Access

The intersection of Dillon Drive at the Site Access is proposed to be a tee intersection, controlled by a stop sign on the northbound approach. The proposed geometry for the northbound approach is a single ingress lane and a single egress lane. From the results provided in Table 3, it is observed that the intersection of Dillon Drive at St. Pierre Street will be nominally affected by distribution of the site generated traffic; the change in level of service will be effectively imperceptible. It is the engineers' expectation that the intersection will continue to operate favourably in all horizon traffic scenarios.

Table 3: Level of Service by Approach – Dillon Drive at Site Access

| Scenario | Dillon Drive at Site Access | | | | | | | |
|---------------------------|-----------------------------|-----|-----|-----|--------------|-----|-----|-----|
| | AM Peak Hour | | | | PM Peak Hour | | | |
| | E/B | W/B | N/B | S/B | E/B | W/B | N/B | S/B |
| Existing + Site Generated | A | A | A | - | A | A | A | - |
| Total Traffic 2025 | A | A | A | - | A | A | A | - |
| Total Traffic 2030 | A | A | A | - | A | A | A | - |

Dillon Drive at Lacasse Boulevard

The intersection of Dillon Drive at Lacasse Boulevard is a four-way stop-controlled intersection. Dillon Drive is comprised of a two-lane cross-section. Lacasse Boulevard is a divided roadway to the north and south; it is comprised of a single lane in either direction. There are sidewalks on both sides of both roads. From the results provided in Table 4, it is observed that the intersection of Dillon Drive at Lacasse Boulevard will be nominally affected by the distribution of site generated traffic; the change in level of service will be effectively imperceptible. It is the engineers' expectation that the intersection will continue to operate favourably in all horizon traffic scenarios.

Table 4: Level of Service by Approach – Dillon Drive at Lacasse Boulevard

| Scenario | Dillon Drive at Lacasse Boulevard | | | | | | | |
|---------------------------|-----------------------------------|-----|-----|-----|--------------|-----|-----|-----|
| | AM Peak Hour | | | | PM Peak Hour | | | |
| | E/B | W/B | N/B | S/B | E/B | W/B | N/B | S/B |
| Existing Traffic | A | A | A | A | A | A | A | A |
| Existing + Site Generated | A | A | A | A | A | A | A | A |
| Background Traffic 2025 | A | A | A | A | A | A | A | A |
| Total Traffic 2025 | A | A | A | A | A | A | A | A |
| Background Traffic 2030 | A | A | A | A | A | A | A | A |
| Total Traffic 2030 | A | A | A | A | A | A | A | A |

SIGNAL WARRANT ANALYSIS

From the above results, there is no reason to suggest that traffic signals are warranted at any of the non-signalized intersections. However, for the sake of discussion, a signal warrant analysis was completed for the intersection of Dillon Drive at Lesperance Road.

The detailed results of the signal warrant analysis are presented in Appendix E. As expected, the intersection does not meet the provincial warrants for signalization; geometric and / or traffic control improvements are not required.

SIGHT LINE ANALYSIS

A sight line analysis was completed at the Dillon Drive access to the proposed development. The analysis was completed per the TAC Geometric Design Guide for Canadian Roads (2017). On Dillon Drive, the posted speed limit is 40 km/h, so the analysis was completed for a 50 km/h design speed. As calculated in Appendix F, the minimum intersection sight distance is determined to be 104m for the worst-case left turn egress maneuver and 90m for the right turn egress maneuver.

Based on the illustrated sight lines provided on Figure 10, it is the engineers' opinion that there is sufficient sight distance in both directions for safe egress from the proposed site access. It is the engineers' recommendation that the access be allowed but reviewed at the time of construction to ensure that sight lines are clear of potential obstructions.

SUMMARY AND CONCLUSIONS

A residential development has been proposed for lands situated at 12433 Dillon Drive in the Town of Tecumseh. The proposed site is located on the south side of Dillon Drive between Lacasse Boulevard to the east and Lesperance Road to the west. Lesperance Road is a north / south roadway with a three-lane cross-section (one lane in each direction and a two-way left-turn lane) that is part of the arterial grid system in Tecumseh and a principal means of external access to the area. Dillon Drive is an east / west collector road and Lacasse Boulevard is a north / south collector road. St. Pierre Street, just west of the site, is a local north / south road. The intersection of Dillon Drive at Lesperance Road is controlled by a two-way stop on the minor street, Dillon Drive. The intersection of Dillon Drive at Lacasse Boulevard is all-way stop-controlled, as is Dillon Drive at St. Pierre Street.

The proposed site plan consists of 63 low-rise multifamily housing units in eight buildings. Two of the buildings are stacked townhouses consisting of twenty-four and sixteen units with a total of sixty-eight parking spaces proposed to be developed to service these two buildings. The remaining 23 units are part of three-section and four-section row houses, each unit will have its own driveway. The developer is proposing only one driveway access at Dillon Drive, which is located to the north of the subject lands.

Using recently obtained turning movement counts and applying the best available trip generation and distribution data and methodologies, an analysis was completed to measure the operational impact of the development on traffic conditions on the adjacent intersections. The analysis was carried out assuming full build-out in 2020 and projected horizon years of 2025 and 2030. Background traffic was increased by 2% per year, compounded annually. After modelling the traffic network and extracting the relevant traffic operations metrics, the following conclusions were made:

- The intersection of Dillon Drive at Lesperance Road will be nominally affected by the distribution of the site generated traffic, and it will continue to operate at a very favourable level of service in all horizon traffic scenarios;

- The intersection of Dillon Drive at St. Pierre Street will be nominally affected by the distribution of the site generated traffic, and it will continue to operate at a very favourable level of service in all horizon traffic scenarios;
- The intersection of Dillon Drive at the Site Access is proposed to operate as a single ingress lane and a single egress lane, and it has been determined that this intersection will operate at a very favourable level of service in all horizon traffic scenarios;
- The intersection of Dillon Drive at Lacasse Boulevard will be nominally affected by the distribution of the site generated traffic, and it will continue to operate at a very favourable level of service in all horizon traffic scenarios;
- Existing and projected traffic volumes at non-signalized intersections within the study area do not satisfy the provincial warrants for traffic signalization;
- A northbound passenger vehicle stopped at the proposed Dillon Drive site access should have adequate sight lines to safely egress from the site.

In consideration of the above findings, it is the engineers' opinion that this development will not have an adverse effect on area traffic operations. Dillon Drive has the capacity to accept the added site generated trips, both now and in the horizon years; levels of service at the peripheral intersections are expected to be largely unaffected by the proposed development.

All of which is respectfully submitted,

RC Spencer Associates Inc.




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RC SPENCER ASSOCIATES INC.
Consulting Engineers



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| 2. | REVISED REPORT FIGURES | MAR 01 2021 | M.C.A. | A.D.B. | CHECKED A.D.B. | FIGURE NO. 1 |
| 1. | COMPLETED REPORT FIGURES | MAY 03 2019 | P.B. | A.D.B. | DATE MARCH 2021 | |
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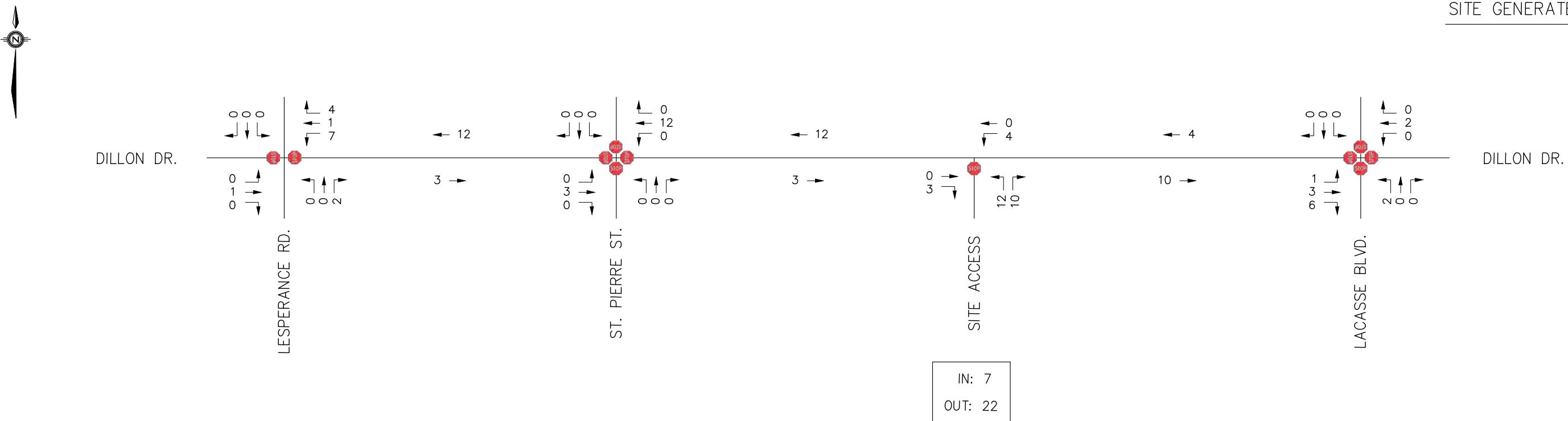
12433 DILLON DRIVE, TECUMSEH – T.I.S.

AREA PLAN

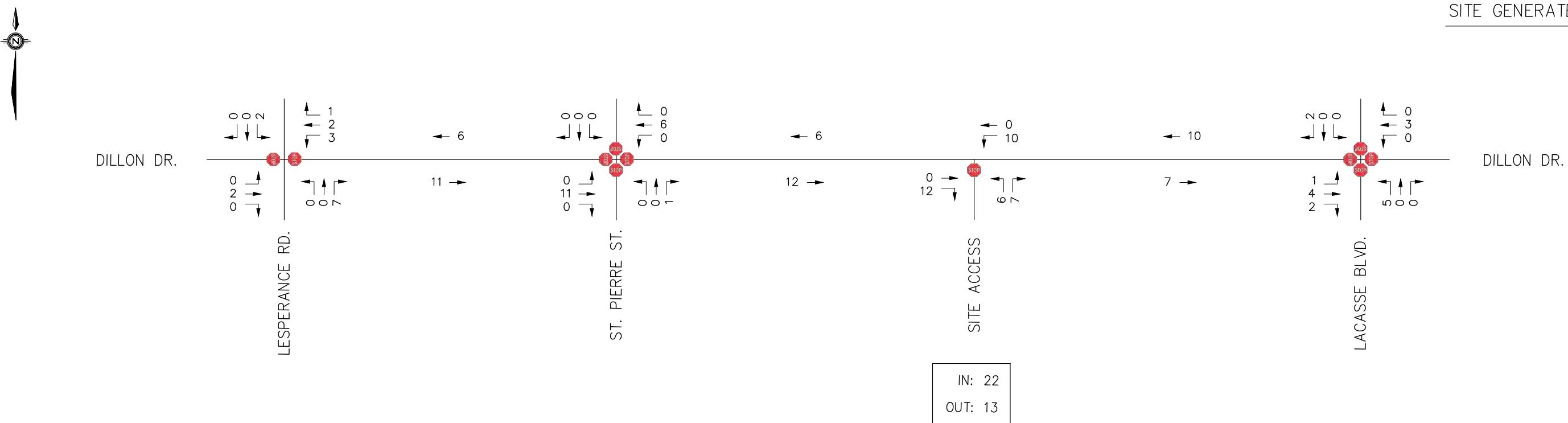


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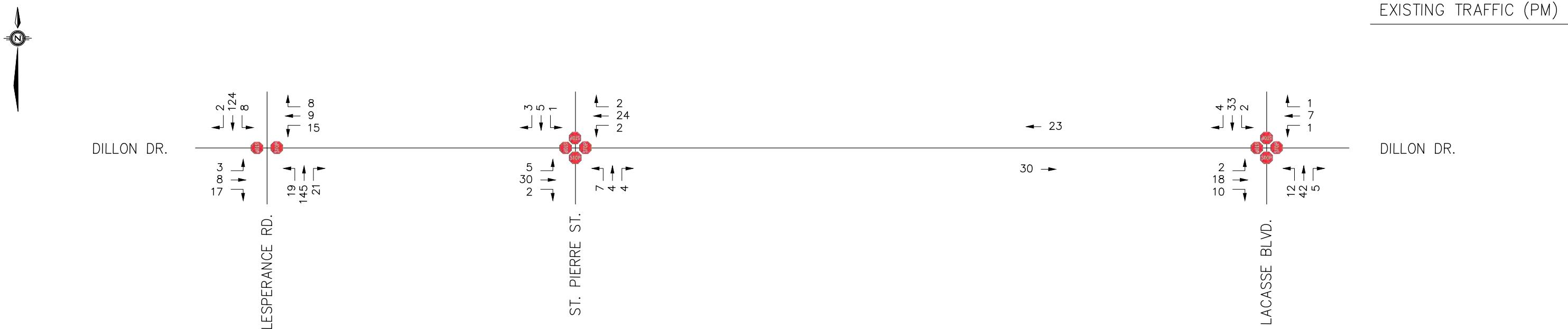
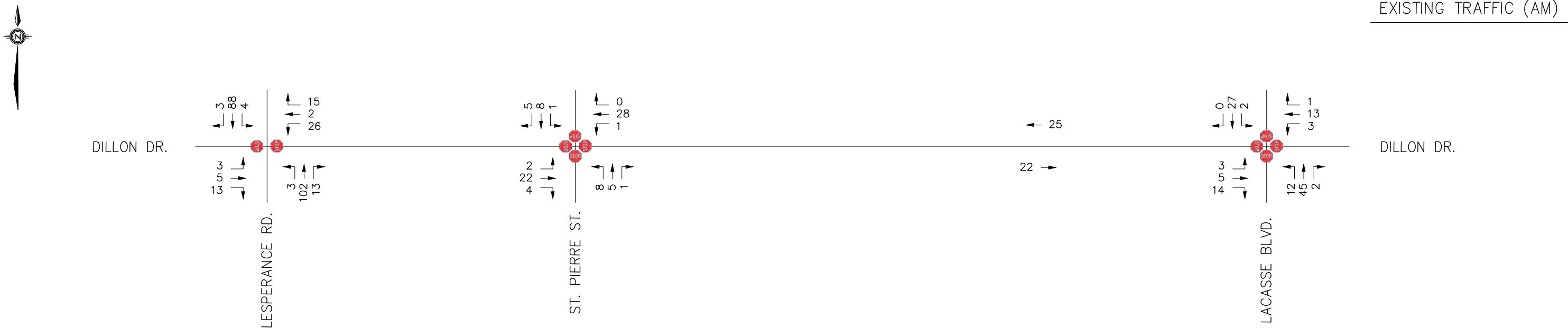
SITE GENERATED TRAFFIC (AM)



SITE GENERATED TRAFFIC (PM)

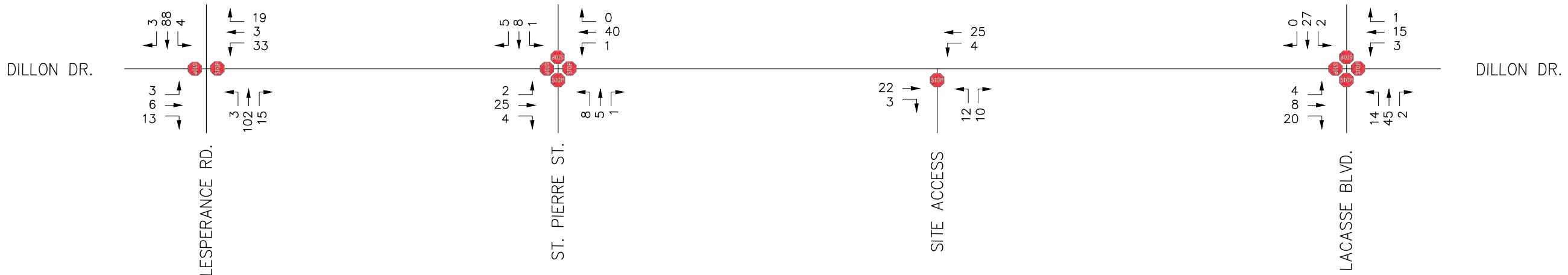


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| | | | | | | | | | FIGURE NO. 3 | |
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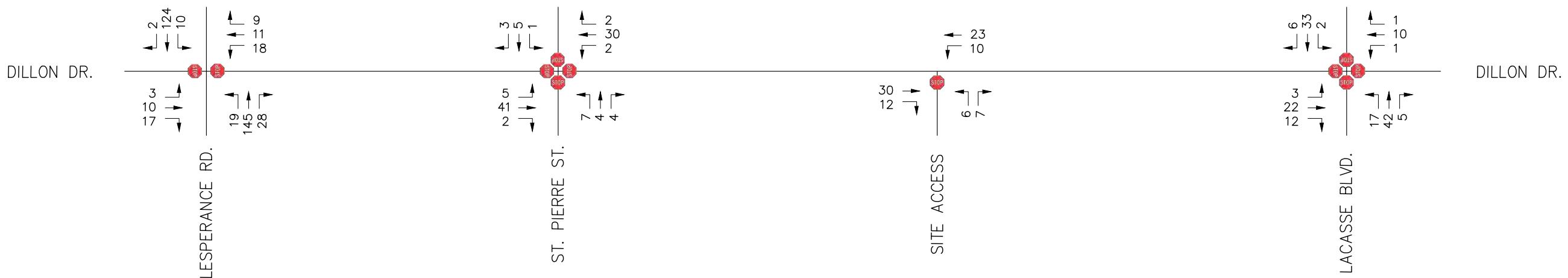
EXISTING + SITE GENERATED TRAFFIC (AM)



IN: 7
OUT: 22

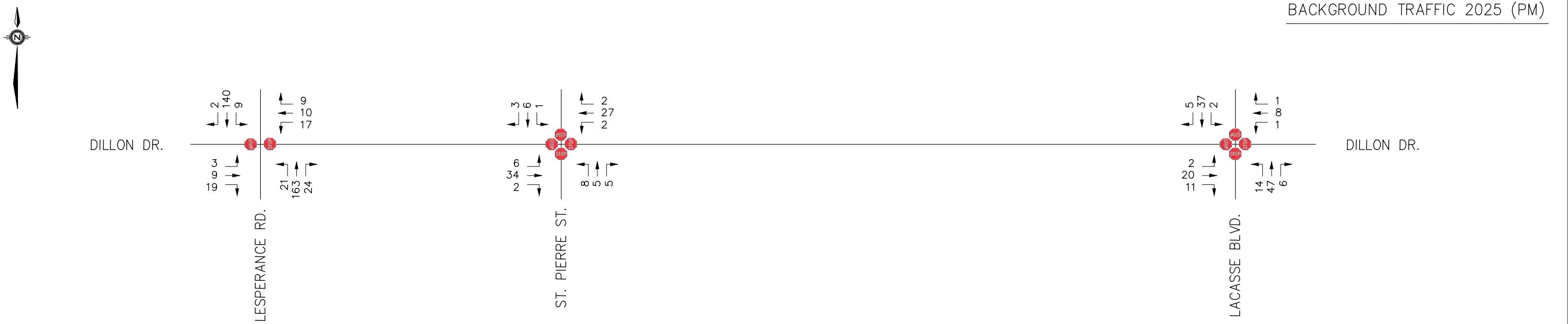
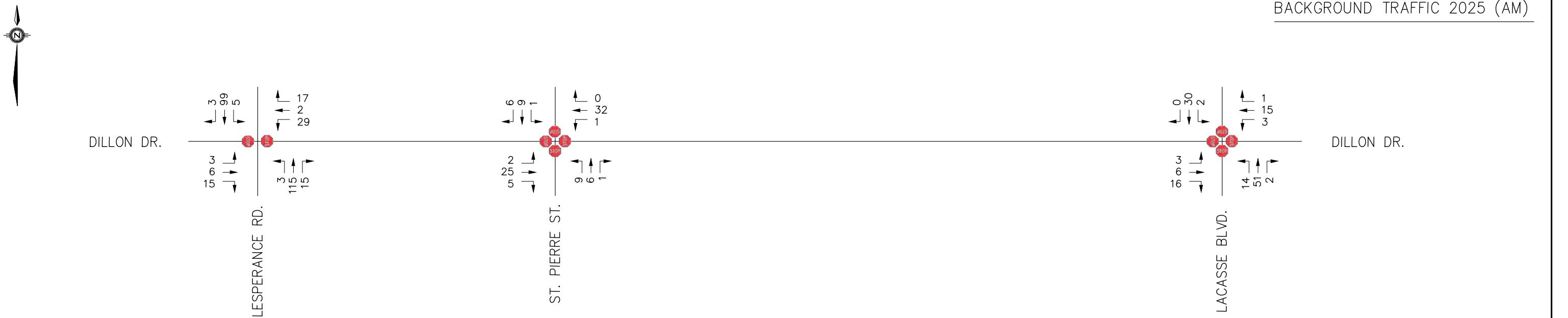


EXISTING + SITE GENERATED TRAFFIC (PM)



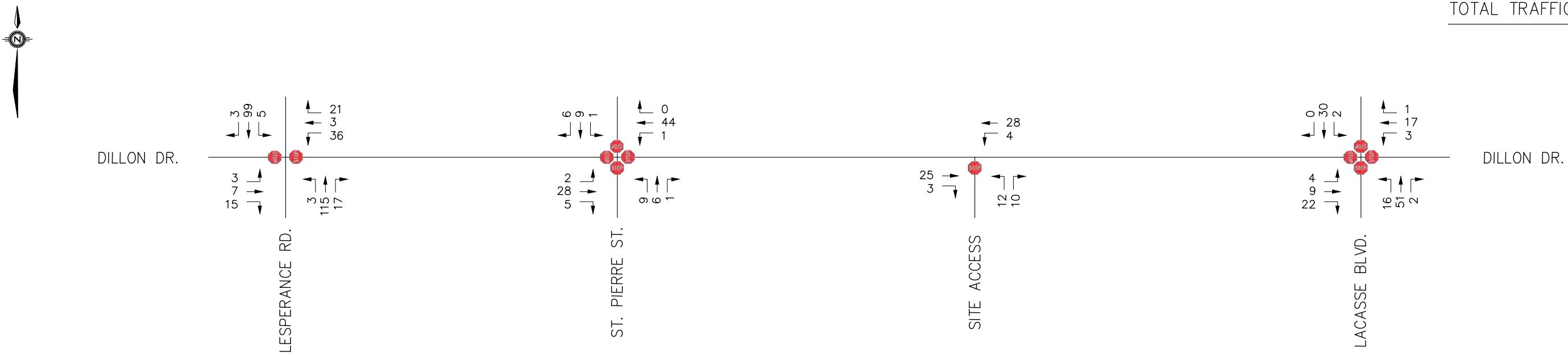
IN: 22
OUT: 13

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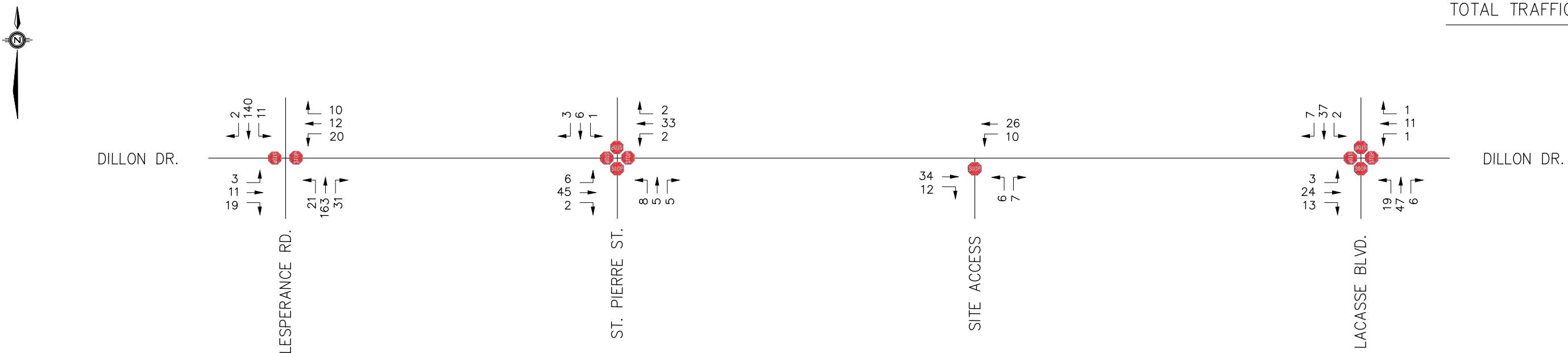


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| | | | | | | CHECKED J.T. | | |
| | | | | | | DRAWN P.B. | | |
| | | | 2. REVISED REPORT FIGURES | MAR 01 2021 | M.C.A | A.D.B. | CHECKED A.D.B. | FIGURE NO. 6 |
| | | | 1. COMPLETED REPORT FIGURES | MAY 03 2019 | P.B. | A.D.B. | DATE MARCH 2021 | |
| | | | NO. | REVISION | DATE | BY APP | SCALE N.T.S. | OF 10 |

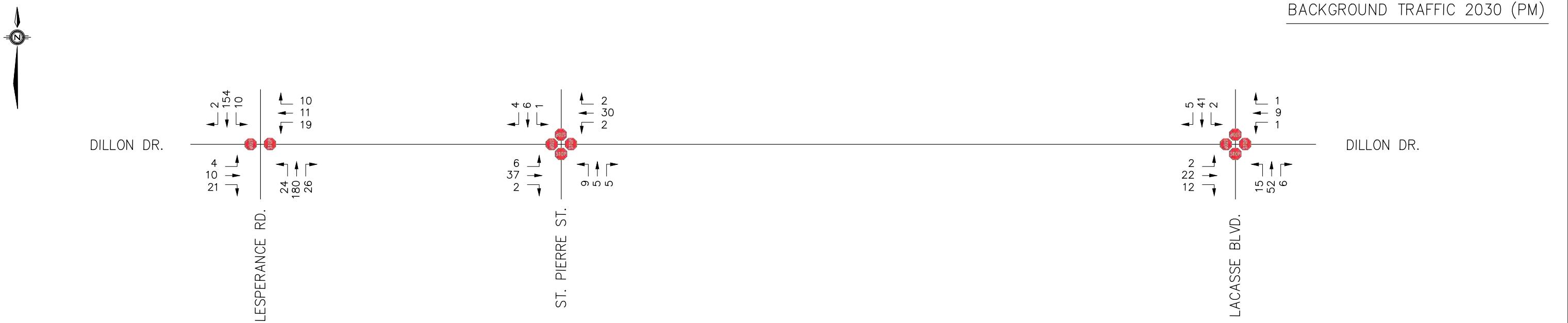
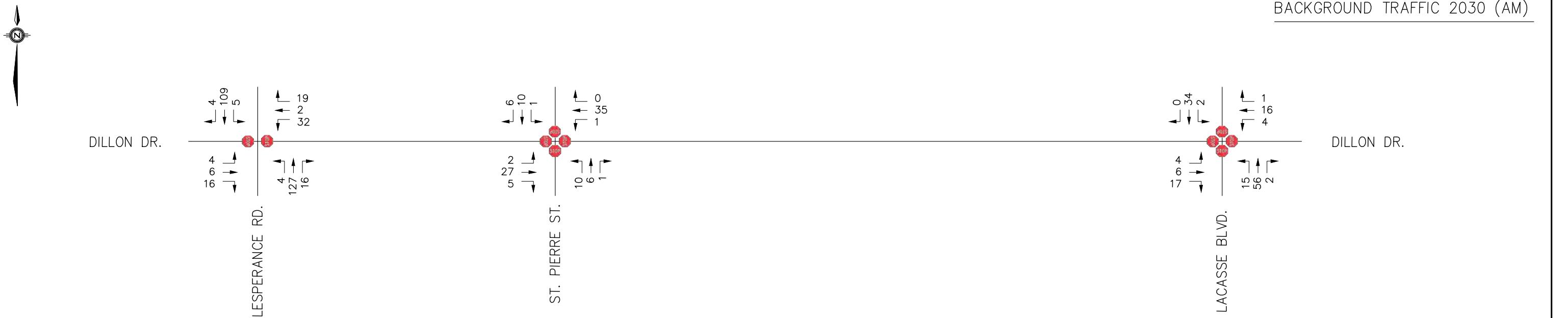
TOTAL TRAFFIC 2025 (AM)



TOTAL TRAFFIC 2025 (PM)

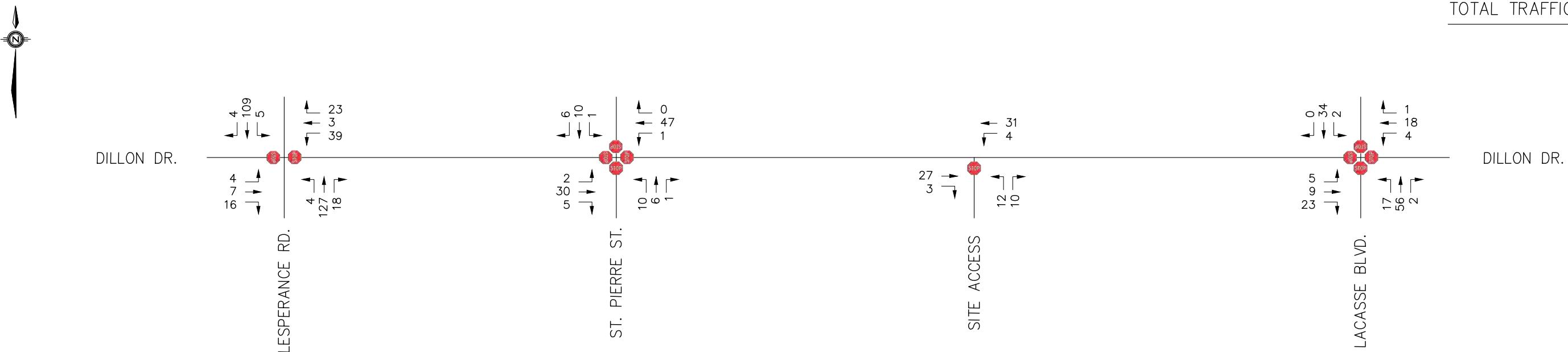


| | | | <p>RC SPENCER ASSOCIATES INC. Consulting Engineers Windsor: 800 University Avenue W. - Windsor ON N9A 5R9 Leamington: 18 Talbot Street W. - Leamington ON N8H 1M4 Chatham-Kent: 49 Raleigh Street - Chatham ON N7M 2M6</p> <p>Professional Engineers Ontario</p> | <table border="1"> <thead> <tr> <th colspan="2"></th> <th>DESIGN A.D.B.</th> <th>PROJECT NO.</th> </tr> <tr> <th colspan="2"></th> <th>CHECKED J.T.</th> <th>19-864</th> </tr> <tr> <th colspan="2"></th> <th>DRAWN P.B.</th> <th></th> </tr> </thead> <tbody> <tr> <td colspan="2">2. REVISED REPORT FIGURES</td> <td>MAR 01 2021 M.C.A. A.D.B.</td> <td>CHECKED A.D.B.</td> </tr> <tr> <td colspan="2">1. COMPLETED REPORT FIGURES</td> <td>MAY 03 2019 P.B. A.D.B.</td> <td>DATE MARCH 2021</td> </tr> <tr> <td>NO.</td> <td>REVISION</td> <td>DATE BY APP</td> <td>SCALE N.T.S.</td> </tr> </tbody> </table> | | | DESIGN A.D.B. | PROJECT NO. | | | CHECKED J.T. | 19-864 | | | DRAWN P.B. | | 2. REVISED REPORT FIGURES | | MAR 01 2021 M.C.A. A.D.B. | CHECKED A.D.B. | 1. COMPLETED REPORT FIGURES | | MAY 03 2019 P.B. A.D.B. | DATE MARCH 2021 | NO. | REVISION | DATE BY APP | SCALE N.T.S. | <p>12433 DILLON DRIVE, TECUMSEH – T.I.S.</p> <p>TOTAL TRAFFIC 2025 (AM/PM PEAK HOUR)</p> | FIGURE NO. 7 OF 10 |
|-----------------------------|----------|---------------------------|--|--|--|--|---------------|-------------|--|--|--------------|--------|--|--|------------|--|---------------------------|--|---------------------------|----------------|-----------------------------|--|-------------------------|-----------------|-----|----------|-------------|--------------|---|--------------------------|
| | | DESIGN A.D.B. | PROJECT NO. | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | CHECKED J.T. | 19-864 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | DRAWN P.B. | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2. REVISED REPORT FIGURES | | MAR 01 2021 M.C.A. A.D.B. | CHECKED A.D.B. | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1. COMPLETED REPORT FIGURES | | MAY 03 2019 P.B. A.D.B. | DATE MARCH 2021 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO. | REVISION | DATE BY APP | SCALE N.T.S. | | | | | | | | | | | | | | | | | | | | | | | | | | | |



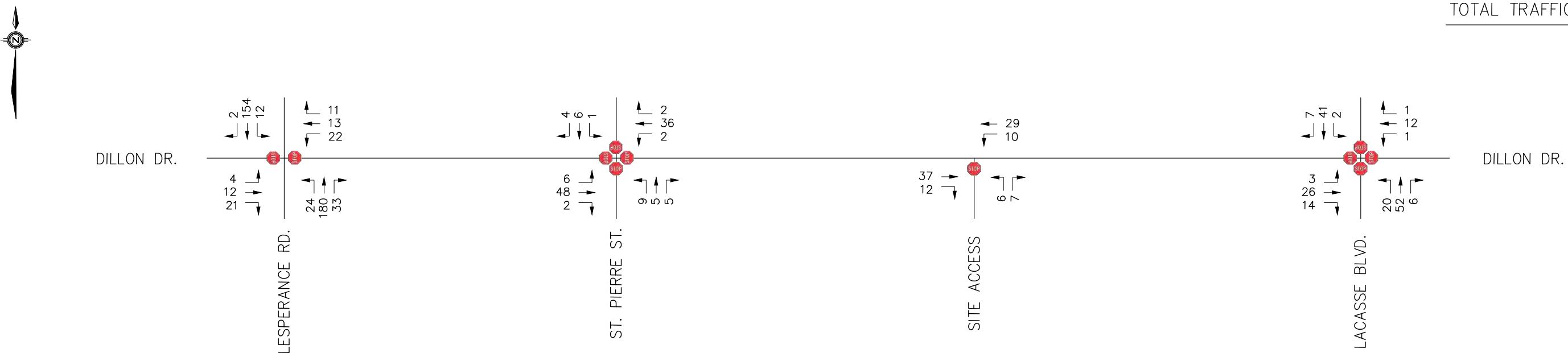
| | | | | | | | | | |
|--|--|--|---|-------------|-------|--------|-----------------|--|-----------------------|
| | | |  RC SPENCER ASSOCIATES INC. Consulting Engineers Windsor: 800 University Avenue W. - Windsor ON N9A 5R9 Leamington: 18 Talbot Street W. - Leamington ON N8H 1M4 Chatham-Kent: 49 Raleigh Street - Chatham ON N7M 2M6 | | | | DESIGN A.D.B. | 12433 DILLON DRIVE, TECUMSEH – T.I.S. | PROJECT NO. 19-864 |
| | | | | | | | CHECKED J.T. | | |
| | | | | | | | DRAWN P.B. | | |
| | | | 2. REVISED REPORT FIGURES | MAR 01 2021 | M.C.A | A.D.B. | CHECKED A.D.B. | | FIGURE NO. |
| | | | 1. COMPLETED REPORT FIGURES | MAY 03 2019 | P.B. | A.D.B. | DATE MARCH 2021 | | 8 |
| | | | NO. | REVISION | DATE | BY APP | SCALE N.T.S. | | OF 10 |
| | | | | | | | | BACKGROUND TRAFFIC 2030 (AM/PM PEAK HOUR) | |

TOTAL TRAFFIC 2030 (AM)



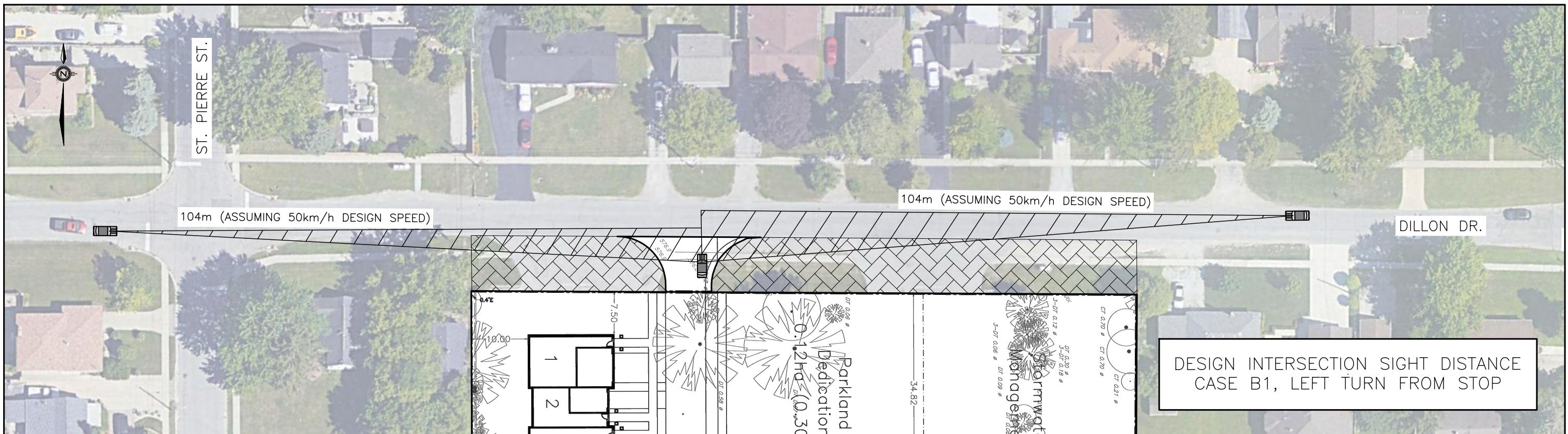
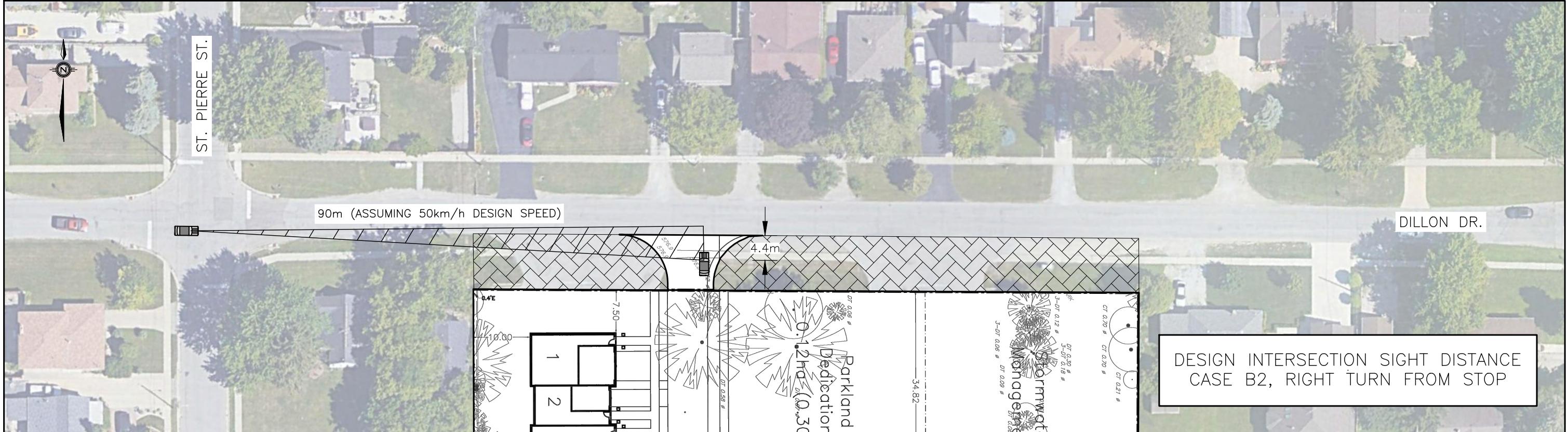
IN: 7
OUT: 22

TOTAL TRAFFIC 2030 (PM)



IN: 22
OUT: 13

| | | | <p>RC SPENCER ASSOCIATES INC. Consulting Engineers Windsor: 800 University Avenue W. - Windsor ON N9A 5R9 Leamington: 18 Talbot Street W. - Leamington ON N8H 1M4 Chatham-Kent: 49 Raleigh Street - Chatham ON N7M 2M6</p> <p>Professional Engineers Ontario</p> | <table border="1"> <thead> <tr> <th colspan="2"></th> <th colspan="2">DESIGN</th> <th>A.D.B.</th> </tr> <tr> <th colspan="2"></th> <th>CHECKED</th> <th>J.T.</th> <th></th> </tr> <tr> <th colspan="2"></th> <th>DRAWN</th> <th>P.B.</th> <th></th> </tr> </thead> <tbody> <tr> <td colspan="2">2. REVISED REPORT FIGURES</td> <td>MAR 01 2021</td> <td>M.C.A.</td> <td>A.D.B.</td> </tr> <tr> <td colspan="2">1. COMPLETED REPORT FIGURES</td> <td>MAY 03 2019</td> <td>P.B.</td> <td>A.D.B.</td> </tr> <tr> <td>NO.</td> <td>REVISION</td> <td>DATE</td> <td>BY APP</td> <td>SCALE N.T.S.</td> </tr> </tbody> </table> | | | DESIGN | | A.D.B. | | | CHECKED | J.T. | | | | DRAWN | P.B. | | 2. REVISED REPORT FIGURES | | MAR 01 2021 | M.C.A. | A.D.B. | 1. COMPLETED REPORT FIGURES | | MAY 03 2019 | P.B. | A.D.B. | NO. | REVISION | DATE | BY APP | SCALE N.T.S. | <p>12433 DILLON DRIVE, TECUMSEH – T.I.S.</p> <p>TOTAL TRAFFIC 2030 (AM/PM PEAK HOUR)</p> | <p>PROJECT NO. 19-864</p> <p>FIGURE NO. 9 OF 10</p> |
|-----------------------------|----------|-------------|--|--|--|--|--------|--|--------|--|--|---------|------|--|--|--|-------|------|--|---------------------------|--|-------------|--------|--------|-----------------------------|--|-------------|------|--------|-----|----------|------|--------|--------------|--|---|
| | | DESIGN | | A.D.B. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | CHECKED | J.T. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | DRAWN | P.B. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2. REVISED REPORT FIGURES | | MAR 01 2021 | M.C.A. | A.D.B. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1. COMPLETED REPORT FIGURES | | MAY 03 2019 | P.B. | A.D.B. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NO. | REVISION | DATE | BY APP | SCALE N.T.S. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |



| | | | <p>RC SPENCER ASSOCIATES INC. Consulting Engineers Windsor: 800 University Avenue W. - Windsor ON N9A 5R9 Leamington: 18 Talbot Street W. - Leamington ON N8H 1M4 Chatham-Kent: 49 Raleigh Street - Chatham ON N7M 2M6</p> <p>Professional Engineers Ontario</p> | <table border="1"> <thead> <tr> <th></th> <th></th> <th></th> <th>DESIGN A.D.B. CHECKED J.T.</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td></td> <td>DRAWN P.B.</td> </tr> <tr> <td>2.</td> <td>REVISED REPORT FIGURES</td> <td>MAR 01 2021</td> <td>checked A.D.B.</td> </tr> <tr> <td>1.</td> <td>COMPLETED REPORT FIGURES</td> <td>MAY 03 2019</td> <td>P.B. A.D.B. DATE MARCH 2021</td> </tr> <tr> <td>NO.</td> <td>REVISION</td> <td>DATE BY APP</td> <td>SCALE N.T.S.</td> </tr> </tbody> </table> | | | | DESIGN A.D.B. CHECKED J.T. | | | | DRAWN P.B. | 2. | REVISED REPORT FIGURES | MAR 01 2021 | checked A.D.B. | 1. | COMPLETED REPORT FIGURES | MAY 03 2019 | P.B. A.D.B. DATE MARCH 2021 | NO. | REVISION | DATE BY APP | SCALE N.T.S. | <p>12433 DILLON DRIVE, TECUMSEH – T.I.S.</p> <p>SIGHT LINE ANALYSIS SITE ACCESS</p> | <p>PROJECT NO. 19-864</p> <p>FIGURE NO. 10 OF 10</p> |
|-----|--------------------------|-------------|--|---|--|--|--|-------------------------------|--|--|--|------------|----|------------------------|-------------|----------------|----|--------------------------|-------------|-----------------------------|-----|----------|-------------|--------------|---|--|
| | | | DESIGN A.D.B. CHECKED J.T. | | | | | | | | | | | | | | | | | | | | | | | |
| | | | DRAWN P.B. | | | | | | | | | | | | | | | | | | | | | | | |
| 2. | REVISED REPORT FIGURES | MAR 01 2021 | checked A.D.B. | | | | | | | | | | | | | | | | | | | | | | | |
| 1. | COMPLETED REPORT FIGURES | MAY 03 2019 | P.B. A.D.B. DATE MARCH 2021 | | | | | | | | | | | | | | | | | | | | | | | |
| NO. | REVISION | DATE BY APP | SCALE N.T.S. | | | | | | | | | | | | | | | | | | | | | | | |

Appendix A

TRAFFIC COUNTS

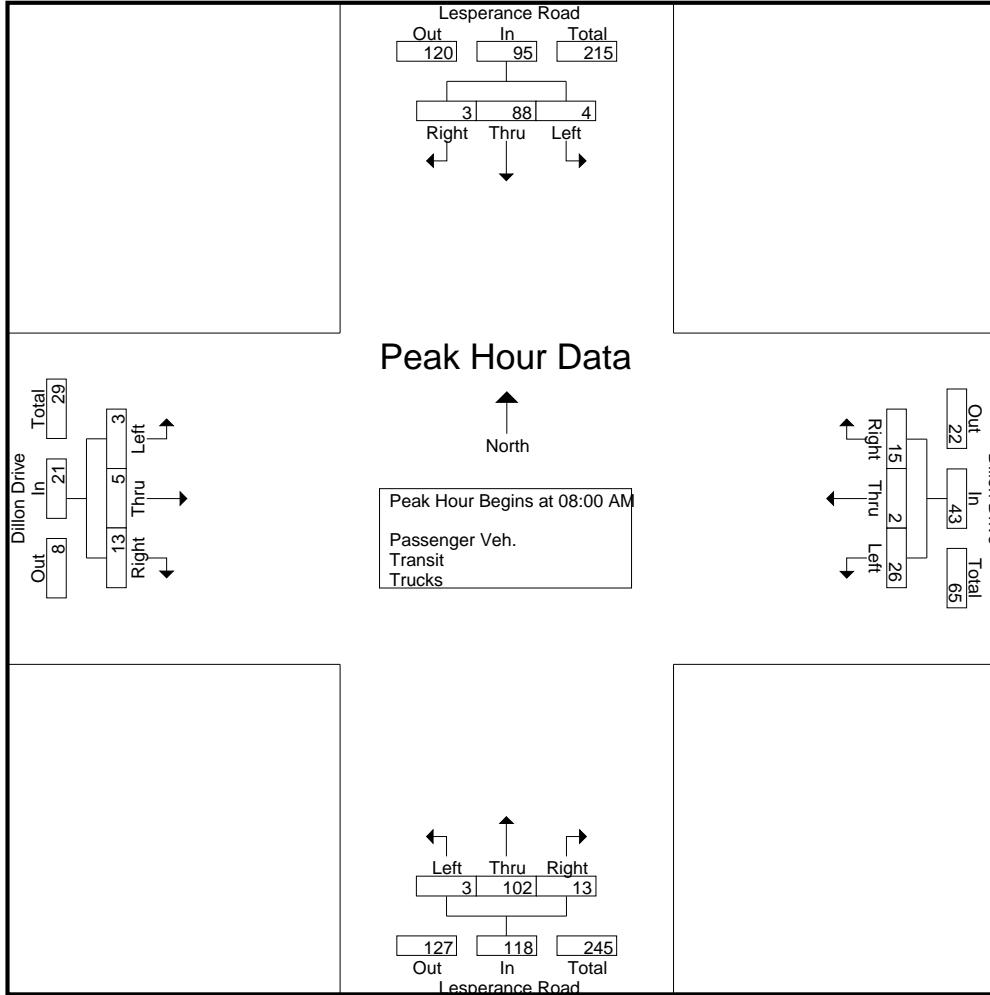
Dillon Drive at Lesperance Road

Dillon Drive at St. Pierre Street

Dillon Drive at Lacasse Boulevard

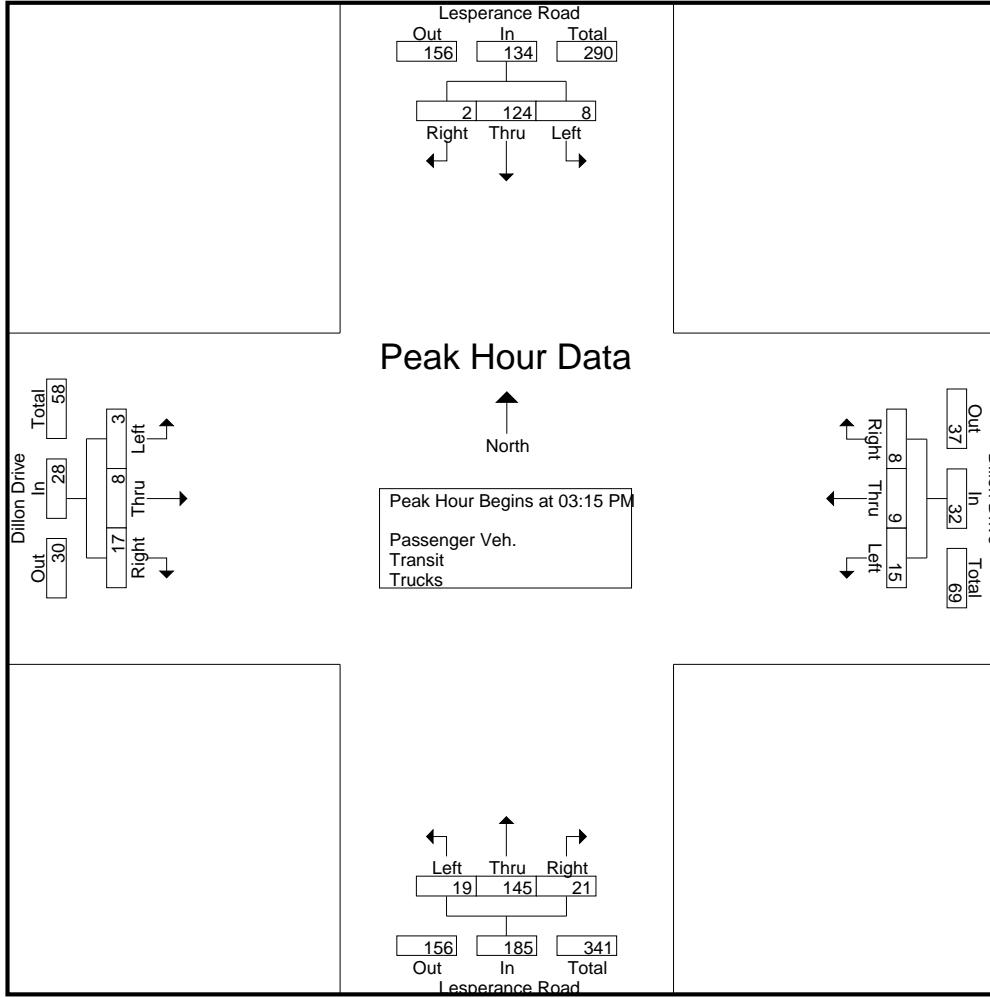


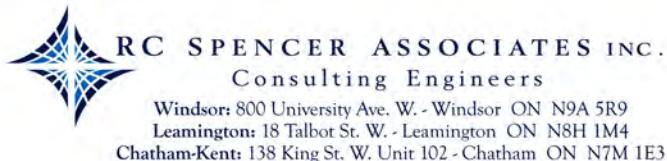
| | Dillon Drive W/B | | | | Lesperance Road N/B | | | | Lesperance Road S/B | | | | Dillon Drive E/B | | | | |
|--|---------------------|------|------|------------|------------------------|------|------|------------|------------------------|------|------|------------|---------------------|------|------|------------|------------|
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Analysis From 07:00 AM to 11:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | |
| 08:00 AM | 3 | 0 | 6 | 9 | 3 | 18 | 1 | 22 | 0 | 22 | 0 | 22 | 2 | 0 | 1 | 3 | 56 |
| 08:15 AM | 3 | 0 | 5 | 8 | 2 | 29 | 1 | 32 | 2 | 24 | 2 | 28 | 6 | 0 | 0 | 6 | 74 |
| 08:30 AM | 5 | 2 | 7 | 14 | 5 | 25 | 1 | 31 | 0 | 21 | 1 | 22 | 2 | 3 | 0 | 5 | 72 |
| 08:45 AM | 4 | 0 | 8 | 12 | 3 | 30 | 0 | 33 | 1 | 21 | 1 | 23 | 3 | 2 | 2 | 7 | 75 |
| Total Volume | 15 | 2 | 26 | 43 | 13 | 102 | 3 | 118 | 3 | 88 | 4 | 95 | 13 | 5 | 3 | 21 | 277 |
| % App. Total | 34.9 | 4.7 | 60.5 | | 11 | 86.4 | 2.5 | | 3.2 | 92.6 | 4.2 | | 61.9 | 23.8 | 14.3 | | |
| PHF | .750 | .250 | .813 | .768 | .650 | .850 | .750 | .894 | .375 | .917 | .500 | .848 | .542 | .417 | .375 | .750 | .923 |





| | Dillon Drive W/B | | | | Lesperance Road N/B | | | | Lesperance Road S/B | | | | Dillon Drive E/B | | | | |
|--|---------------------|------|------|------------|------------------------|------|------|------------|------------------------|------|------|------------|---------------------|------|------|------------|------------|
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Analysis From 12:00 PM to 05:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 03:15 PM | | | | | | | | | | | | | | | | | |
| 03:15 PM | 2 | 3 | 3 | 8 | 6 | 53 | 5 | 64 | 0 | 34 | 2 | 36 | 4 | 1 | 1 | 6 | 114 |
| 03:30 PM | 1 | 1 | 7 | 9 | 4 | 29 | 4 | 37 | 1 | 33 | 0 | 34 | 5 | 3 | 0 | 8 | 88 |
| 03:45 PM | 3 | 3 | 2 | 8 | 5 | 35 | 3 | 43 | 1 | 22 | 3 | 26 | 3 | 2 | 1 | 6 | 83 |
| 04:00 PM | 2 | 2 | 3 | 7 | 6 | 28 | 7 | 41 | 0 | 35 | 3 | 38 | 5 | 2 | 1 | 8 | 94 |
| Total Volume | 8 | 9 | 15 | 32 | 21 | 145 | 19 | 185 | 2 | 124 | 8 | 134 | 17 | 8 | 3 | 28 | 379 |
| % App. Total | 25 | 28.1 | 46.9 | | 11.4 | 78.4 | 10.3 | | 1.5 | 92.5 | 6 | | 60.7 | 28.6 | 10.7 | | |
| PHF | .667 | .750 | .536 | .889 | .875 | .684 | .679 | .723 | .500 | .886 | .667 | .882 | .850 | .667 | .750 | .875 | .831 |





Date: May 2, 2019

Counted by: Parth Bhatt

Weather Conditions: Overcast

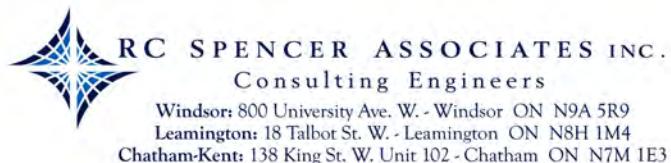
St. Pierre Street at Dillon Drive

Groups Printed- P. Veh. - Buses - Trucks

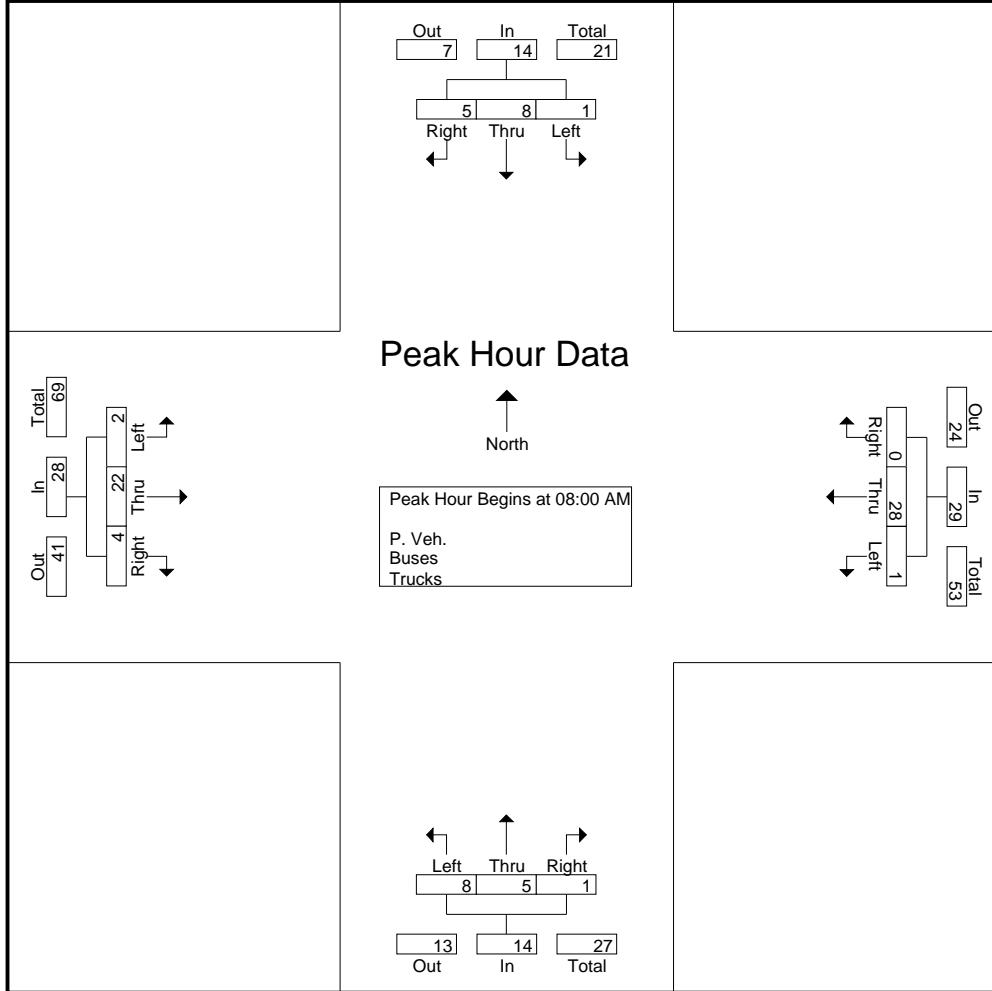
| Start Time | N/B | | | | | S/B | | | | | E/B | | | | | W/B | | | | | Excl. Total | Inclu. Total | Int. Total |
|------------|-------|------|------|------|------------|-------|------|------|------|------------|-------|------|------|------|------------|-------|------|------|------|------------|-------------|--------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | | | |
| 08:00 AM | 1 | 2 | 2 | (0) | 5 | 1 | 3 | 1 | (0) | 5 | 1 | 5 | 0 | (0) | 6 | 0 | 4 | 1 | (0) | 5 | 0 | 21 | 21 |
| 08:15 AM | 0 | 1 | 0 | (0) | 1 | 2 | 2 | 0 | (0) | 4 | 1 | 5 | 2 | (0) | 8 | 0 | 7 | 0 | (0) | 7 | 0 | 20 | 20 |
| 08:30 AM | 0 | 2 | 4 | (0) | 6 | 2 | 1 | 0 | (0) | 3 | 2 | 7 | 0 | (0) | 9 | 0 | 11 | 0 | (1) | 11 | 1 | 29 | 30 |
| 08:45 AM | 0 | 0 | 2 | (1) | 2 | 0 | 2 | 0 | (1) | 2 | 0 | 5 | 0 | (0) | 5 | 0 | 6 | 0 | (2) | 6 | 4 | 15 | 19 |
| Total | 1 | 5 | 8 | (1) | 14 | 5 | 8 | 1 | (1) | 14 | 4 | 22 | 2 | (0) | 28 | 0 | 28 | 1 | (3) | 29 | 5 | 85 | 90 |

** BREAK **

| | | | | | | | | | | | | | | | | | | | | | | | | |
|-------------|------|------|------|-----|----|------|------|-----|-----|----|------|-----|------|-----|----|------|------|------|-----|----|----|------|-----|------|
| 03:15 PM | 4 | 1 | 1 | (1) | 6 | 2 | 2 | 0 | (0) | 4 | 0 | 4 | 2 | (1) | 6 | 0 | 5 | 1 | (2) | 6 | 4 | 22 | 26 | |
| 03:30 PM | 0 | 1 | 2 | (0) | 3 | 0 | 1 | 0 | (0) | 1 | 0 | 8 | 0 | (0) | 8 | 1 | 5 | 0 | (0) | 6 | 0 | 18 | 18 | |
| 03:45 PM | 0 | 2 | 2 | (0) | 4 | 1 | 0 | 0 | (1) | 1 | 2 | 10 | 1 | (0) | 13 | 1 | 11 | 0 | (2) | 12 | 3 | 30 | 33 | |
| Total | 4 | 4 | 5 | (1) | 13 | 3 | 3 | 0 | (1) | 6 | 2 | 22 | 3 | (1) | 27 | 2 | 21 | 1 | (4) | 24 | 7 | 70 | 77 | |
| 04:00 PM | 0 | 0 | 2 | (0) | 2 | 0 | 2 | 1 | (0) | 3 | 0 | 8 | 2 | (0) | 10 | 0 | 3 | 1 | (0) | 4 | 0 | 19 | 19 | |
| Grand Total | 5 | 9 | 15 | (2) | 29 | 8 | 13 | 2 | (2) | 23 | 6 | 52 | 7 | (1) | 65 | 2 | 52 | 3 | (7) | 57 | 12 | 174 | 186 | |
| Apprch % | 17.2 | 31 | 51.7 | | | 34.8 | 56.5 | 8.7 | | | 9.2 | 80 | 10.8 | | | 3.5 | 91.2 | 5.3 | | | | | | |
| Total % | 2.9 | 5.2 | 8.6 | | | 16.7 | 4.6 | 7.5 | 1.1 | | 13.2 | 3.4 | 29.9 | 4 | | 37.4 | 1.1 | 29.9 | 1.7 | | | 32.8 | 6.5 | 93.5 |
| P. Veh. | 3 | 7 | 15 | | | 27 | 8 | 13 | 2 | | 25 | 6 | 52 | 7 | | 66 | 2 | 51 | 3 | | | 0 | 0 | 181 |
| % P. Veh. | 60 | 77.8 | 100 | | | 87.1 | 100 | 100 | 100 | | 100 | 100 | 100 | 100 | | 100 | 98.1 | 100 | 100 | | 0 | 0 | 0 | 97.3 |
| Buses | 2 | 2 | 0 | | | 4 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 1 | 0 | | | 0 | 0 | 0 | 5 |
| % Buses | 40 | 22.2 | 0 | | | 12.9 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 1.9 | 0 | 0 | | 0 | 0 | 0 | 2.7 |
| Trucks | 0 | 0 | 0 | | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | | | 0 | 0 | 0 | 0 |
| % Trucks | 0 | 0 | 0 | | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | | | 0 | 0 | 0 | 0 |

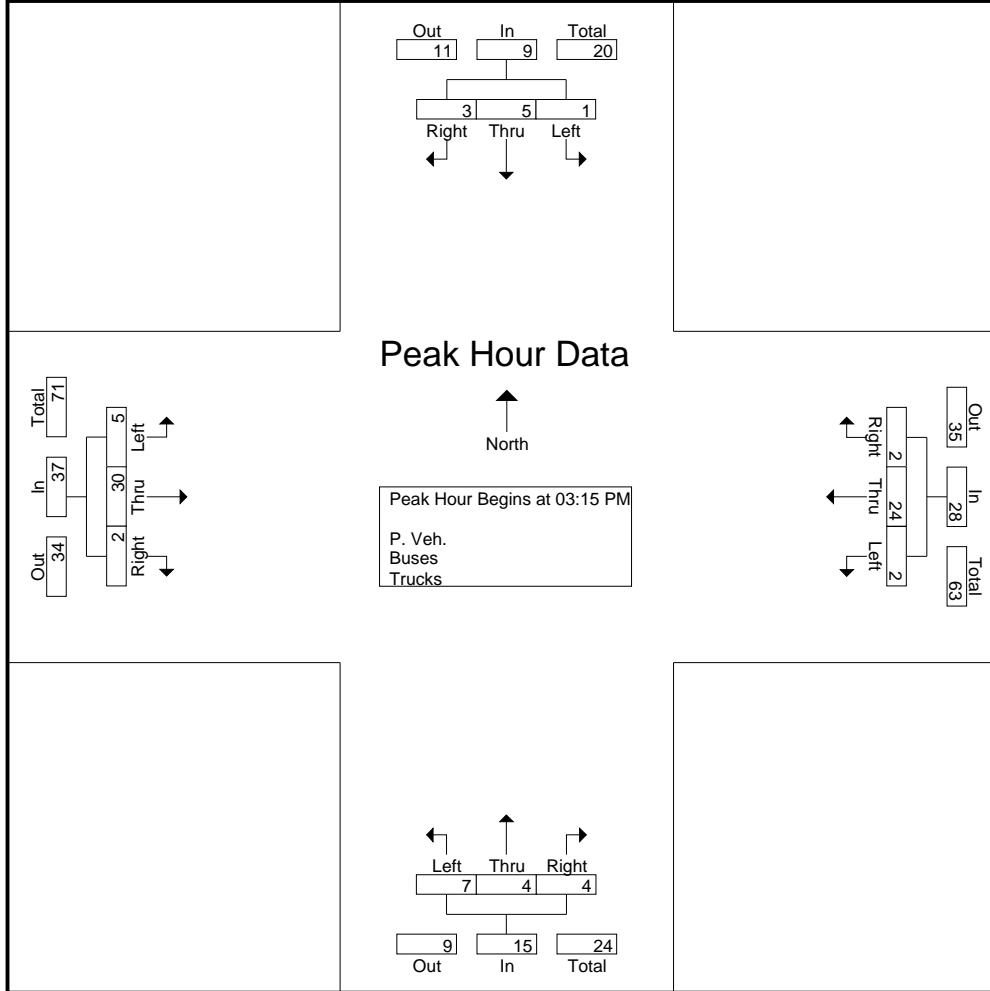


| | N/B | | | | S/B | | | | E/B | | | | W/B | | | | |
|---|-------|------|------|------------|-------|------|------|------------|-------|------|------|------------|-------|------|------|------------|------------|
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Analysis From 08:00 AM to 11:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | |
| 08:00 AM | 1 | 2 | 2 | 5 | 1 | 3 | 1 | 5 | 1 | 5 | 0 | 6 | 0 | 4 | 1 | 5 | 21 |
| 08:15 AM | 0 | 1 | 0 | 1 | 2 | 2 | 0 | 4 | 1 | 5 | 2 | 8 | 0 | 7 | 0 | 7 | 20 |
| 08:30 AM | 0 | 2 | 4 | 6 | 2 | 1 | 0 | 3 | 2 | 7 | 0 | 9 | 0 | 11 | 0 | 11 | 29 |
| 08:45 AM | 0 | 0 | 2 | 2 | 0 | 2 | 0 | 2 | 0 | 5 | 0 | 5 | 0 | 6 | 0 | 6 | 15 |
| Total Volume | 1 | 5 | 8 | 14 | 5 | 8 | 1 | 14 | 4 | 22 | 2 | 28 | 0 | 28 | 1 | 29 | 85 |
| % App. Total | 7.1 | 35.7 | 57.1 | | 35.7 | 57.1 | 7.1 | | 14.3 | 78.6 | 7.1 | | 0 | 96.6 | 3.4 | | |
| PHF | .250 | .625 | .500 | .583 | .625 | .667 | .250 | .700 | .500 | .786 | .250 | .778 | .000 | .636 | .250 | .659 | .733 |



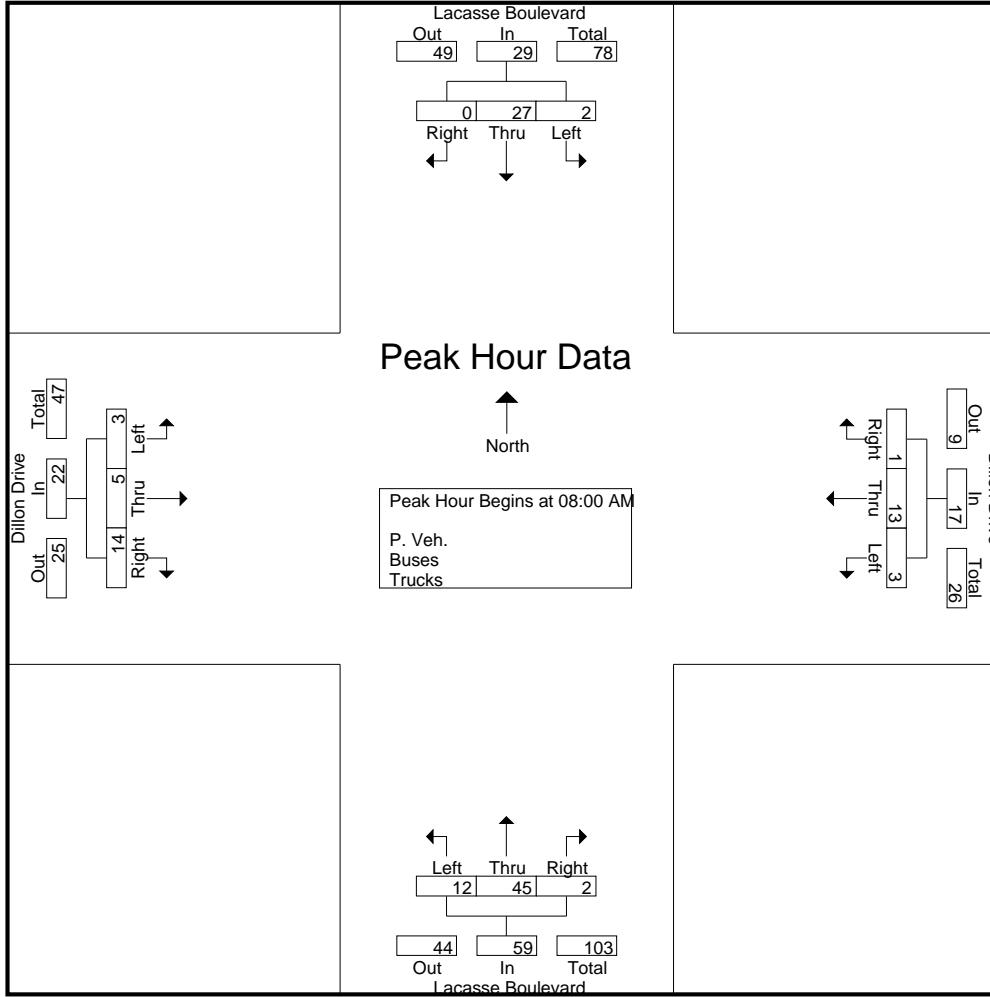


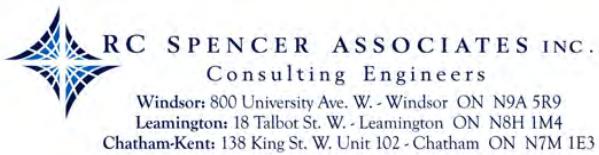
| Start Time | N/B | | | | S/B | | | | E/B | | | | W/B | | | | Int. Total | |
|---|-------|------|------|------------|-------|------|------|------------|-------|------|------|------------|-------|------|------|------------|------------|--|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | | |
| Peak Hour Analysis From 12:00 PM to 04:00 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 03:15 PM | | | | | | | | | | | | | | | | | | |
| 03:15 PM | 4 | 1 | 1 | 6 | 2 | 2 | 0 | 4 | 0 | 4 | 2 | 6 | 0 | 5 | 1 | 6 | 22 | |
| 03:30 PM | 0 | 1 | 2 | 3 | 0 | 1 | 0 | 1 | 0 | 8 | 0 | 8 | 1 | 5 | 0 | 6 | 18 | |
| 03:45 PM | 0 | 2 | 2 | 4 | 1 | 0 | 0 | 1 | 2 | 10 | 1 | 13 | 1 | 11 | 0 | 12 | 30 | |
| 04:00 PM | 0 | 0 | 2 | 2 | 0 | 2 | 1 | 3 | 0 | 8 | 2 | 10 | 0 | 3 | 1 | 4 | 19 | |
| Total Volume | 4 | 4 | 7 | 15 | 3 | 5 | 1 | 9 | 2 | 30 | 5 | 37 | 2 | 24 | 2 | 28 | 89 | |
| % App. Total | 26.7 | 26.7 | 46.7 | | 33.3 | 55.6 | 11.1 | | 5.4 | 81.1 | 13.5 | | 7.1 | 85.7 | 7.1 | | | |
| PHF | .250 | .500 | .875 | .625 | .375 | .625 | .250 | .563 | .250 | .750 | .625 | .712 | .500 | .545 | .500 | .583 | .742 | |



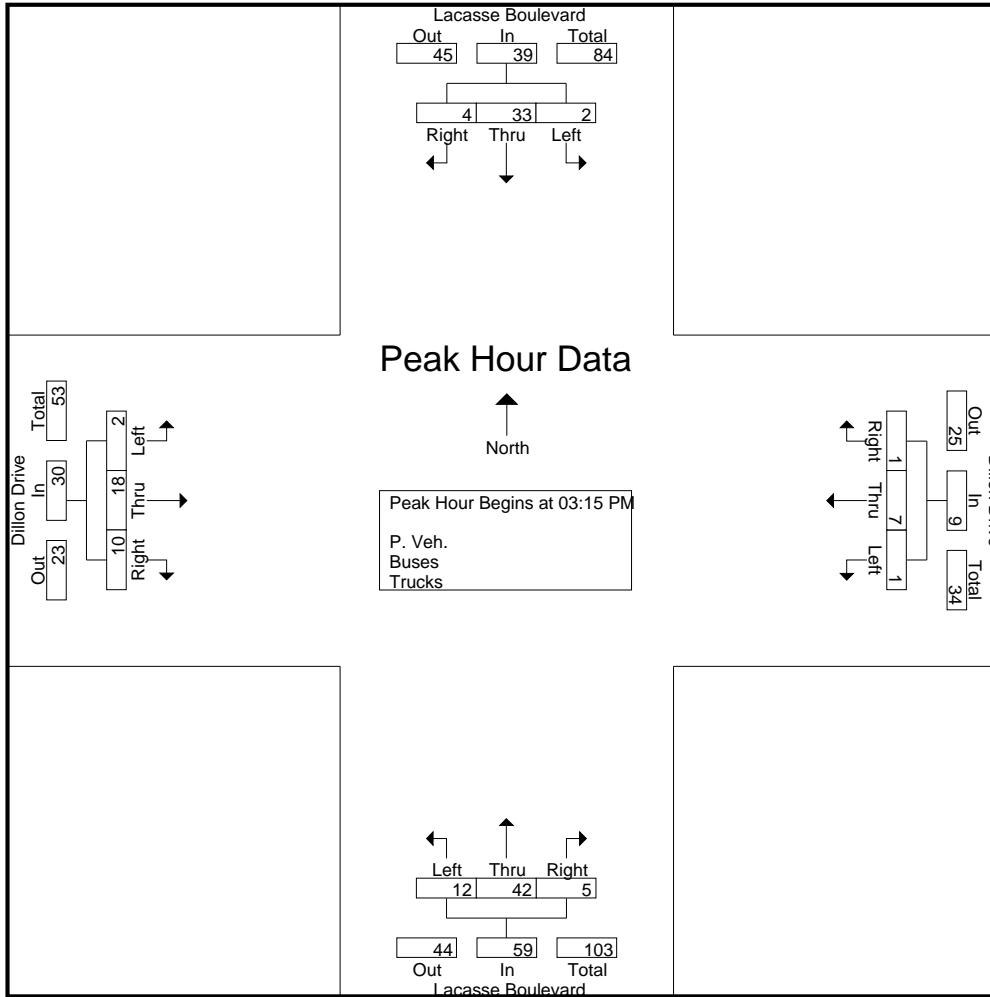


| | Dillon Drive W/B | | | | Lacasse Boulevard N/B | | | | Lacasse Boulevard S/B | | | | Dillon Drive E/B | | | | |
|---|---------------------|------|------|------------|--------------------------|------|------|------------|--------------------------|------|------|------------|---------------------|------|------|------------|------------|
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Analysis From 08:00 AM to 11:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | |
| 08:00 AM | 0 | 2 | 0 | 2 | 0 | 7 | 0 | 7 | 0 | 4 | 0 | 4 | 4 | 0 | 1 | 5 | 18 |
| 08:15 AM | 0 | 6 | 0 | 6 | 2 | 13 | 3 | 18 | 0 | 7 | 2 | 9 | 1 | 0 | 1 | 2 | 35 |
| 08:30 AM | 1 | 0 | 3 | 4 | 0 | 18 | 6 | 24 | 0 | 12 | 0 | 12 | 7 | 1 | 1 | 9 | 49 |
| 08:45 AM | 0 | 5 | 0 | 5 | 0 | 7 | 3 | 10 | 0 | 4 | 0 | 4 | 2 | 4 | 0 | 6 | 25 |
| Total Volume | 1 | 13 | 3 | 17 | 2 | 45 | 12 | 59 | 0 | 27 | 2 | 29 | 14 | 5 | 3 | 22 | 127 |
| % App. Total | 5.9 | 76.5 | 17.6 | | 3.4 | 76.3 | 20.3 | | 0 | 93.1 | 6.9 | | 63.6 | 22.7 | 13.6 | | |
| PHF | .250 | .542 | .250 | .708 | .250 | .625 | .500 | .615 | .000 | .563 | .250 | .604 | .500 | .313 | .750 | .611 | .648 |





| | Dillon Drive W/B | | | | Lacasse Boulevard N/B | | | | Lacasse Boulevard S/B | | | | Dillon Drive E/B | | | | |
|---|---------------------|------|------|------------|--------------------------|------|------|------------|--------------------------|------|------|------------|---------------------|------|------|------------|------------|
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Analysis From 12:00 PM to 04:00 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 03:15 PM | | | | | | | | | | | | | | | | | |
| 03:15 PM | 0 | 3 | 0 | 3 | 2 | 8 | 5 | 15 | 1 | 10 | 1 | 12 | 2 | 4 | 2 | 8 | 38 |
| 03:30 PM | 0 | 0 | 0 | 0 | 0 | 18 | 3 | 21 | 0 | 8 | 0 | 8 | 2 | 6 | 0 | 8 | 37 |
| 03:45 PM | 0 | 1 | 0 | 1 | 1 | 10 | 2 | 13 | 2 | 7 | 1 | 10 | 5 | 5 | 0 | 10 | 34 |
| 04:00 PM | 1 | 3 | 1 | 5 | 2 | 6 | 2 | 10 | 1 | 8 | 0 | 9 | 1 | 3 | 0 | 4 | 28 |
| Total Volume | 1 | 7 | 1 | 9 | 5 | 42 | 12 | 59 | 4 | 33 | 2 | 39 | 10 | 18 | 2 | 30 | 137 |
| % App. Total | 11.1 | 77.8 | 11.1 | | 8.5 | 71.2 | 20.3 | | 10.3 | 84.6 | 5.1 | | 33.3 | 60 | 6.7 | | |
| PHF | .250 | .583 | .250 | .450 | .625 | .583 | .600 | .702 | .500 | .825 | .500 | .813 | .500 | .750 | .250 | .750 | .901 |



Appendix B

ITE TRIP GENERATION MANUAL – 10TH EDITION

REFERENCES

Multifamily Housing (Low-Rise) (220)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban

Number of Studies: 42

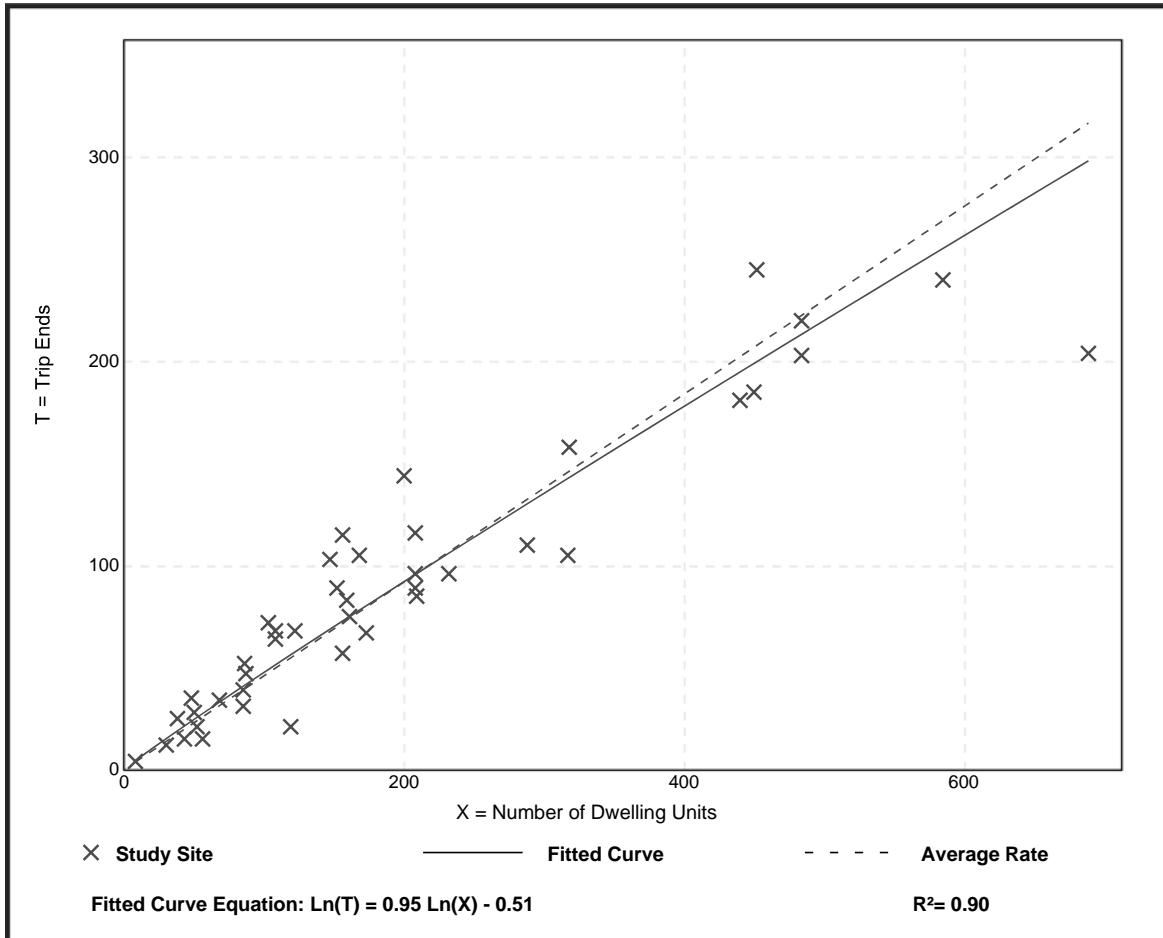
Avg. Num. of Dwelling Units: 199

Directional Distribution: 23% entering, 77% exiting

Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.46 | 0.18 - 0.74 | 0.12 |

Data Plot and Equation



Multifamily Housing (Low-Rise) (220)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 4 and 6 p.m.

Setting/Location: General Urban/Suburban

Number of Studies: 50

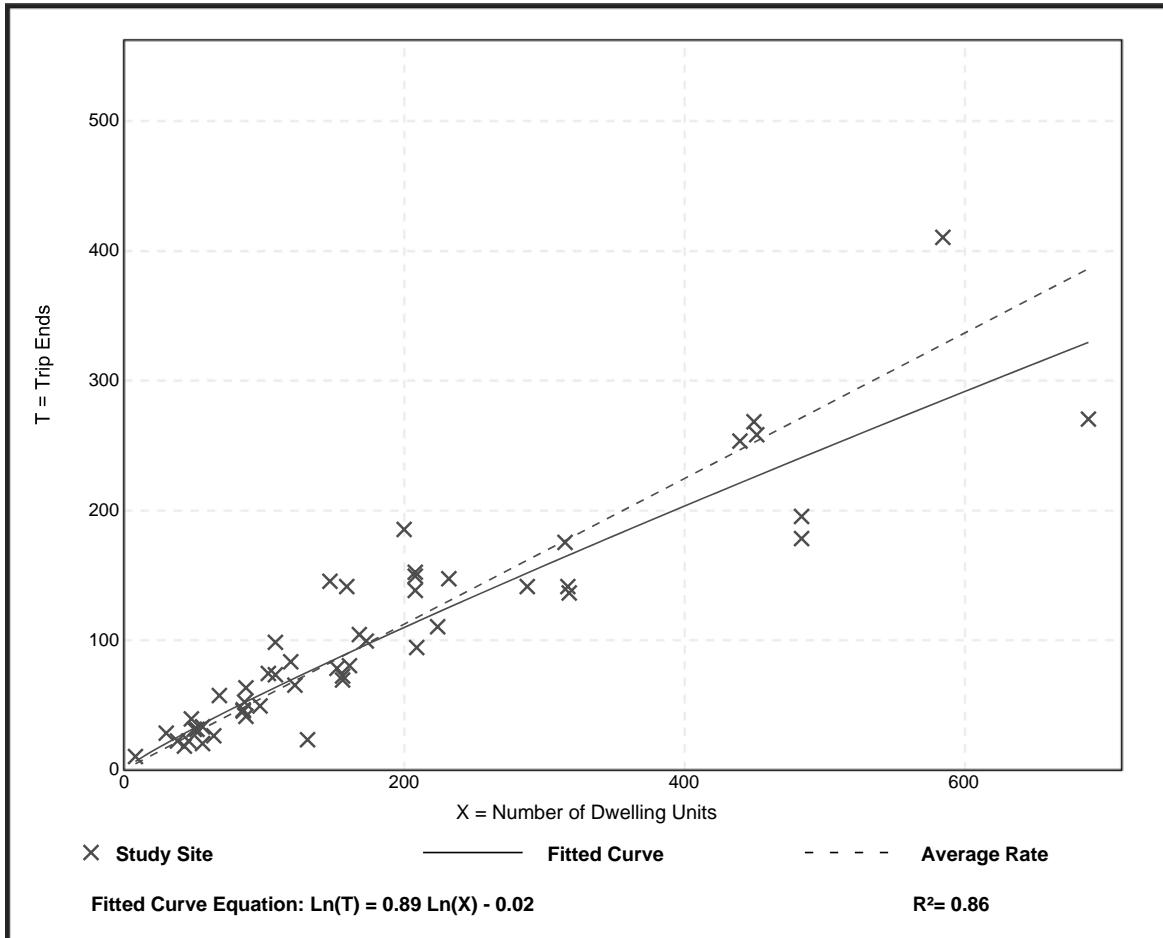
Avg. Num. of Dwelling Units: 187

Directional Distribution: 63% entering, 37% exiting

Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.56 | 0.18 - 1.25 | 0.16 |

Data Plot and Equation



Proposed Site Development Trip Generation and Distribution

Project: Victoria Development

Site: 12433 Dillon Drive, Tecumseh, Ontario

Assumed Land Use (1): Multifamily Housing (Low-Rise) - ITE No. 220

Average Vehicle Trip Ends vs.: Dwelling Units

ITE Trip Generation Data collected on a: Weekday

AM Peak Hour: = Average Rate

| | |
|----|------------|
| 23 | % Entering |
| 77 | % Exiting |

PM Peak Hour: = Average Rate

| | |
|----|------------|
| 63 | % Entering |
| 37 | % Exiting |

| Assumed Land Use (1): Multifamily Housing (Low-Rise) - ITE No. 220 | | | | |
|--|--------------|-----------------|----------------|---------------|
| | No. of Units | Trips Generated | Trips Entering | Trips Exiting |
| AM Peak | 63 | 29 | 7 | 22 |
| PM Peak | 63 | 35 | 22 | 13 |

| Total Trips | | |
|-------------|----------------|---------------|
| | Trips Entering | Trips Exiting |
| AM Peak | 7 | 22 |
| PM Peak | 22 | 13 |

Appendix C

TRAFFIC PROJECTION FIGURES

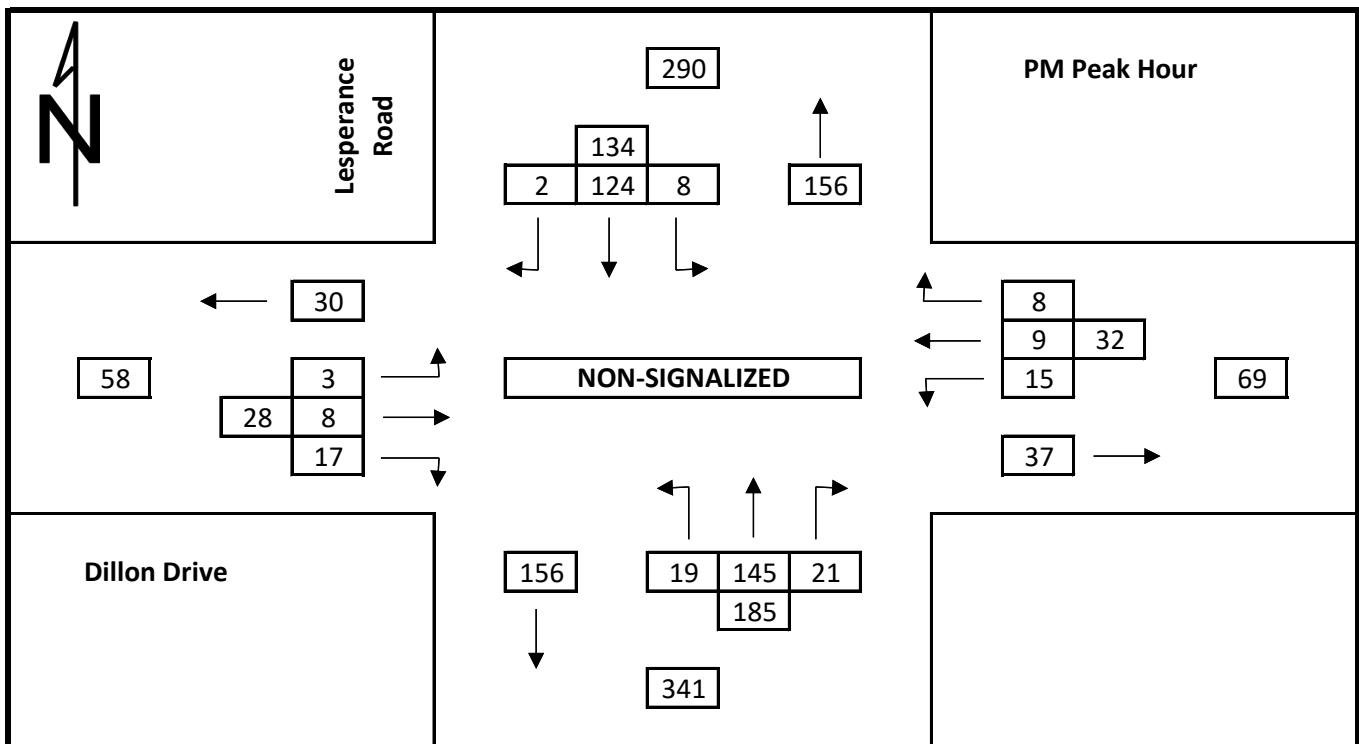
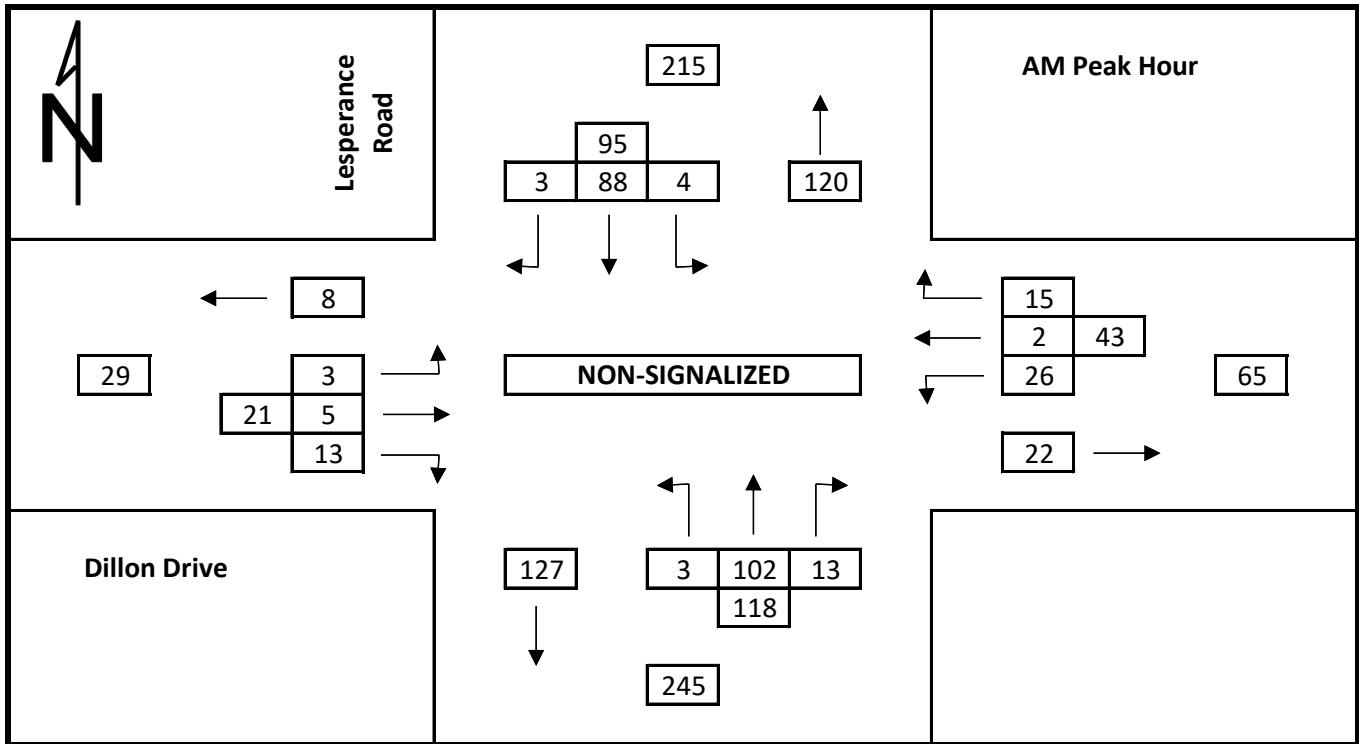
Dillon Drive at Lesperance Road

Dillon Drive at St. Pierre Street

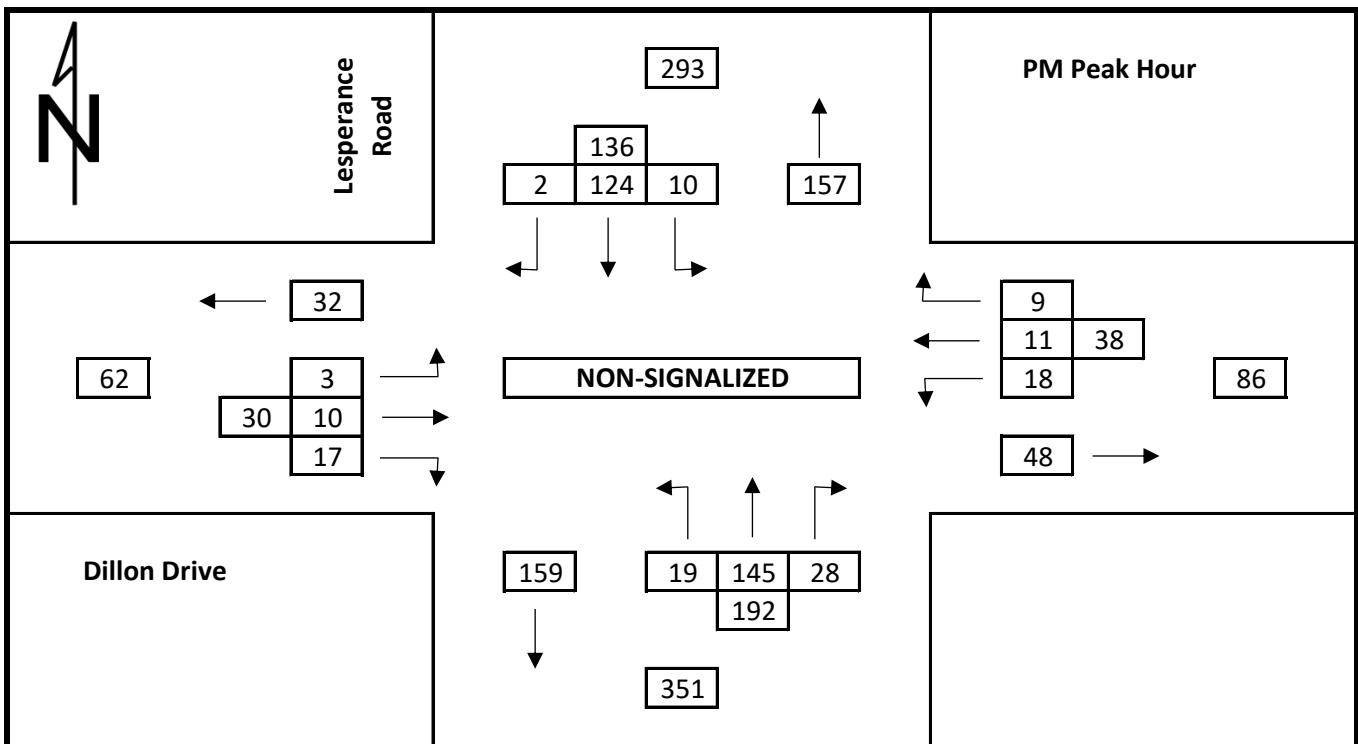
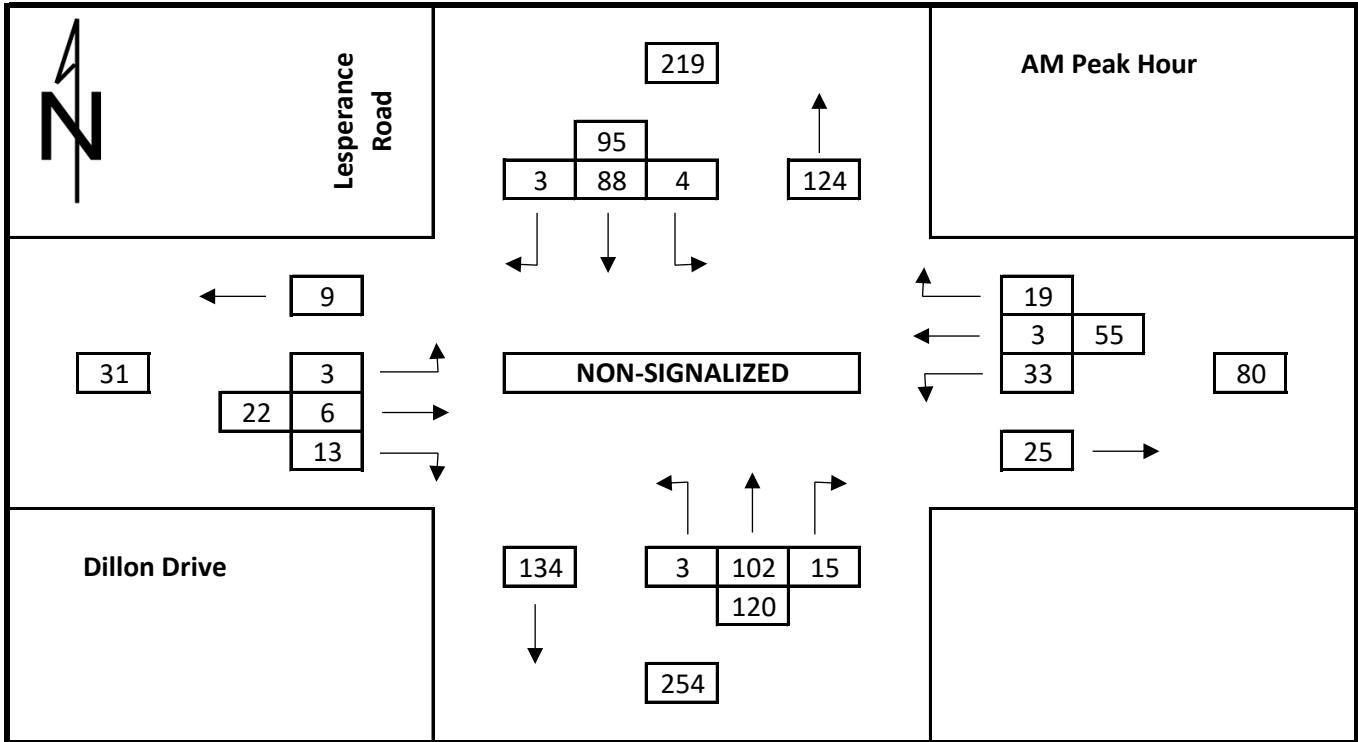
Dillon Drive at Site Access

Dillon Drive at Lacasse Boulevard

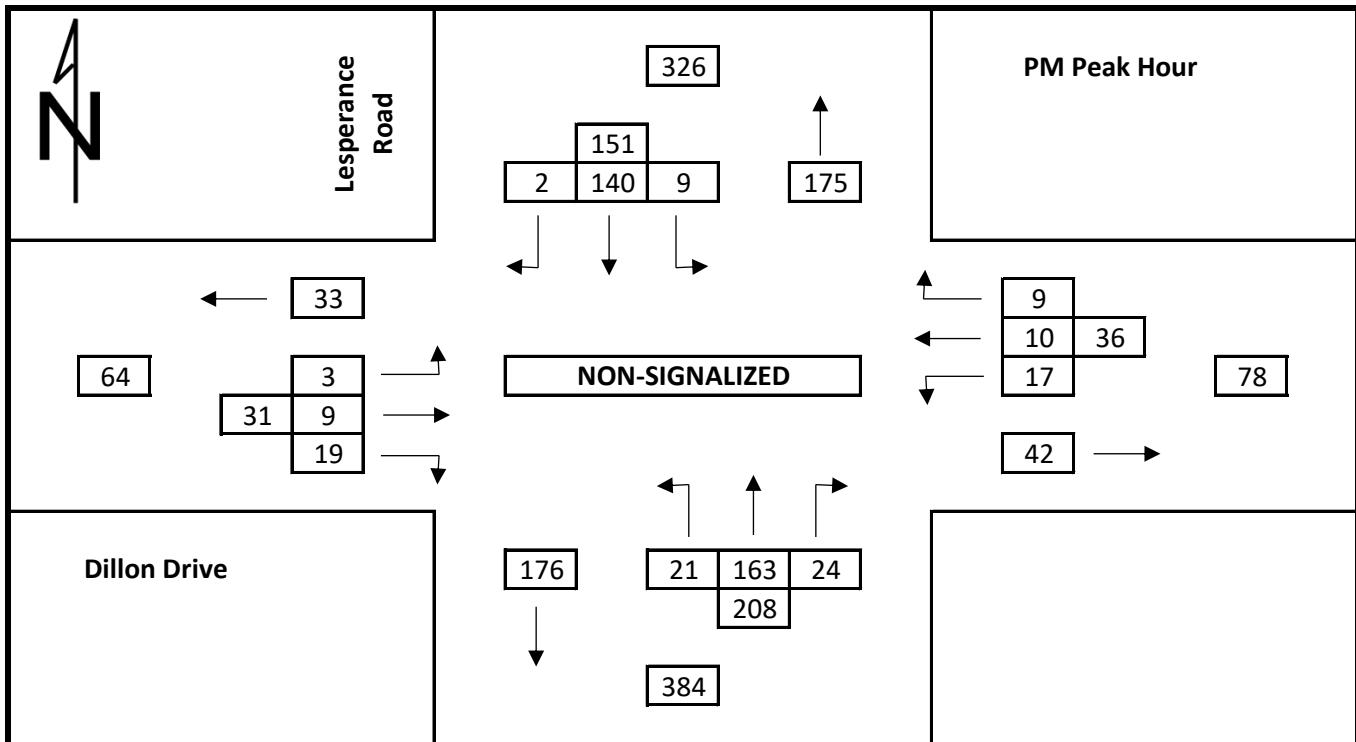
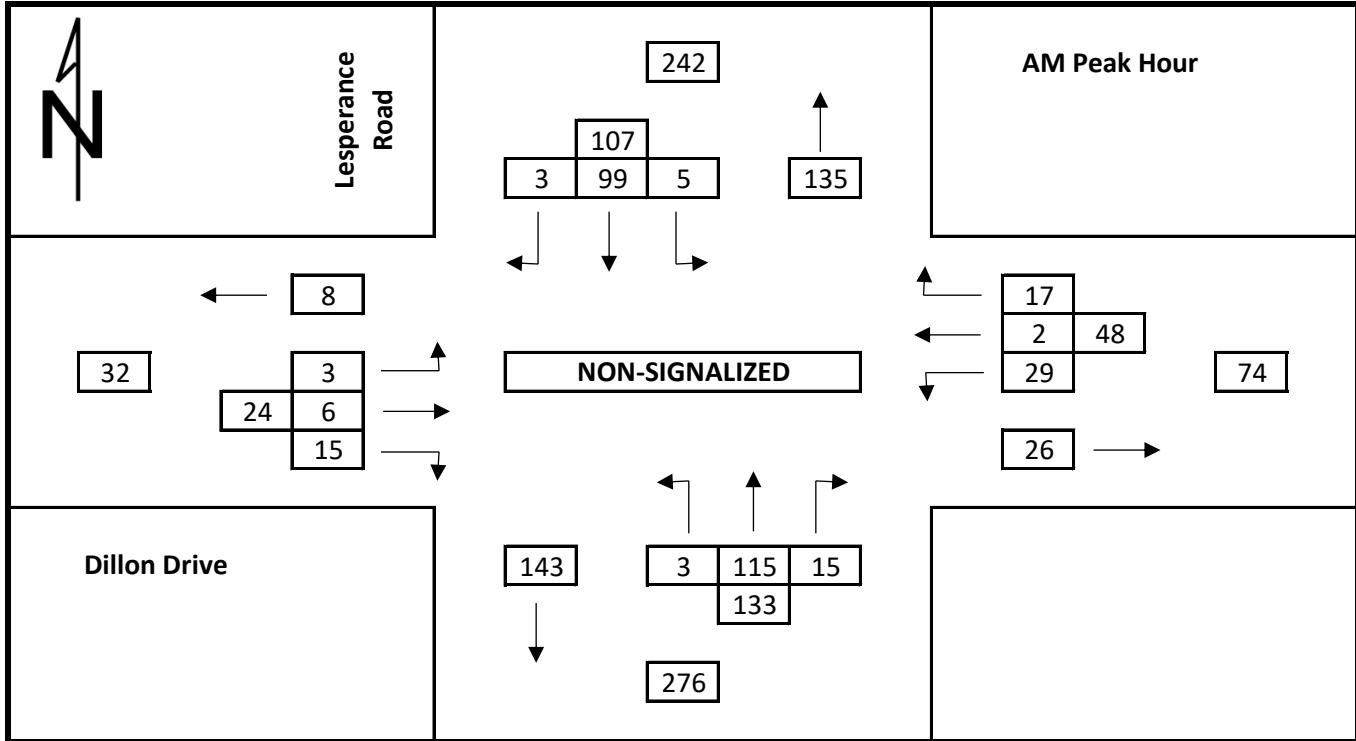
Existing Traffic Counts
 Dillon Drive at Lesperance Road



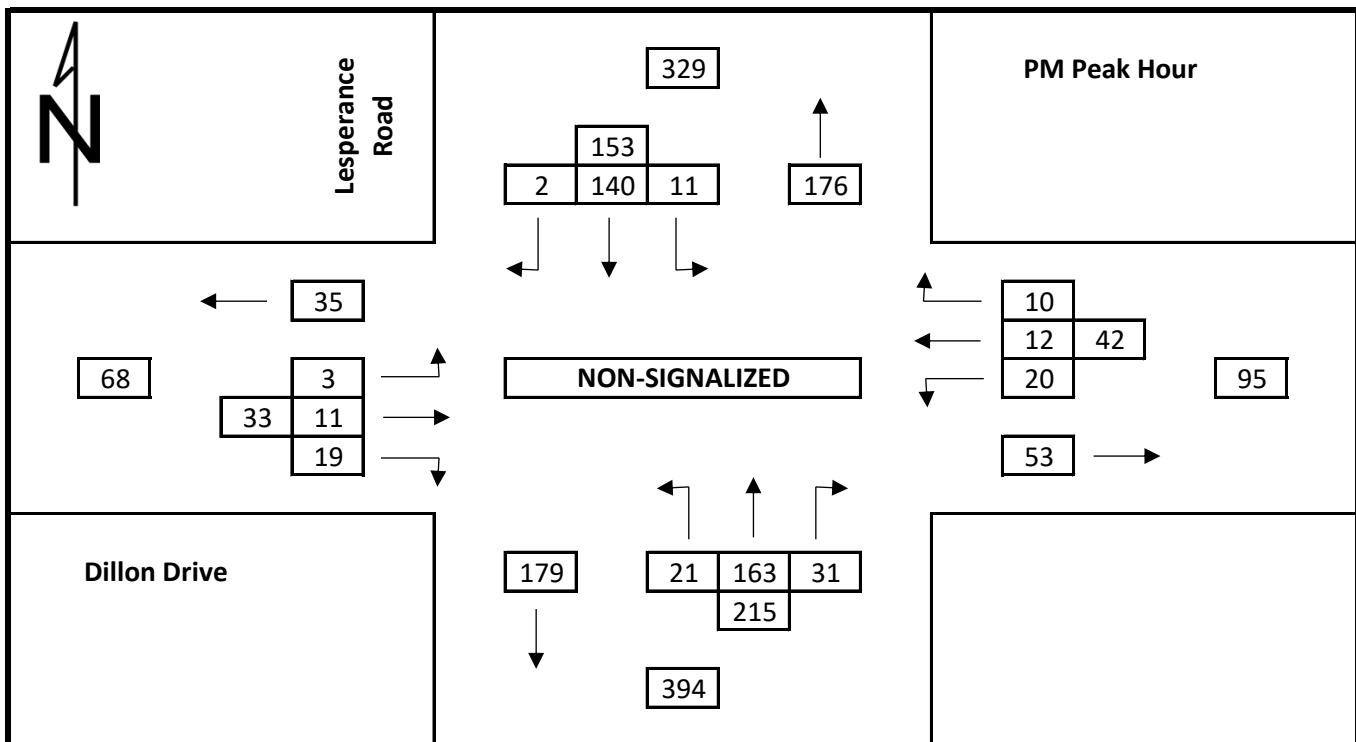
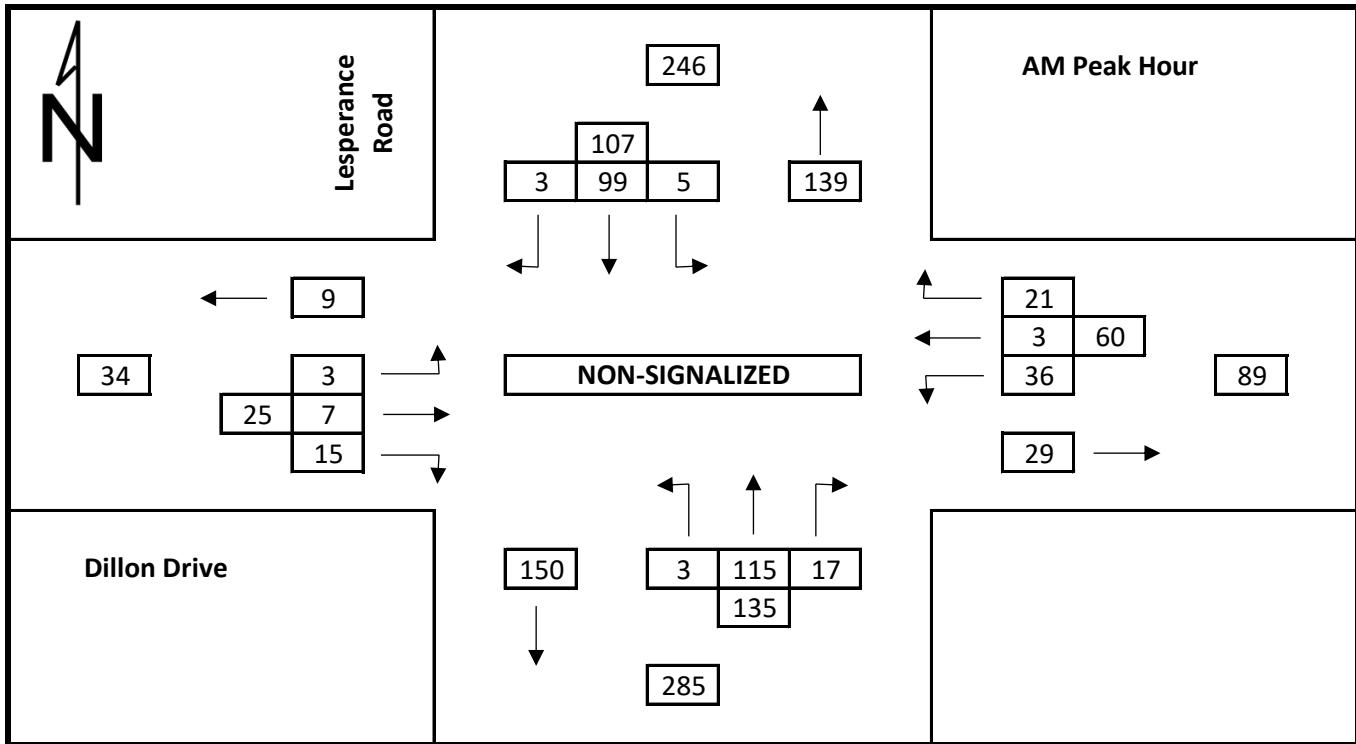
Existing + Site Generated Traffic
Dillon Drive at Lesperance Road



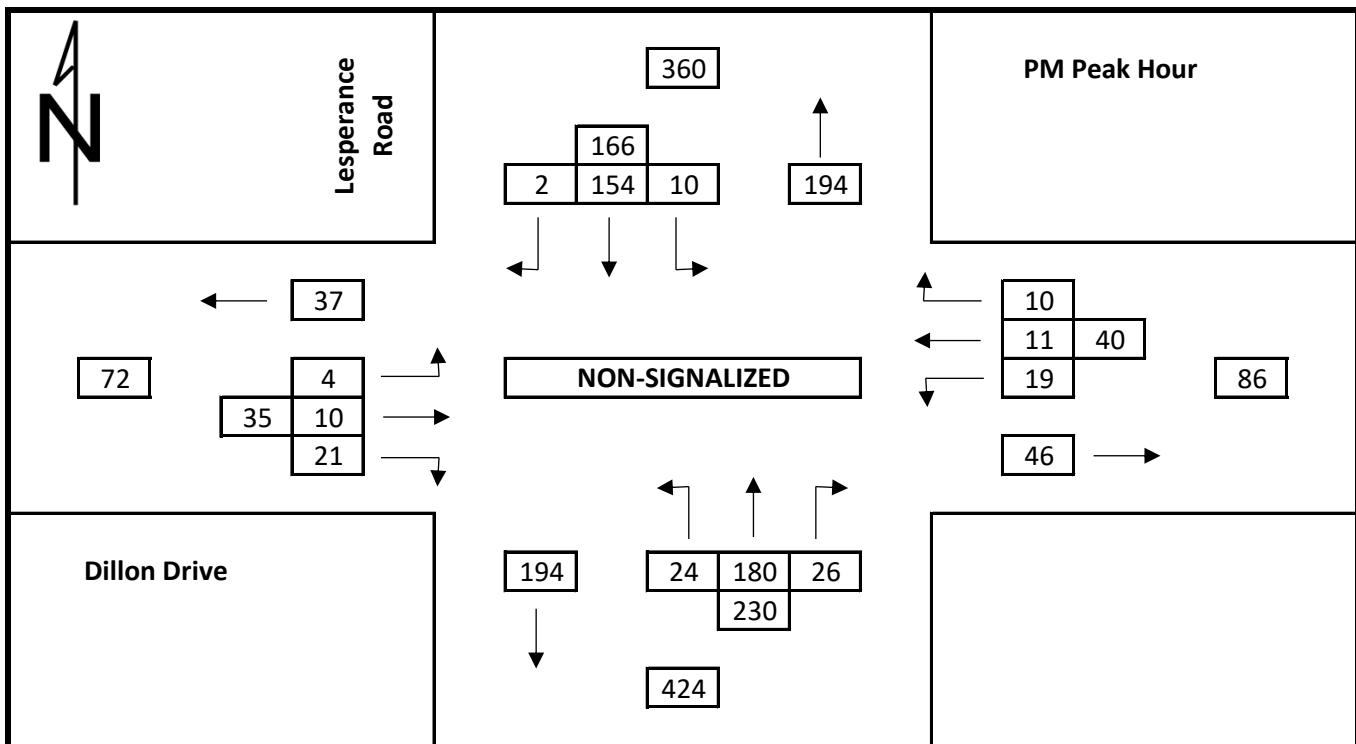
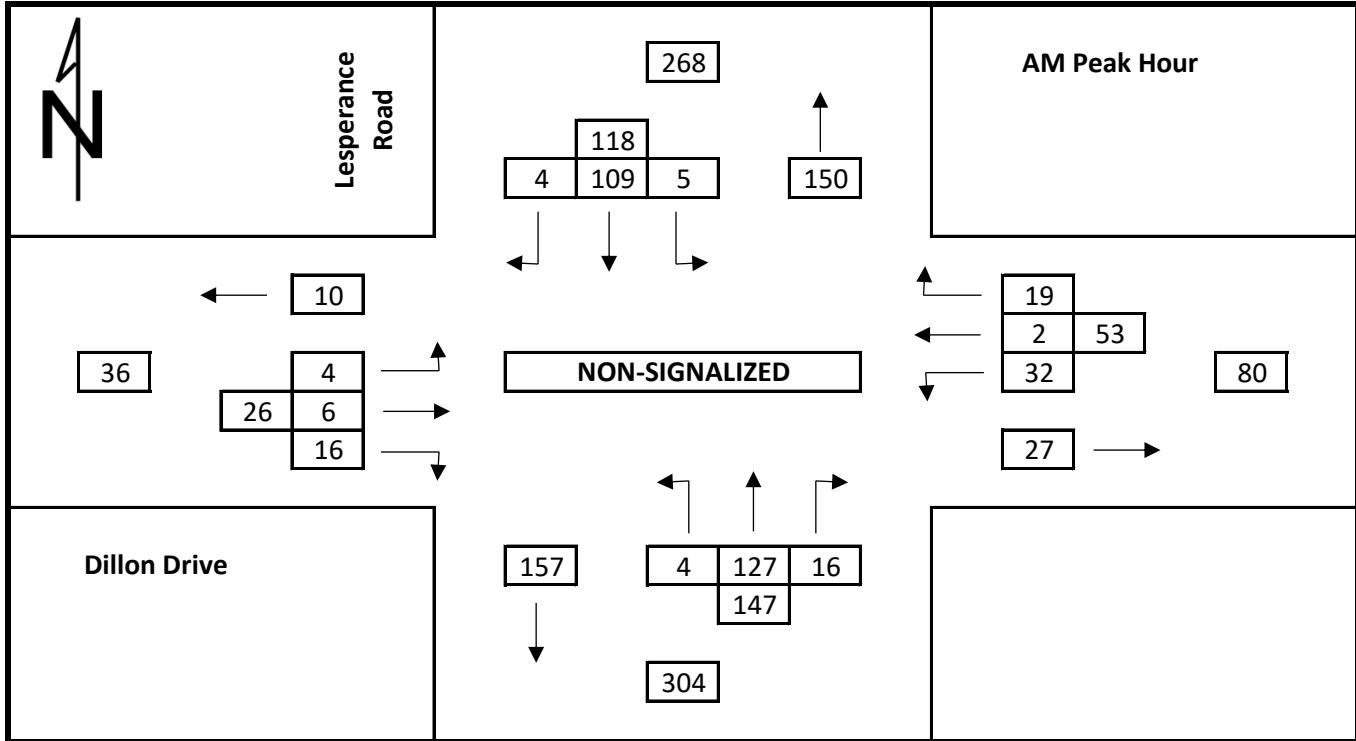
Background Traffic Year 2025
 Dillon Drive at Lesperance Road



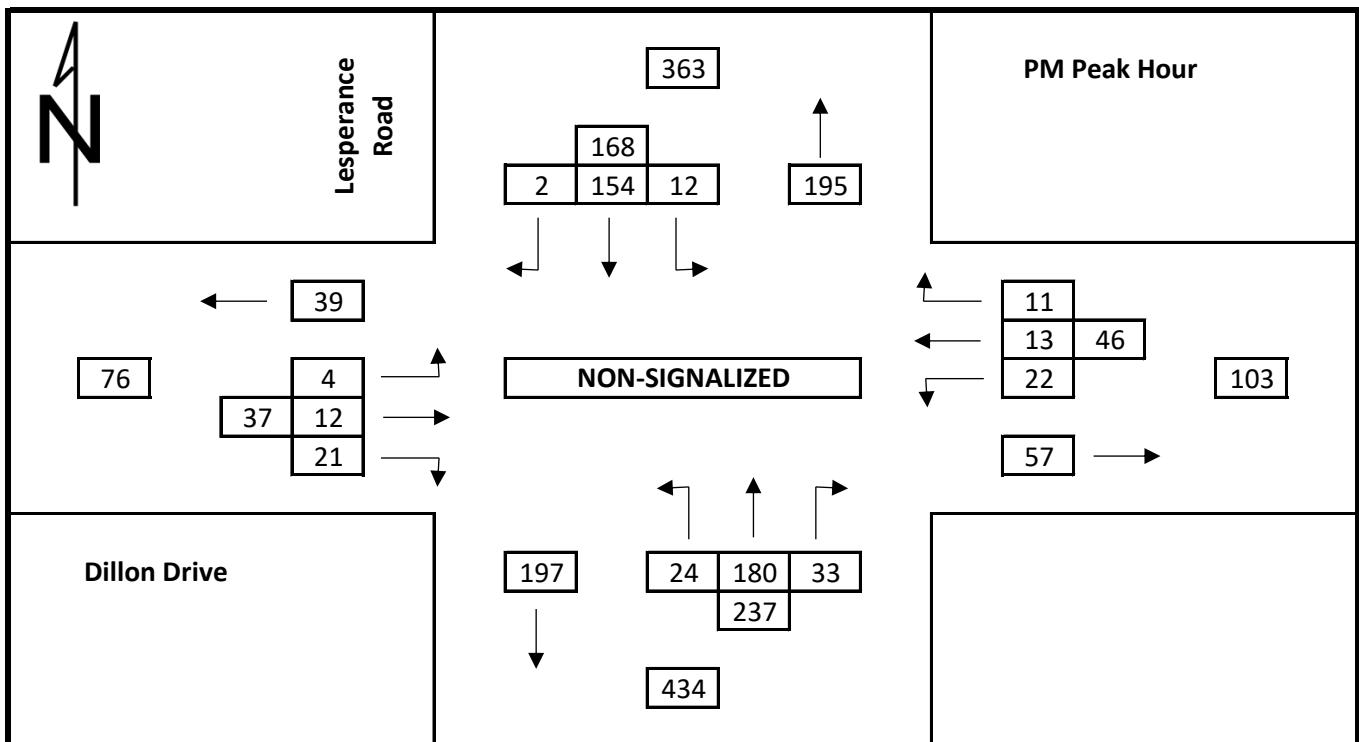
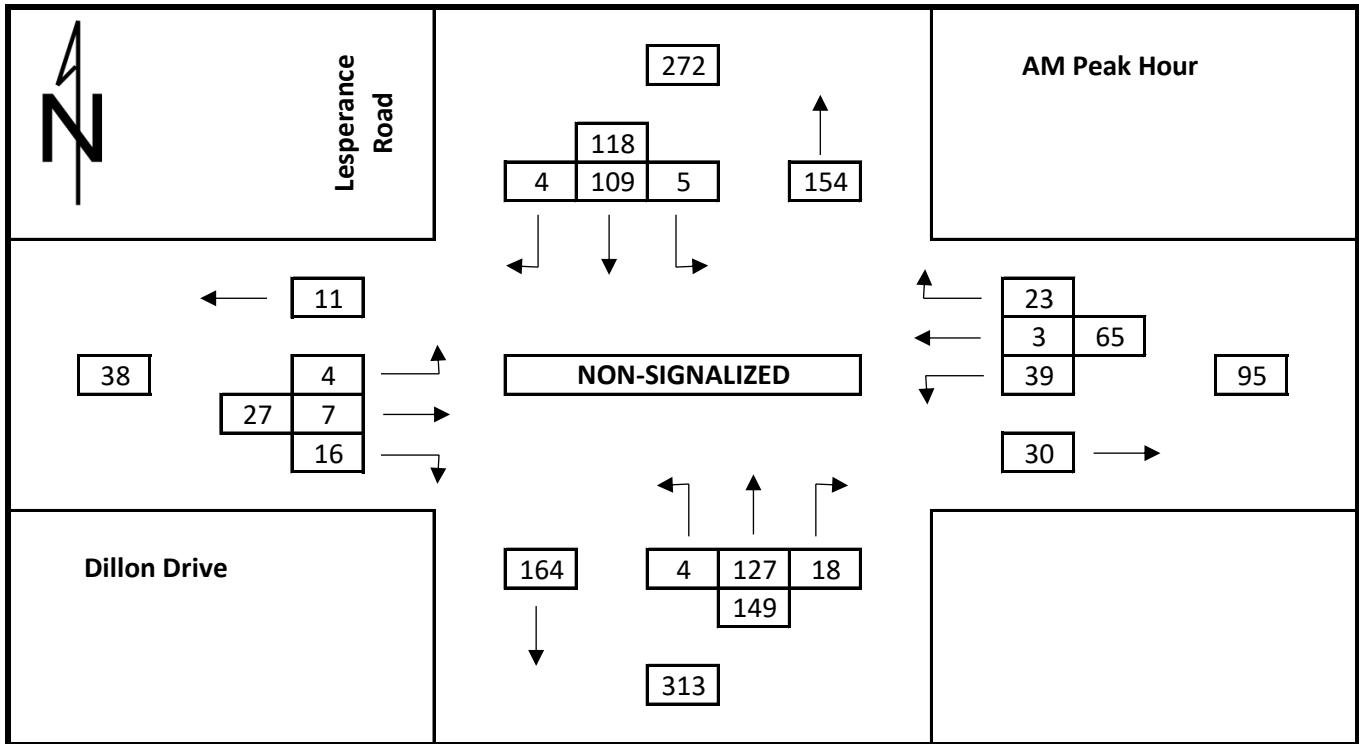
Total Traffic 2025
Dillon Drive at Lesperance Road



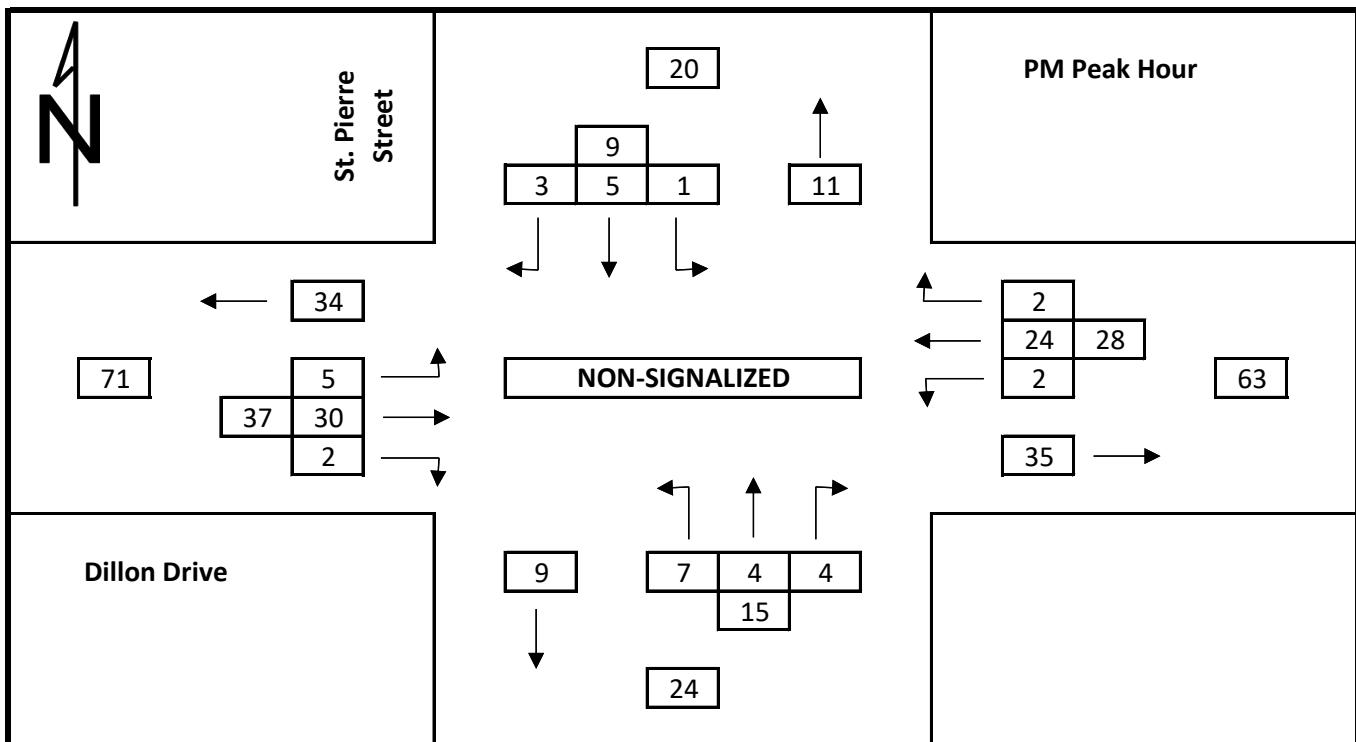
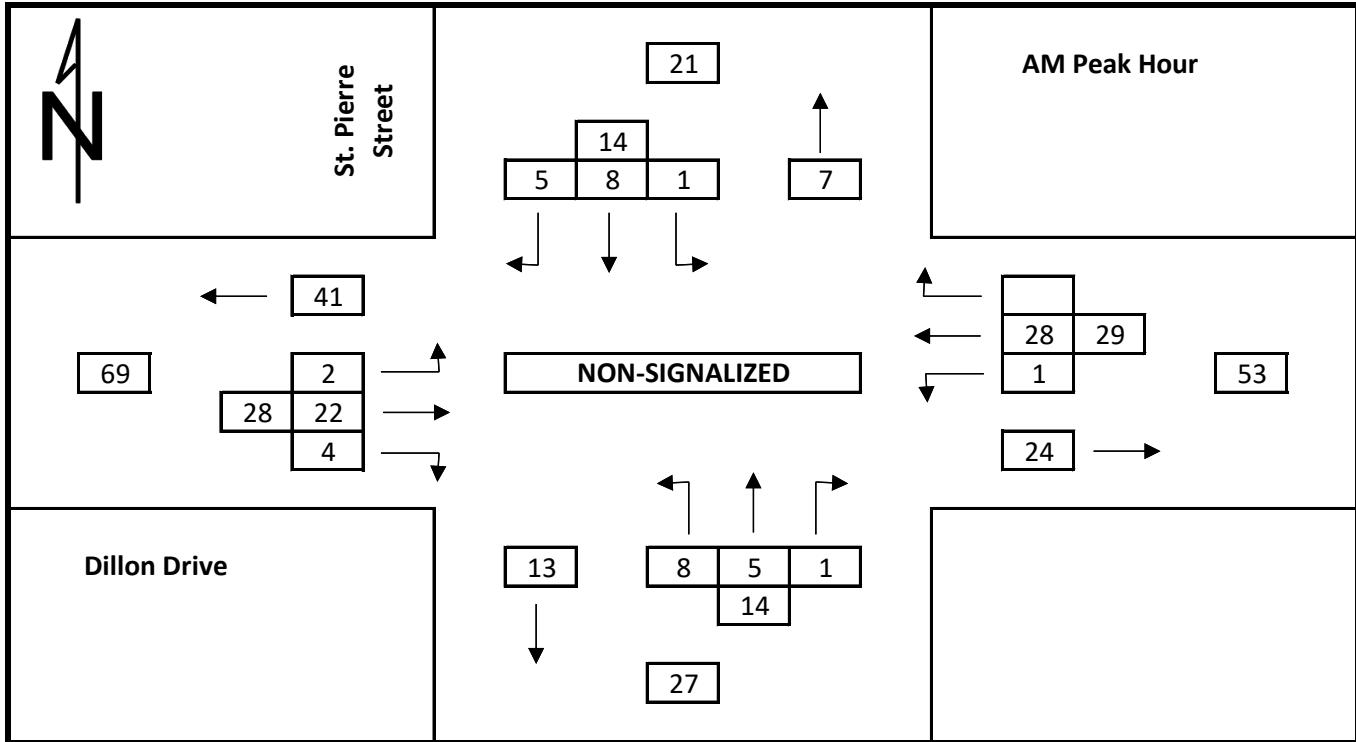
Background Traffic Year 2030
 Dillon Drive at Lesperance Road



Total Traffic 2030
Dillon Drive at Lesperance Road

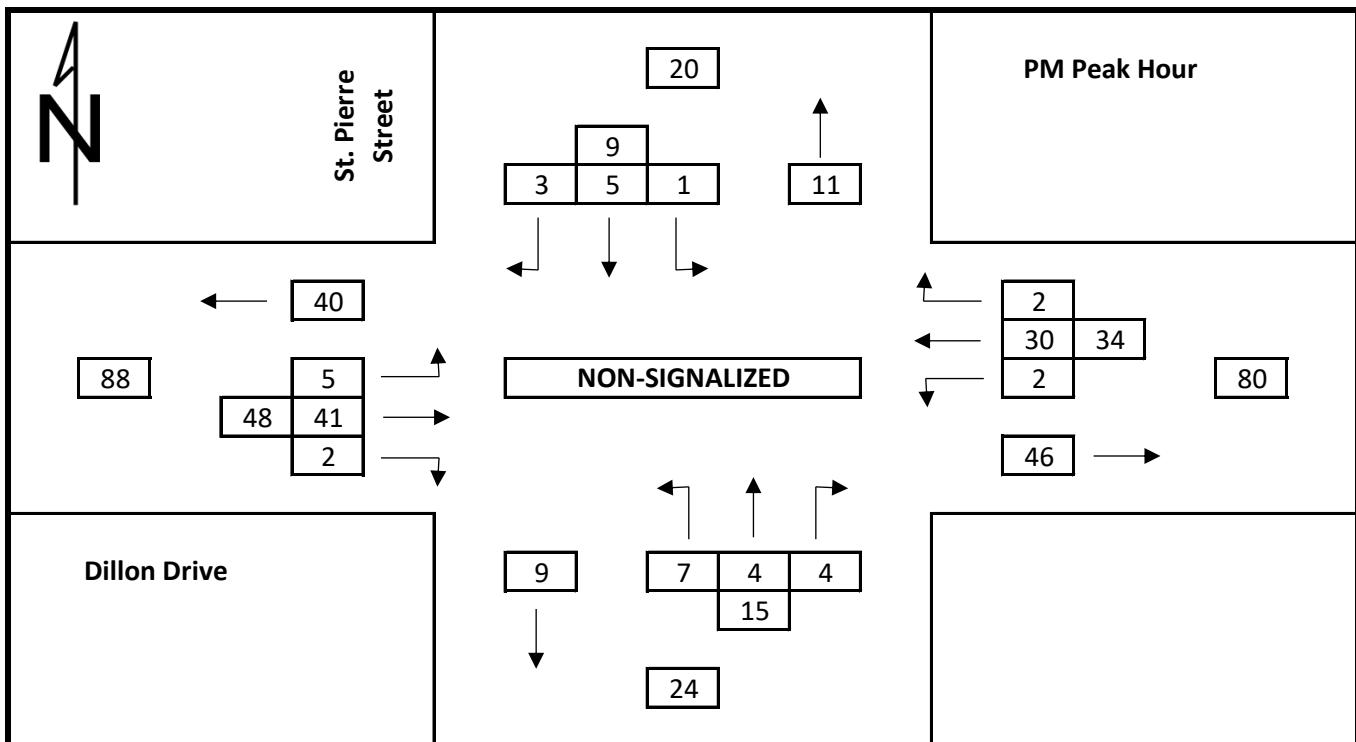
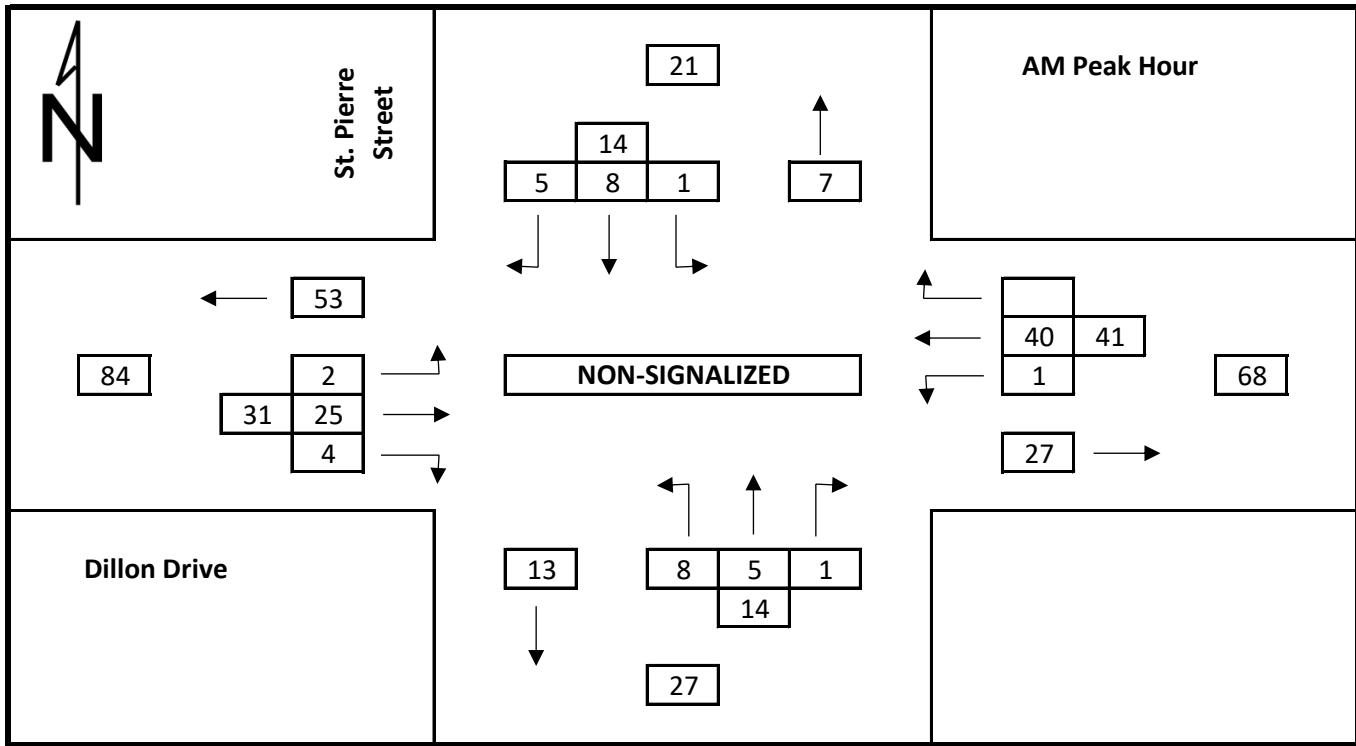


Existing Traffic Counts
Dillon Drive at St. Pierre Street

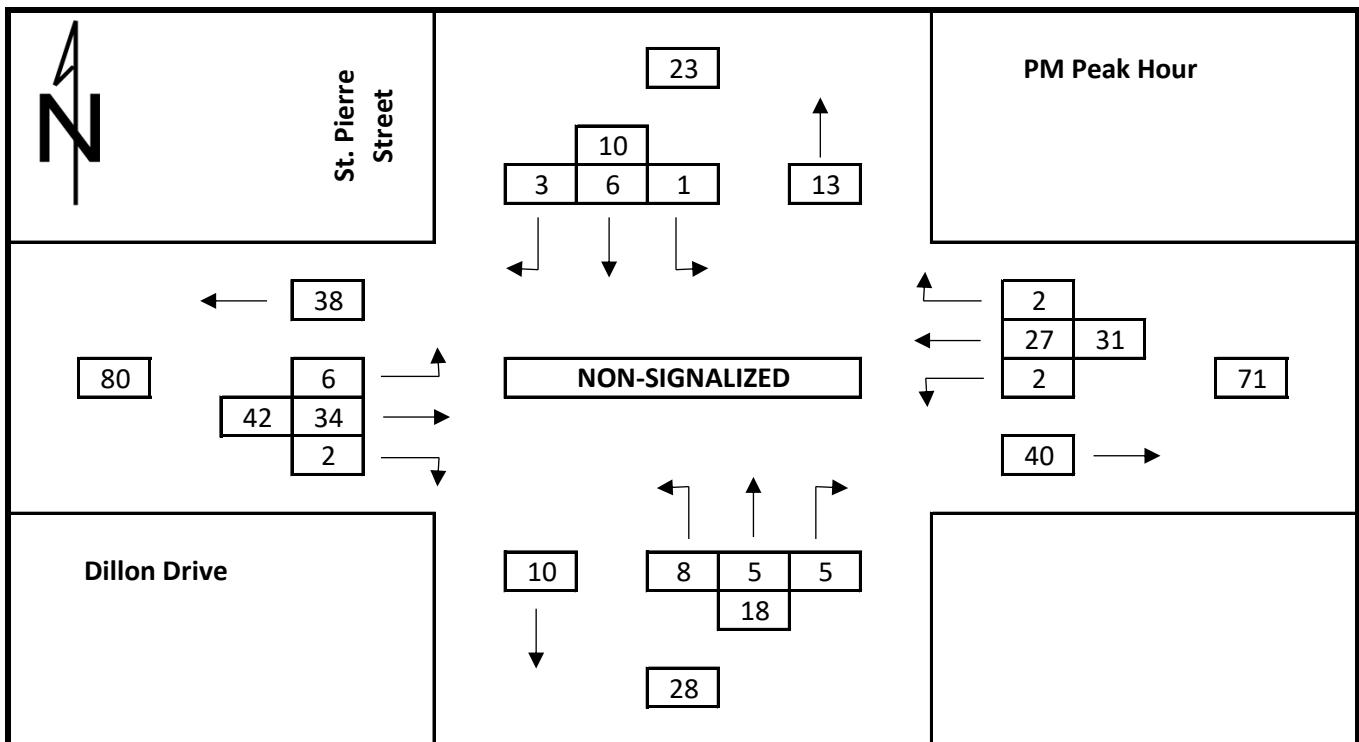
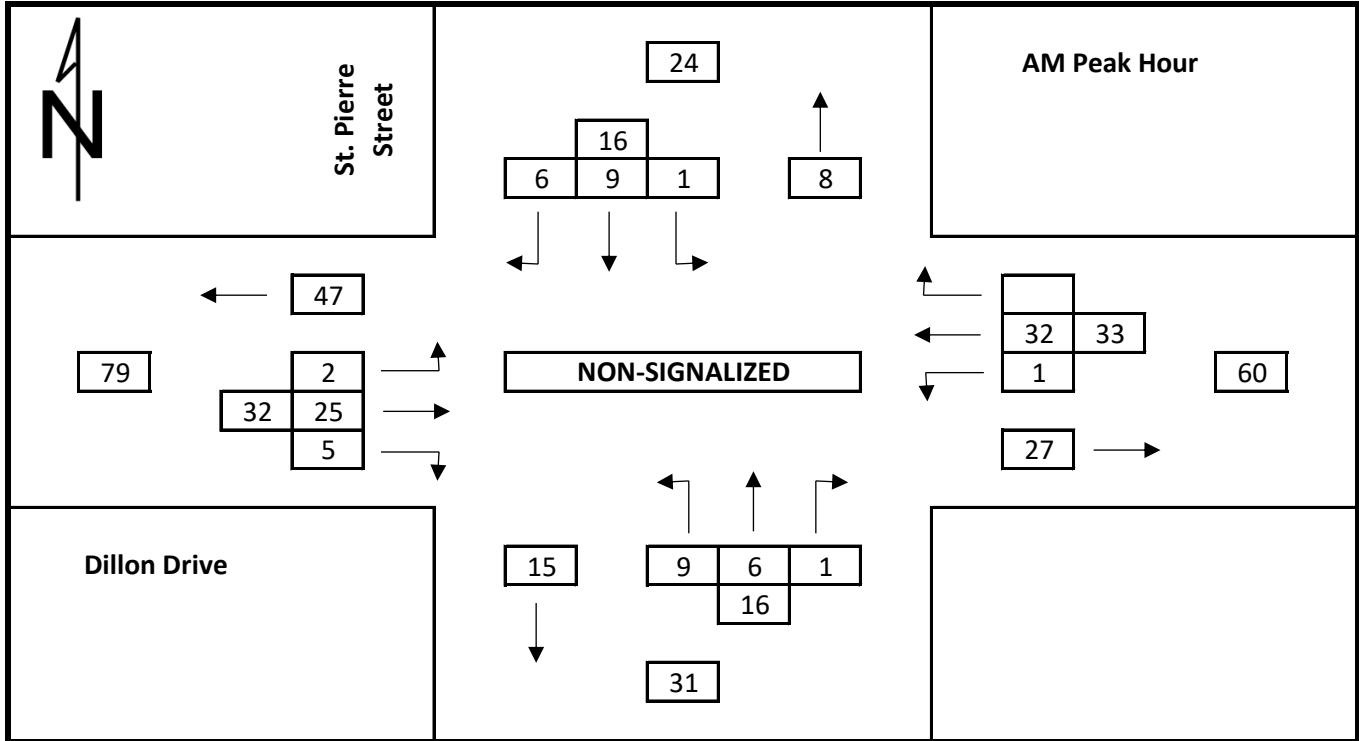


Existing + Site Generated Traffic

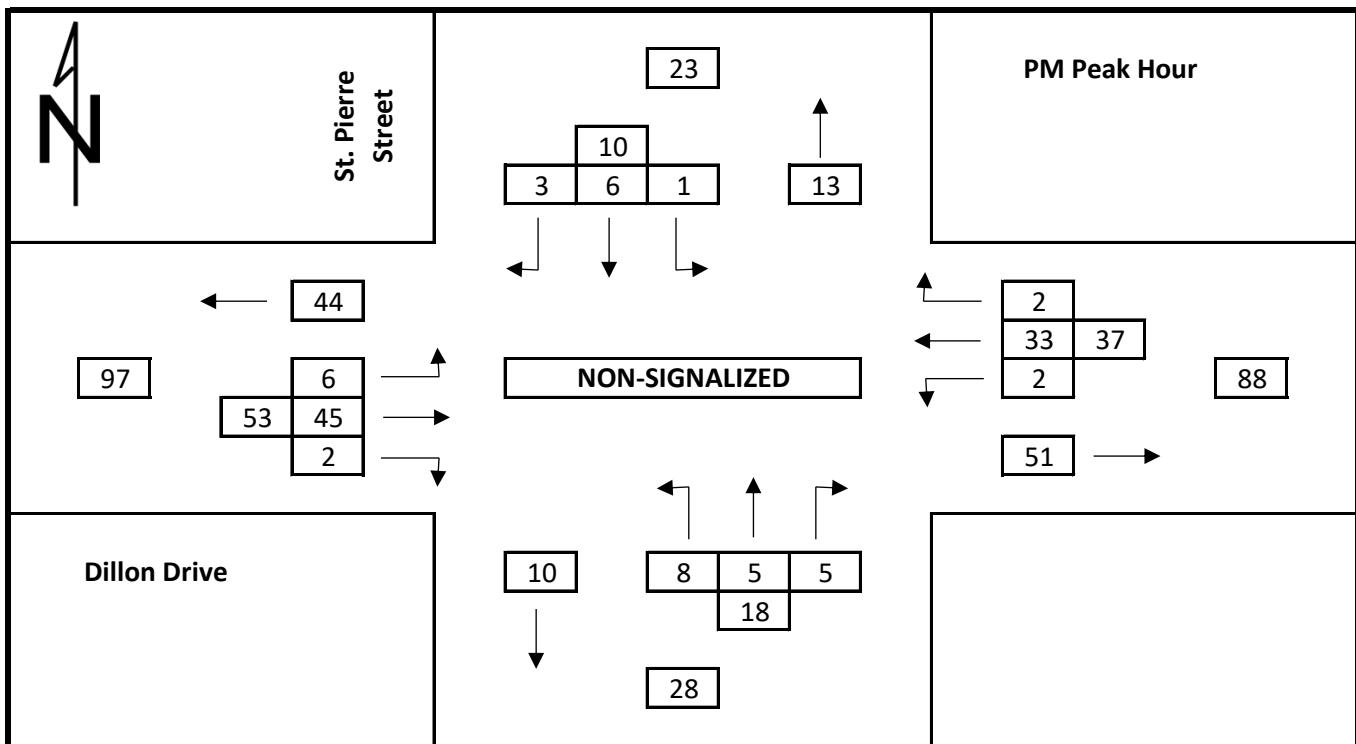
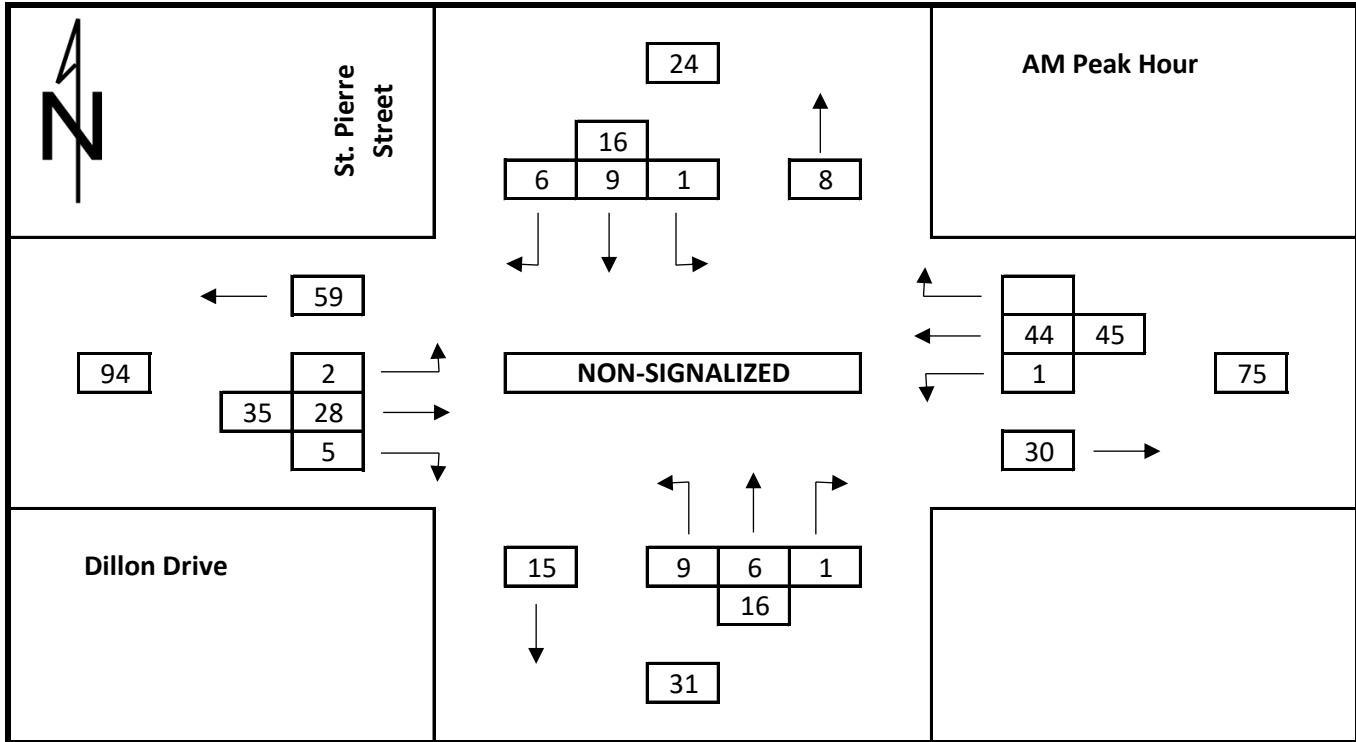
Dillon Drive at St. Pierre Street



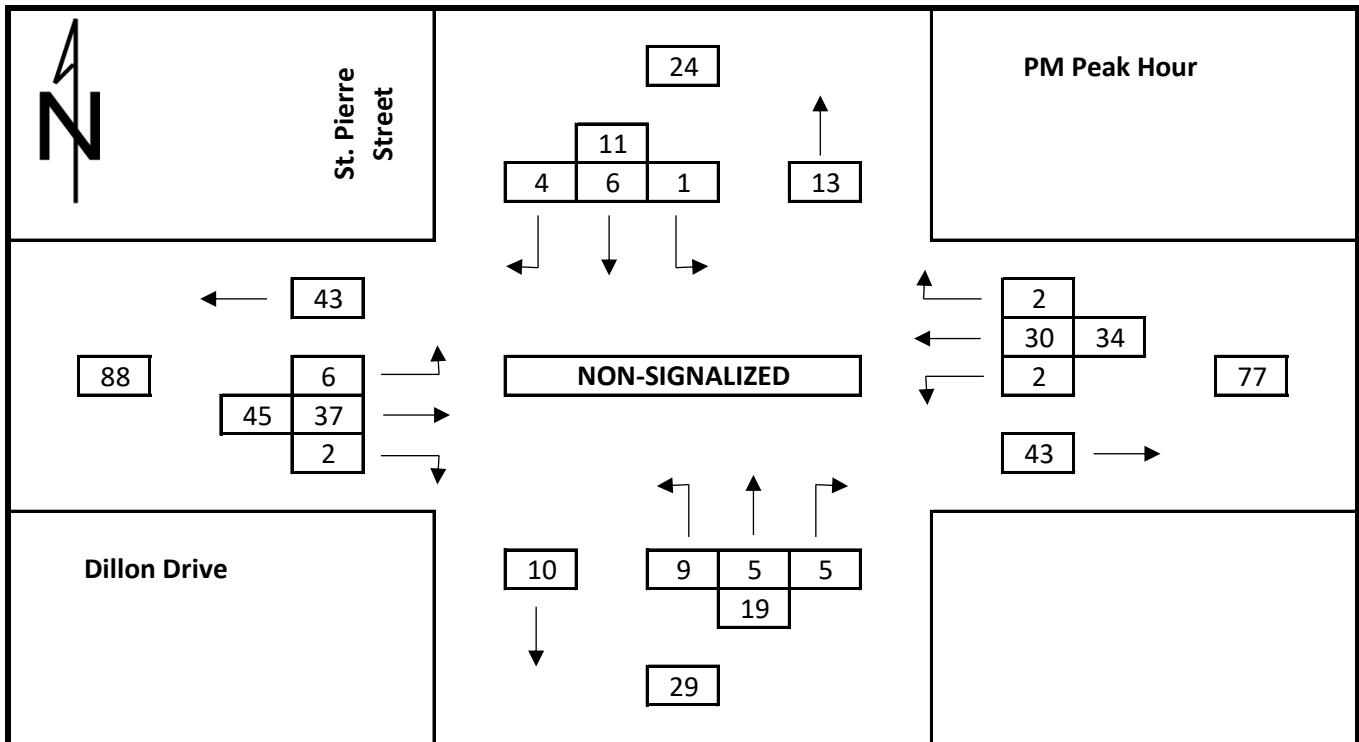
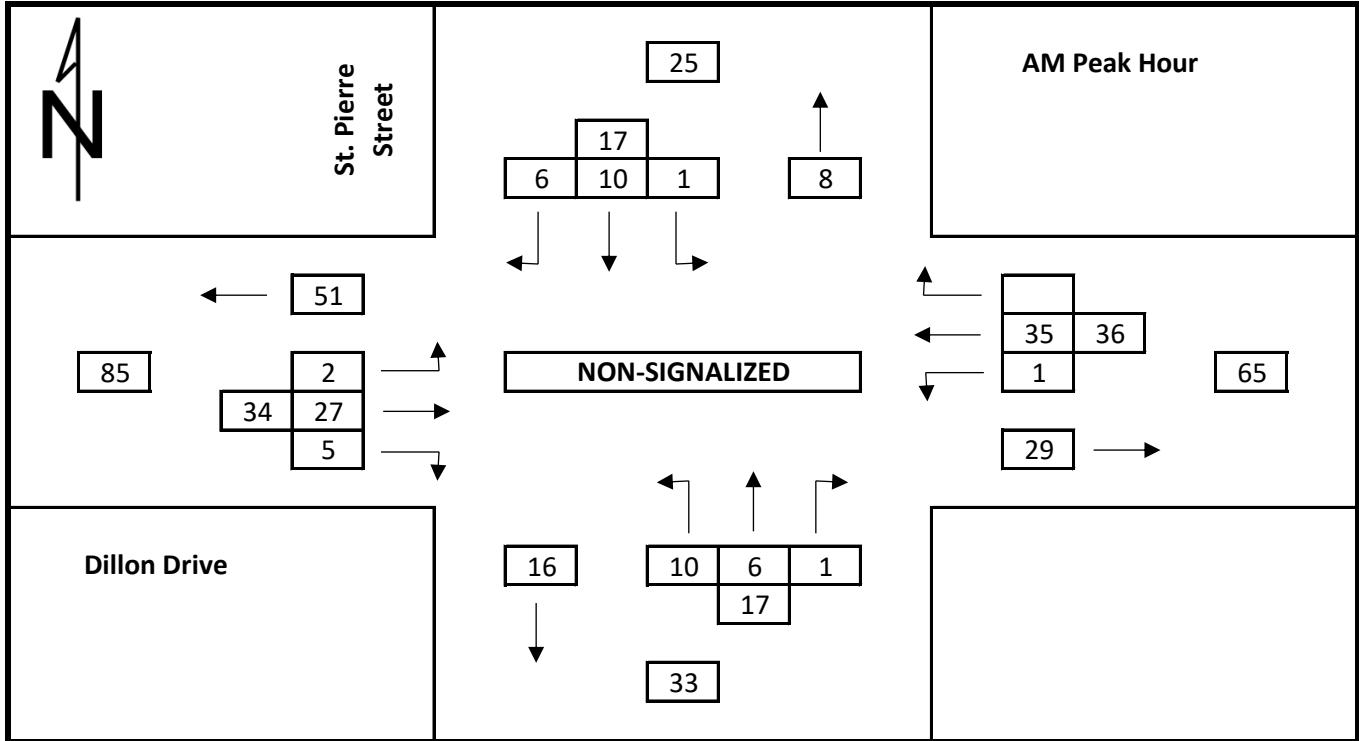
Background Traffic Year 2025
 Dillon Drive at St. Pierre Street



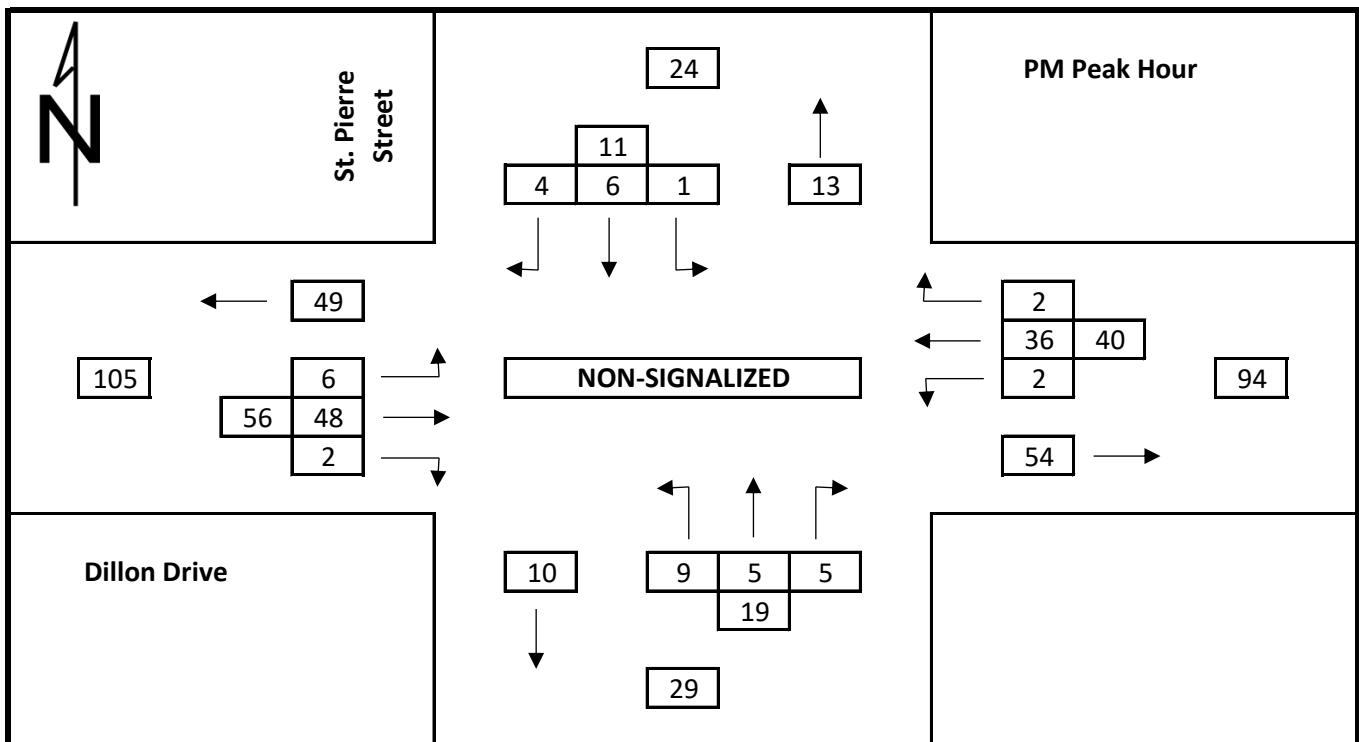
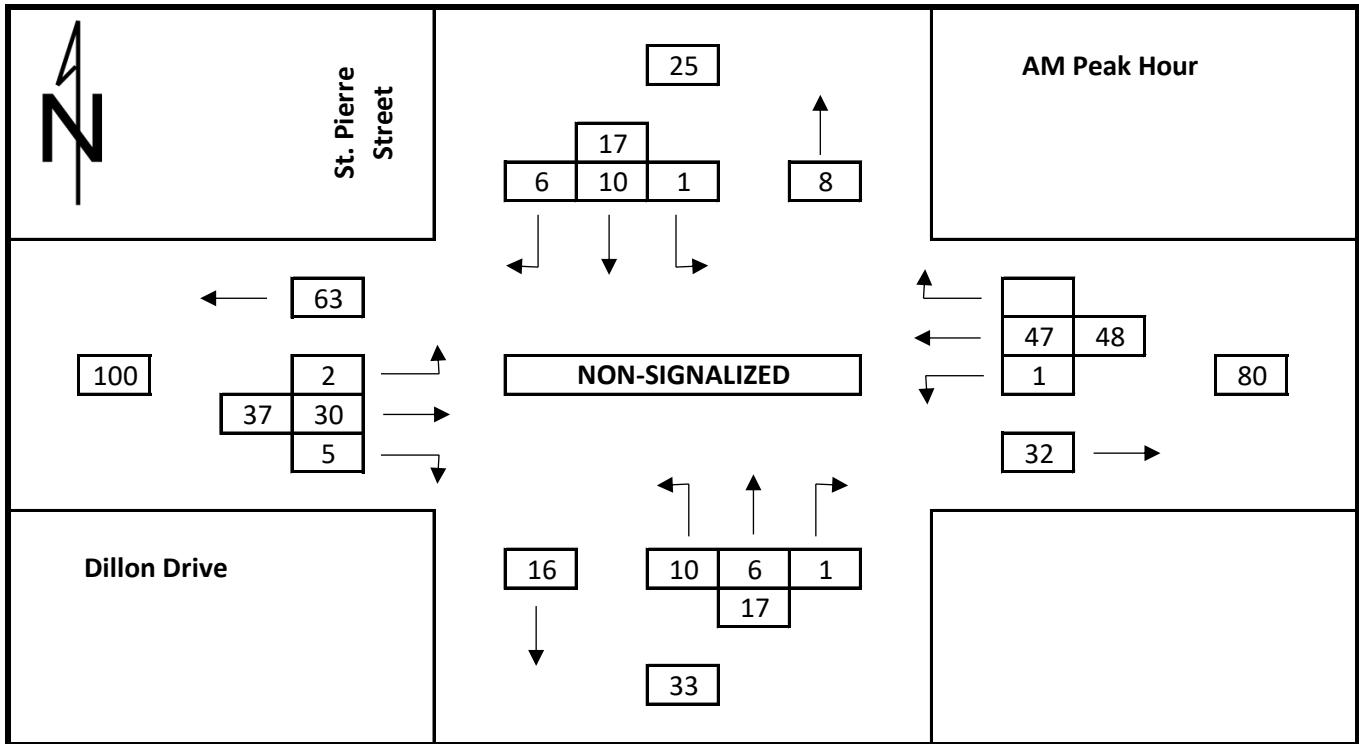
Total Traffic 2025
Dillon Drive at St. Pierre Street



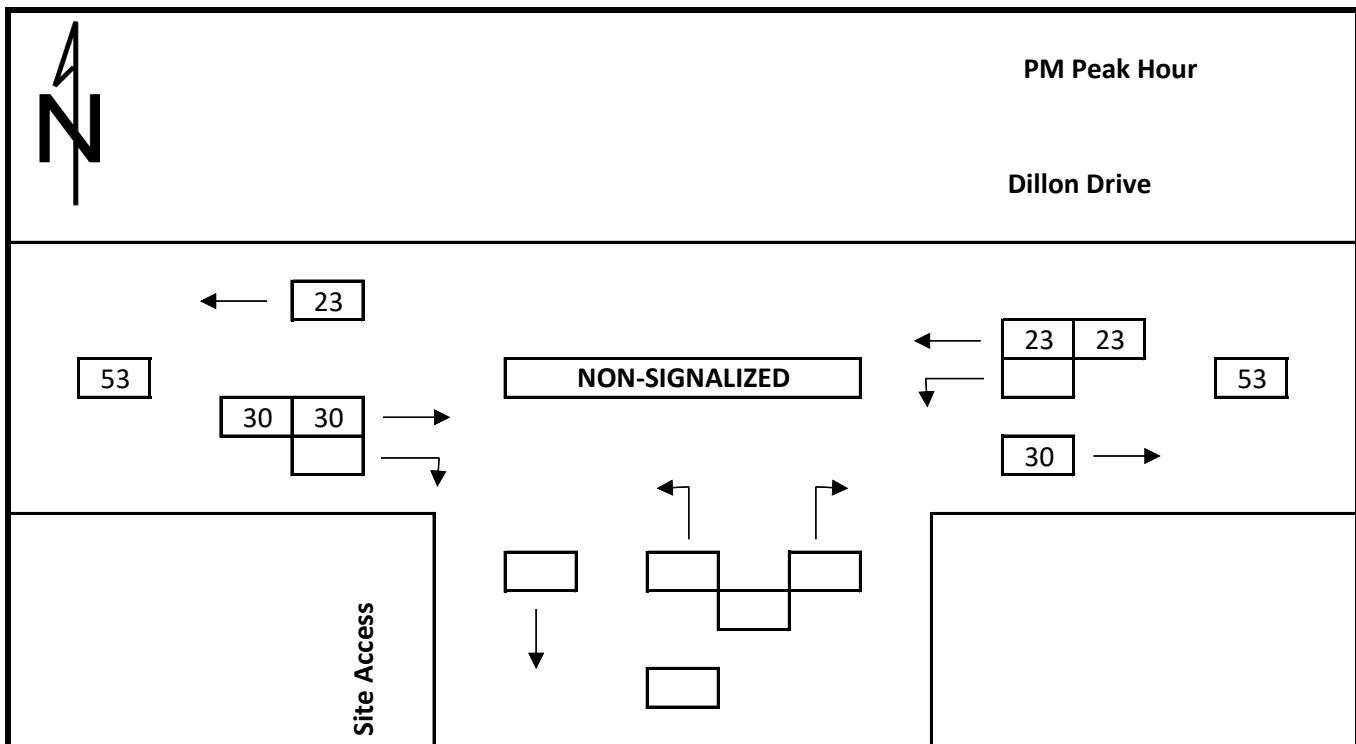
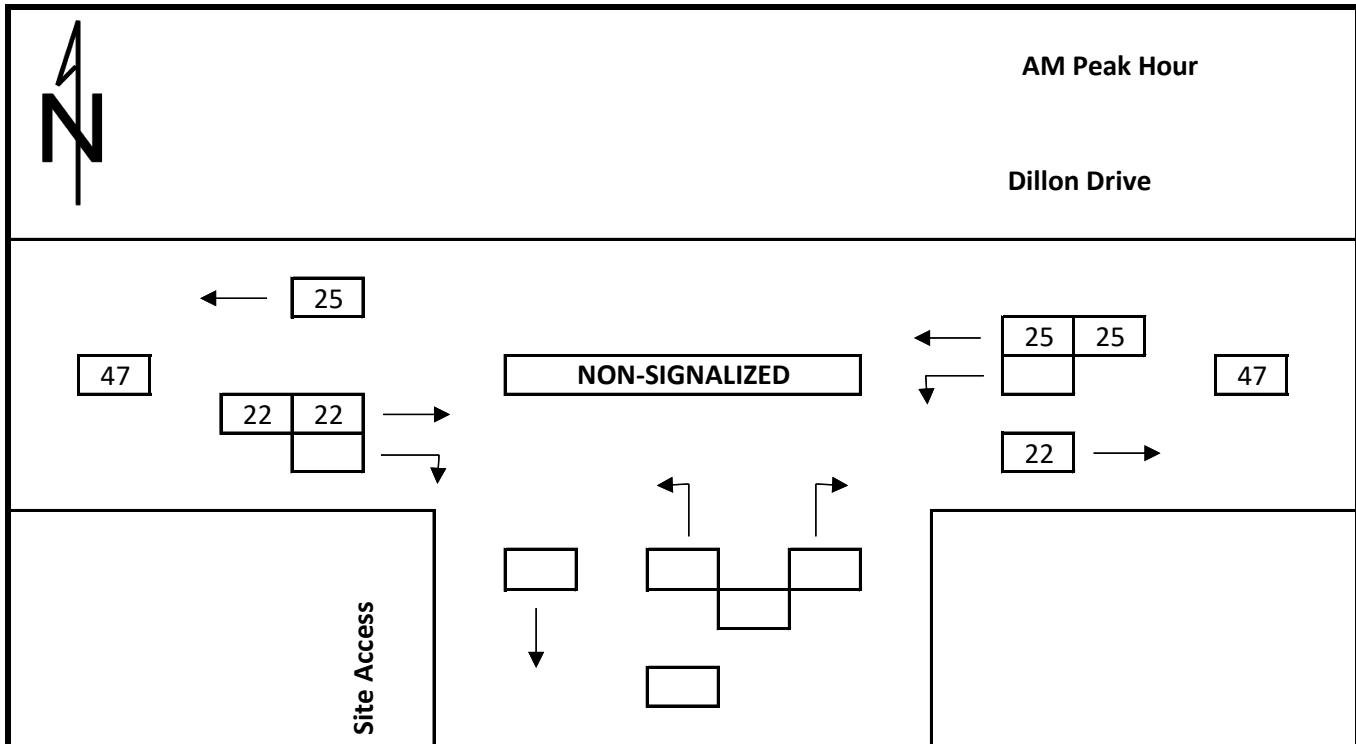
Background Traffic Year 2030
 Dillon Drive at St. Pierre Street



Total Traffic 2030
Dillon Drive at St. Pierre Street

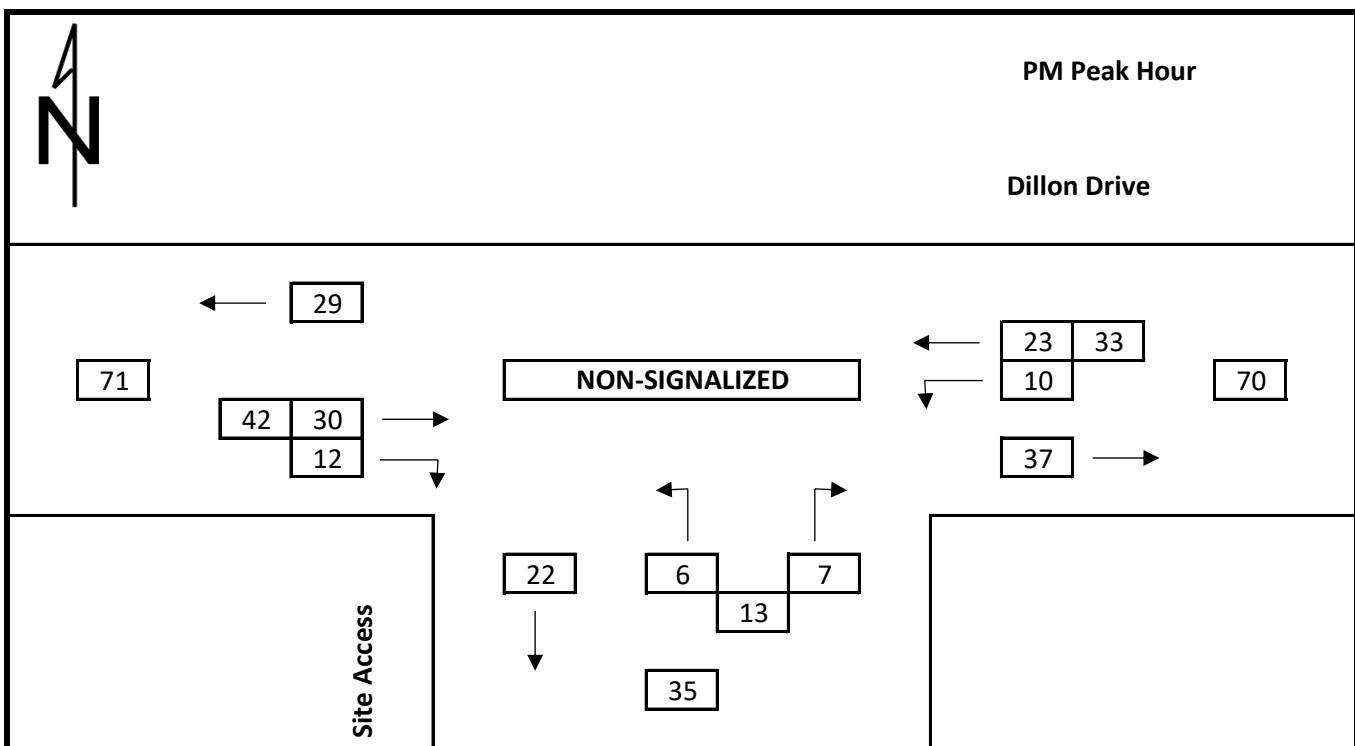
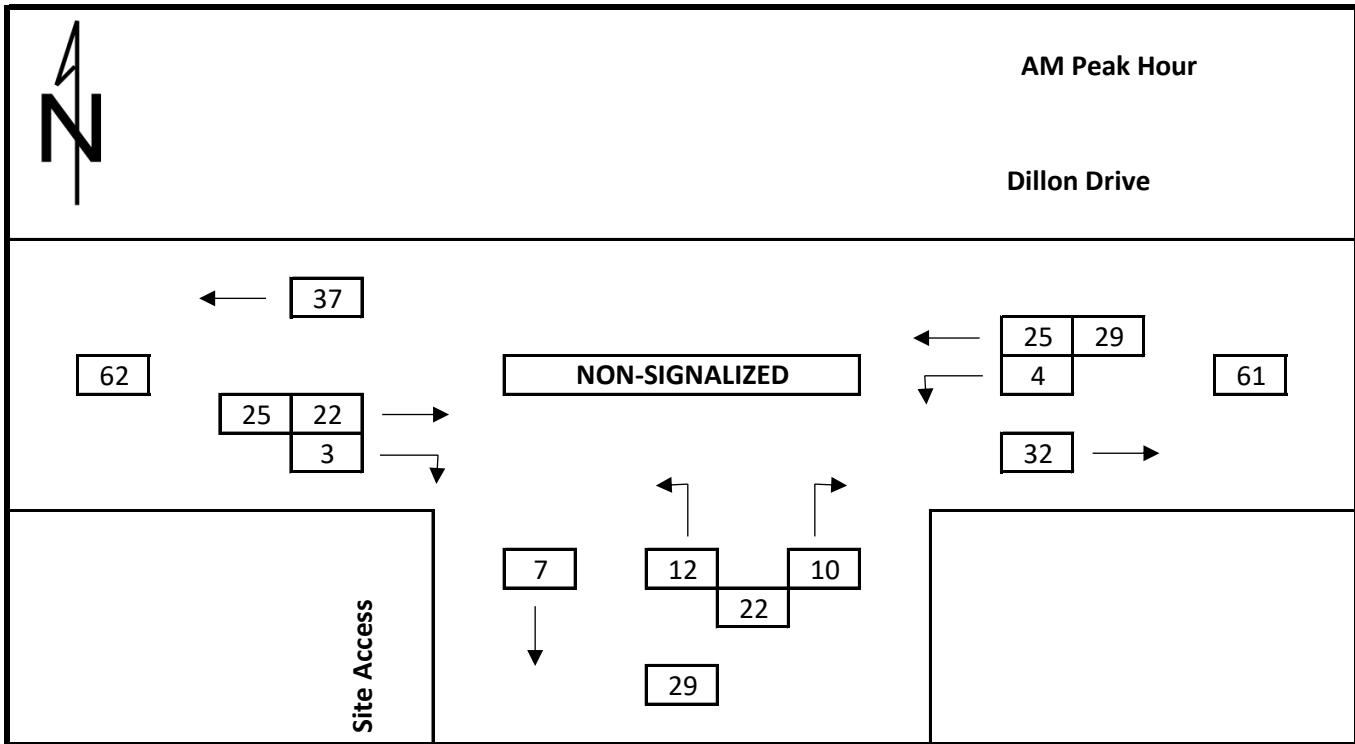


Existing Traffic Counts
Dillon Drive at Site Access



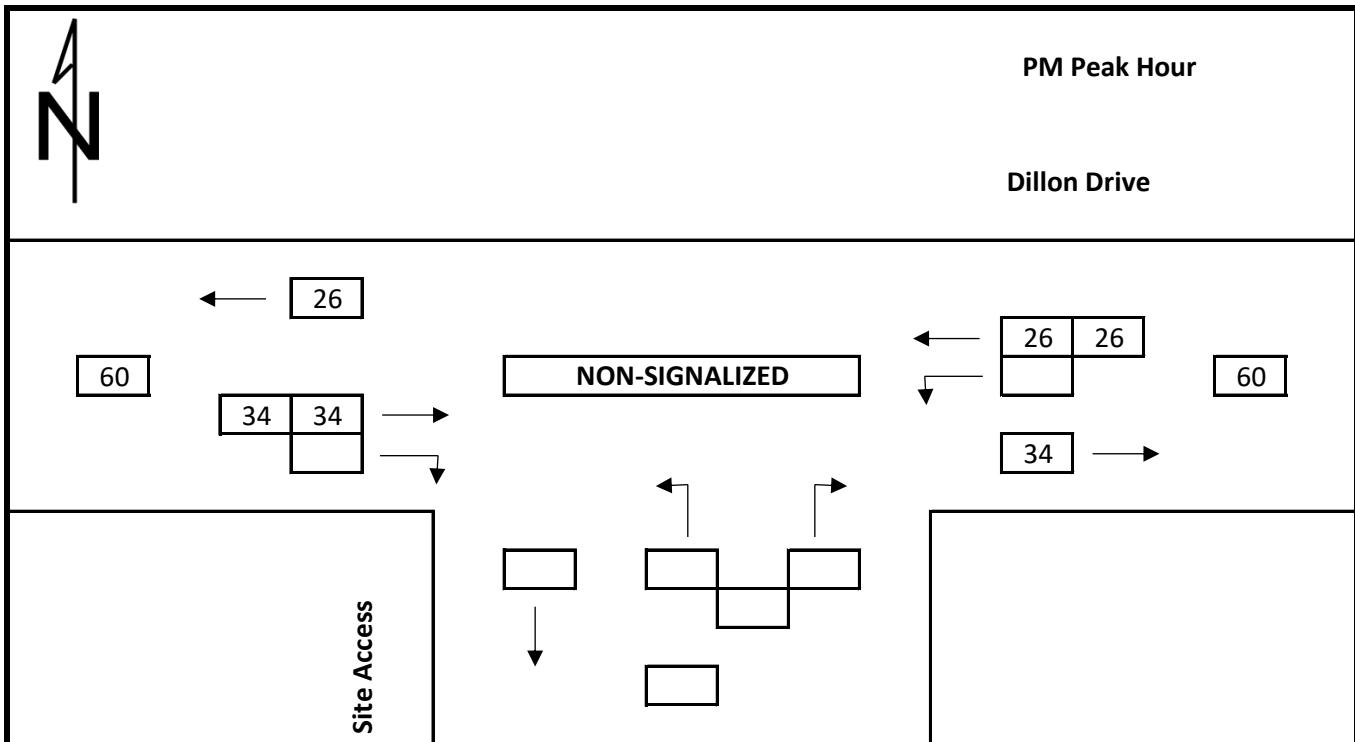
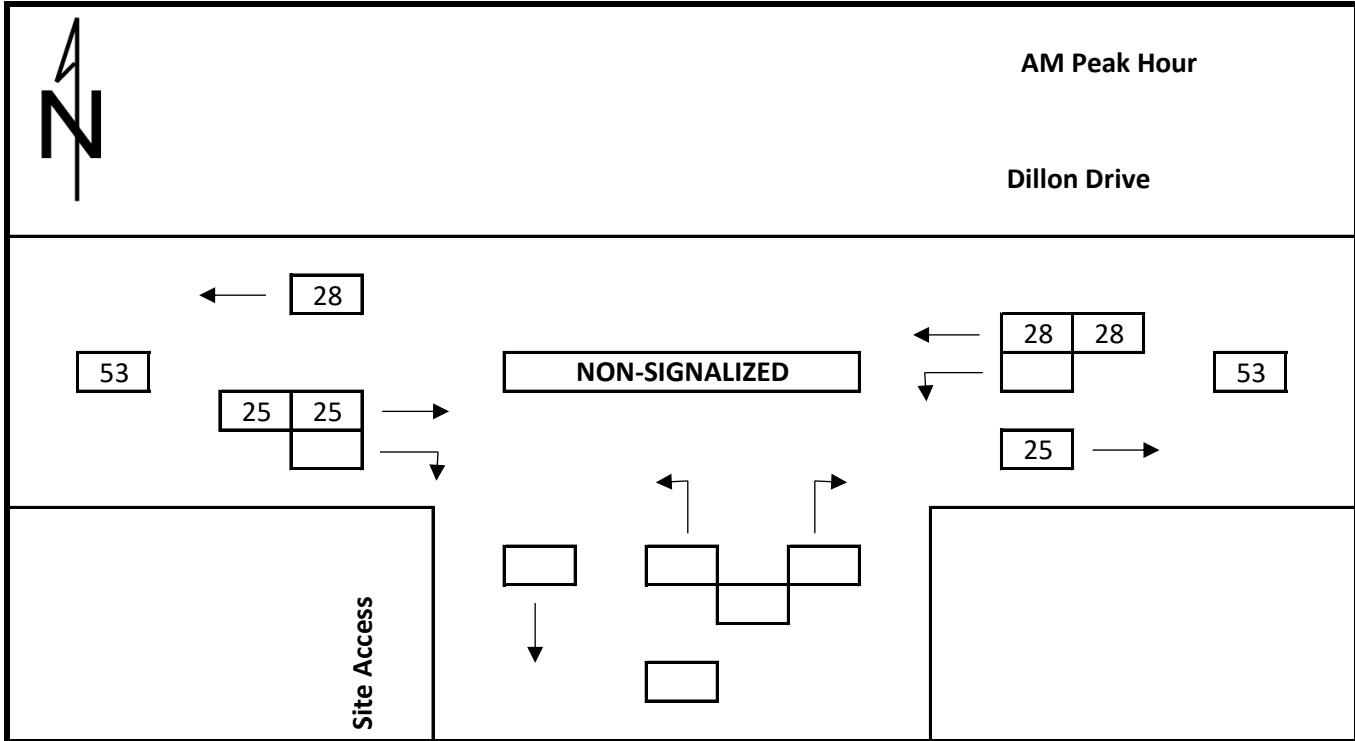
Existing + Site Generated Traffic

Dillon Drive at Site Access

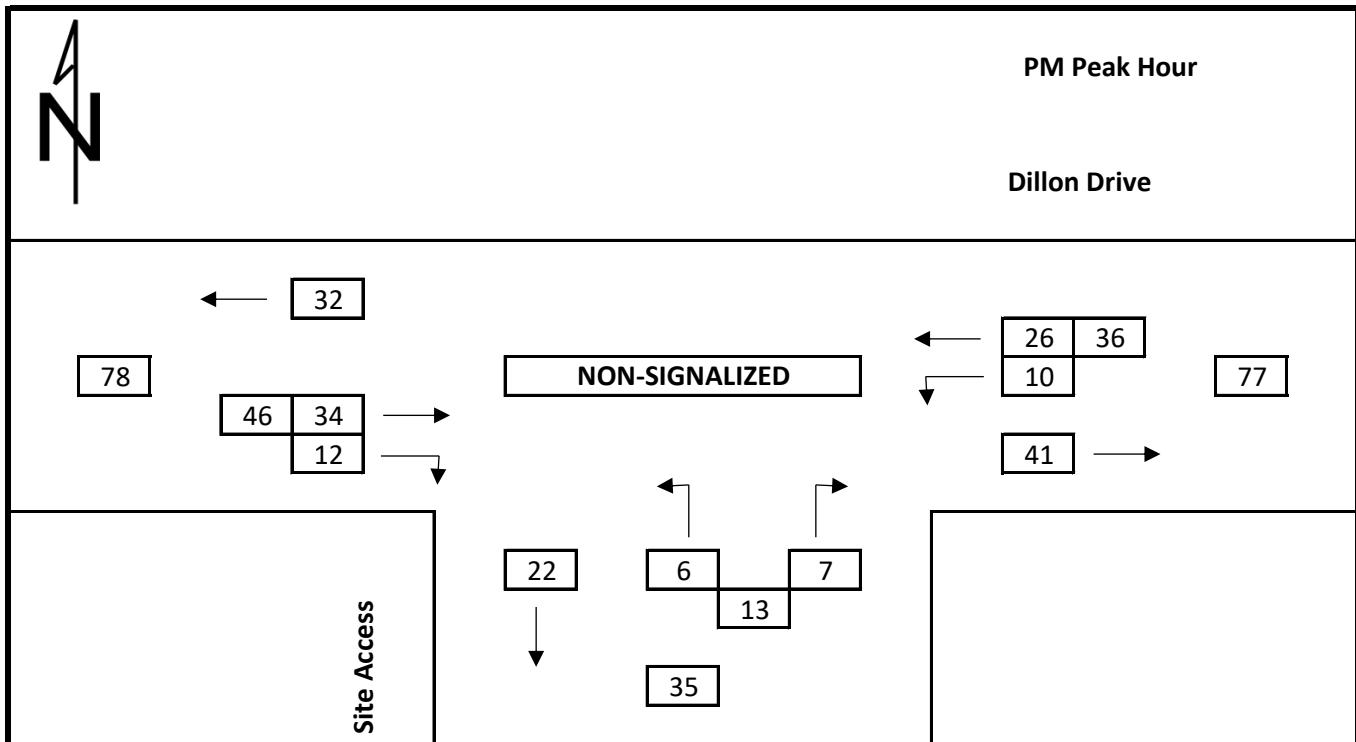
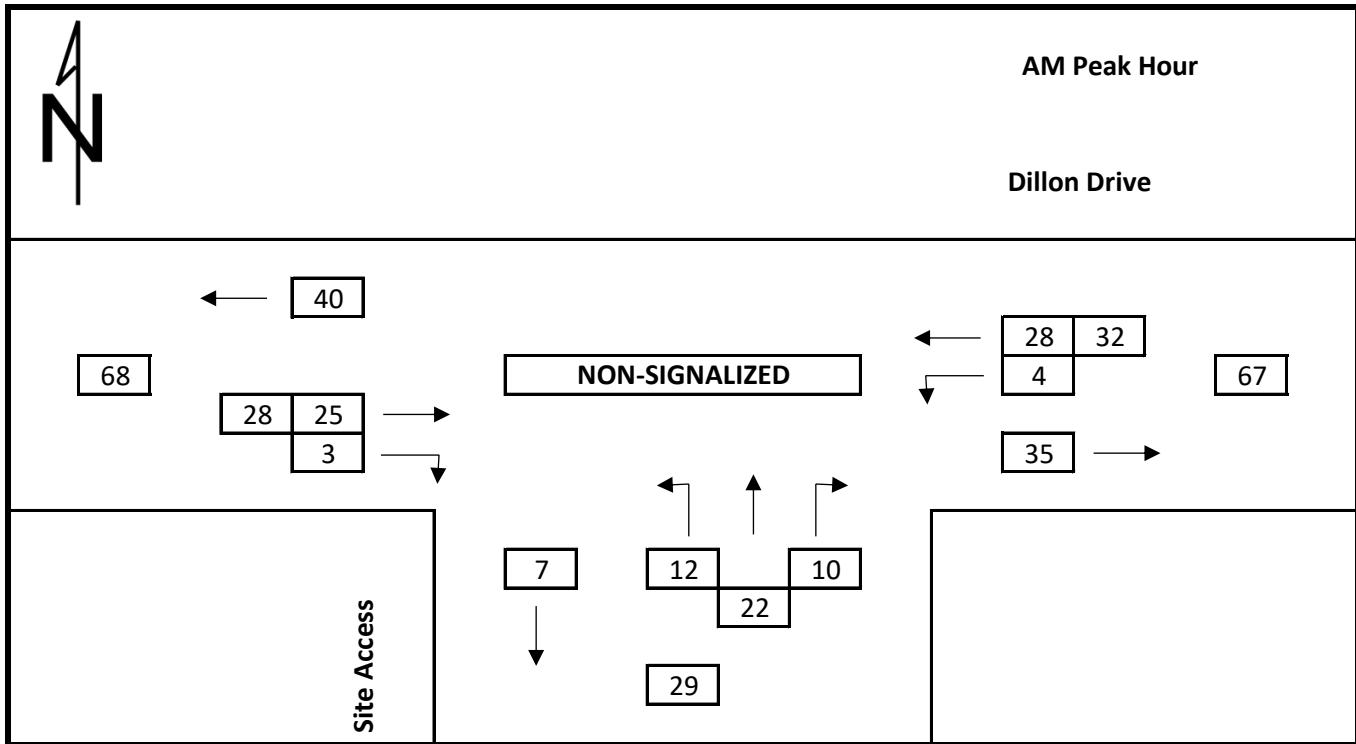


Background Traffic Year 2025

Dillon Drive at Site Access

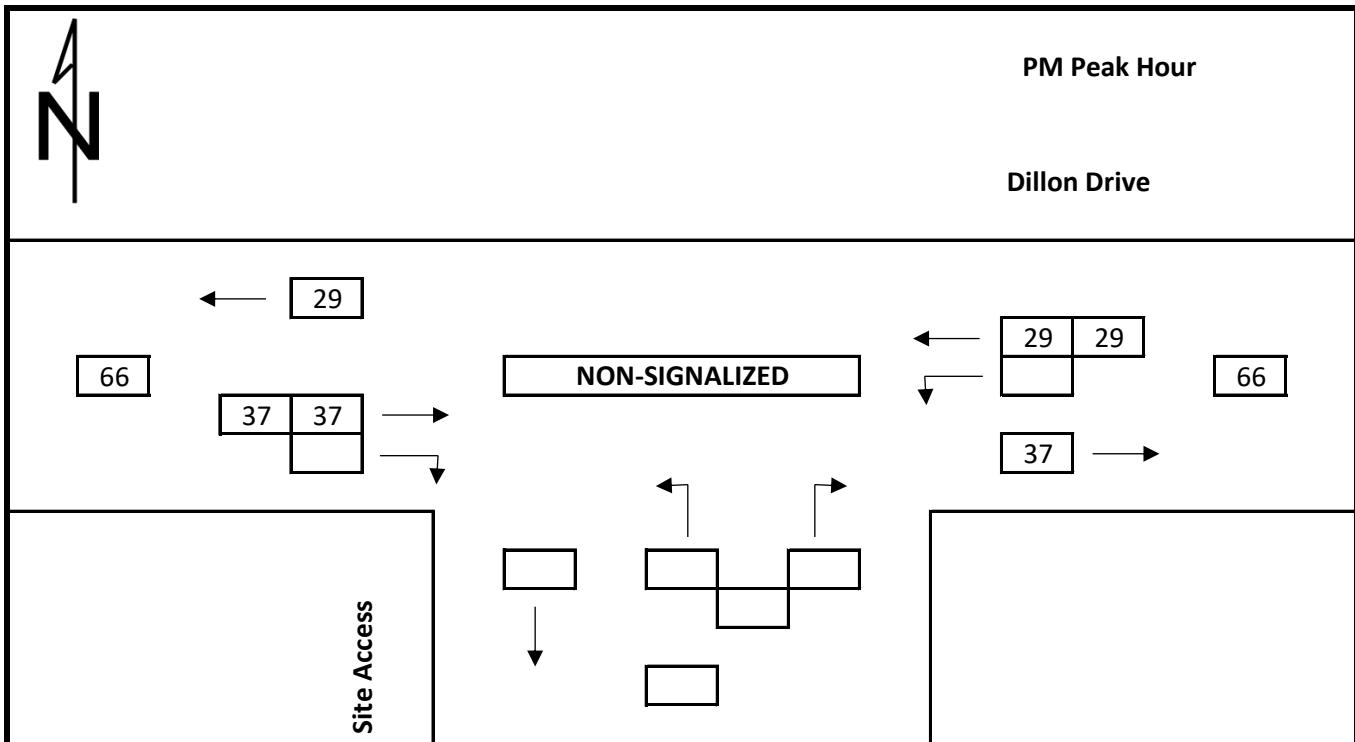
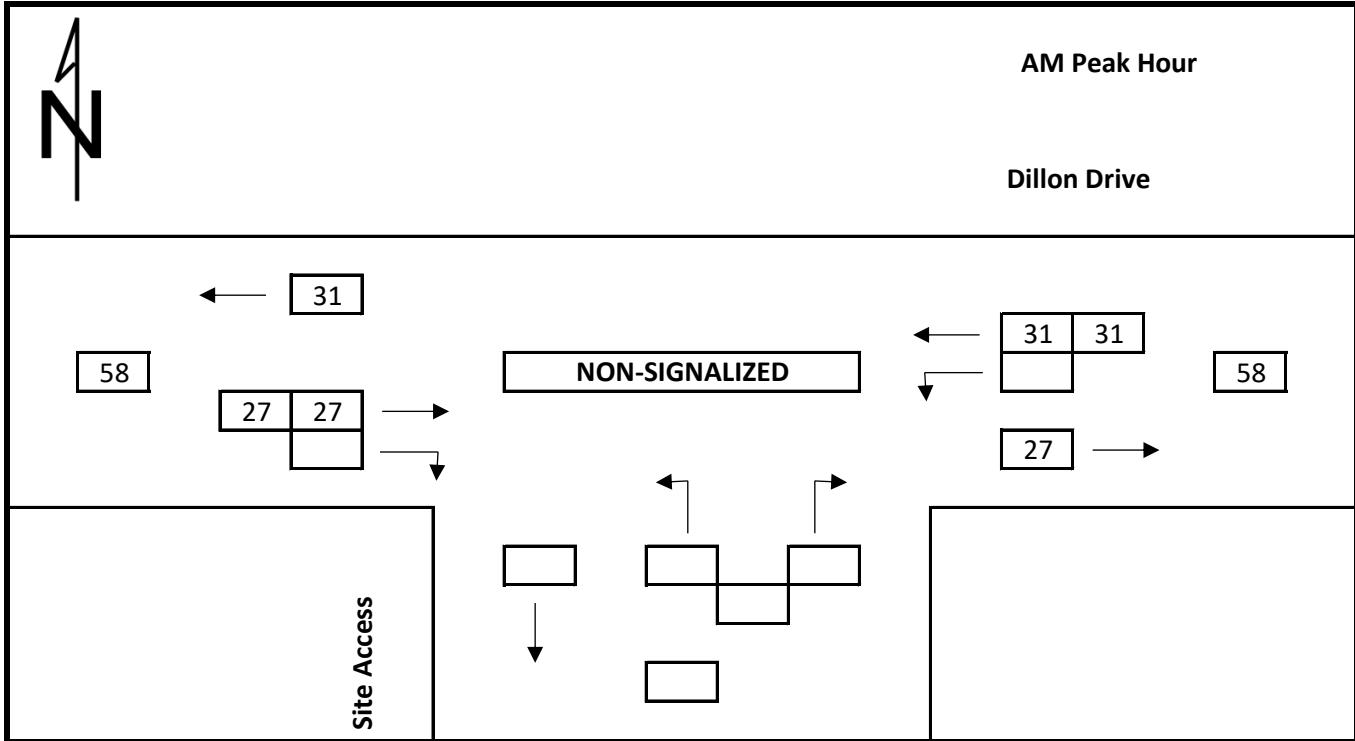


Total Traffic 2025
Dillon Drive at Site Access

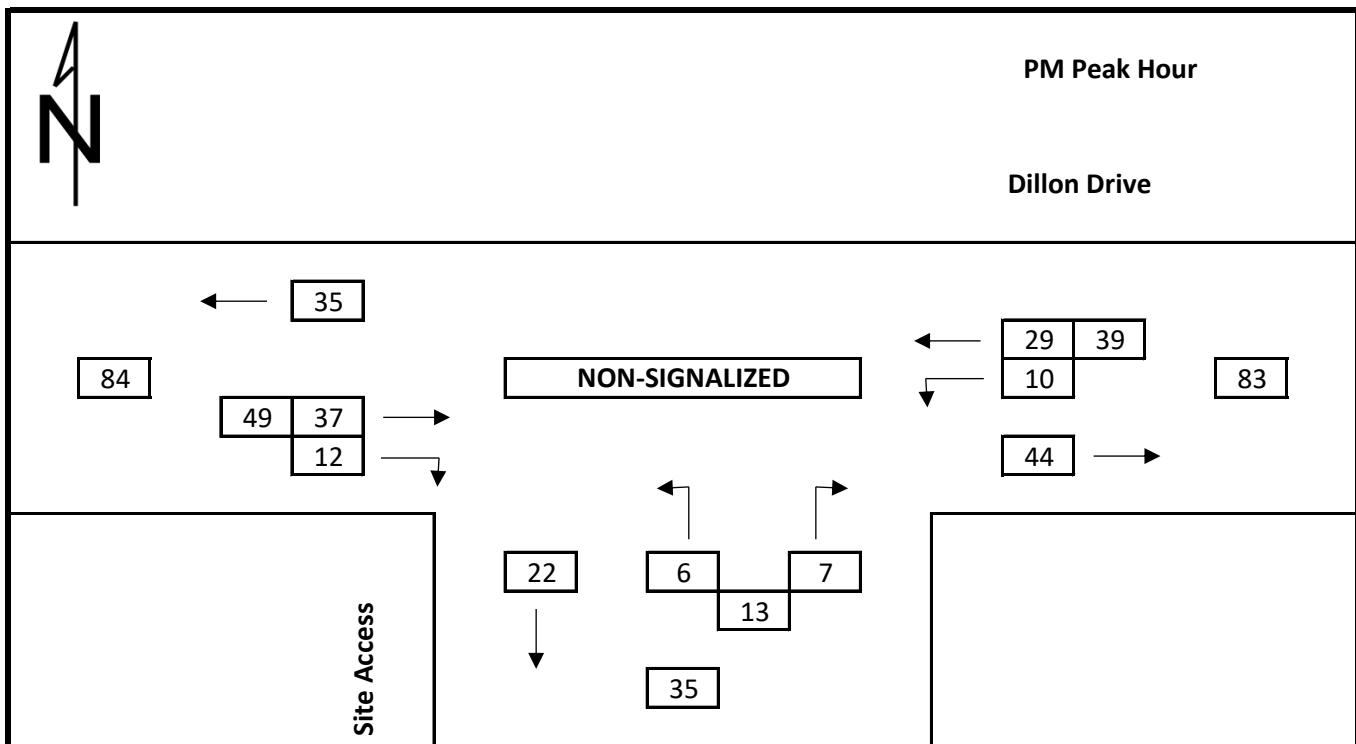
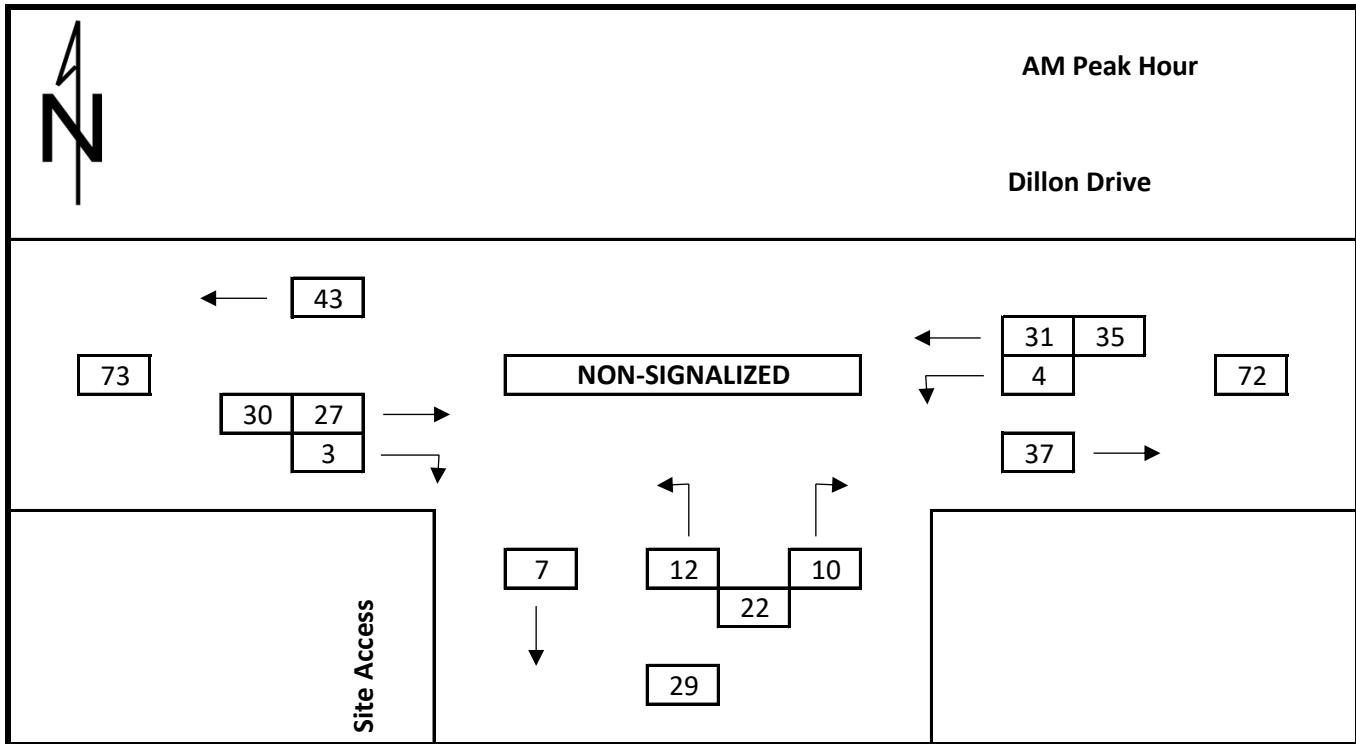


Background Traffic Year 2030

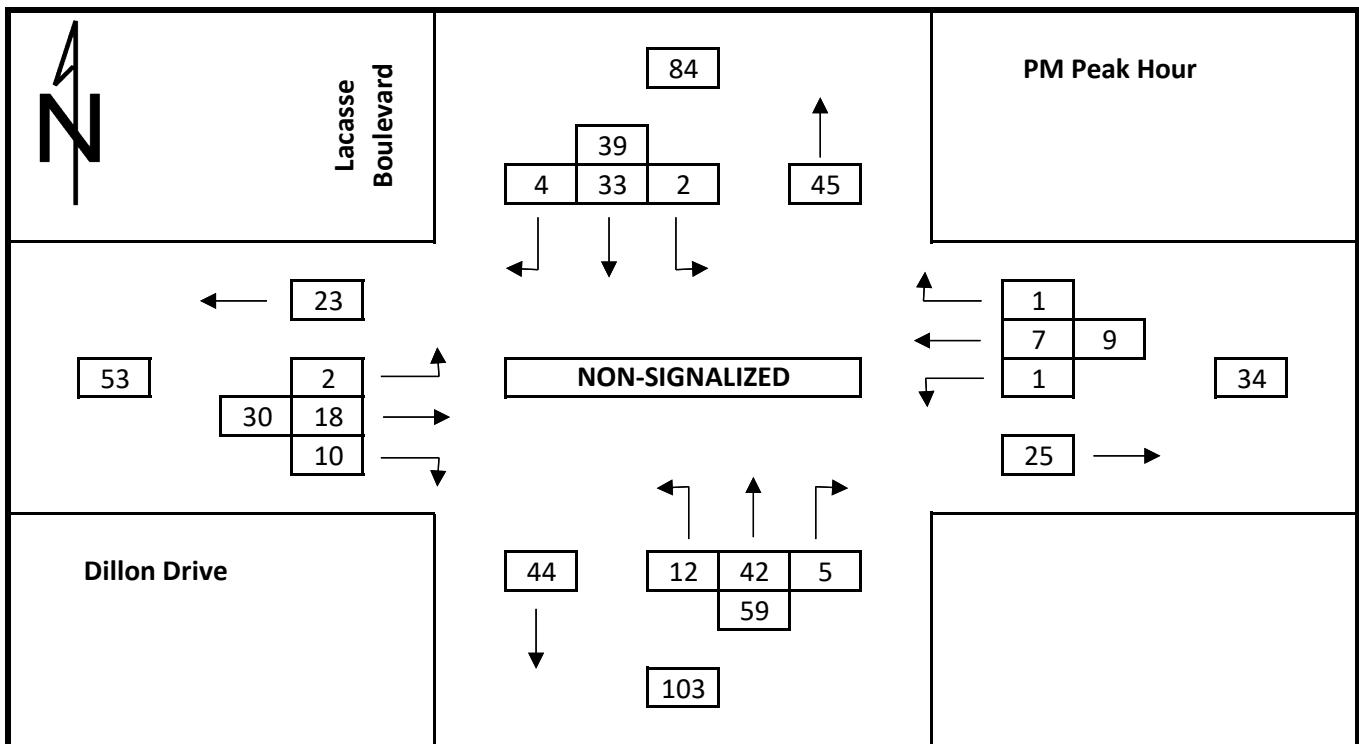
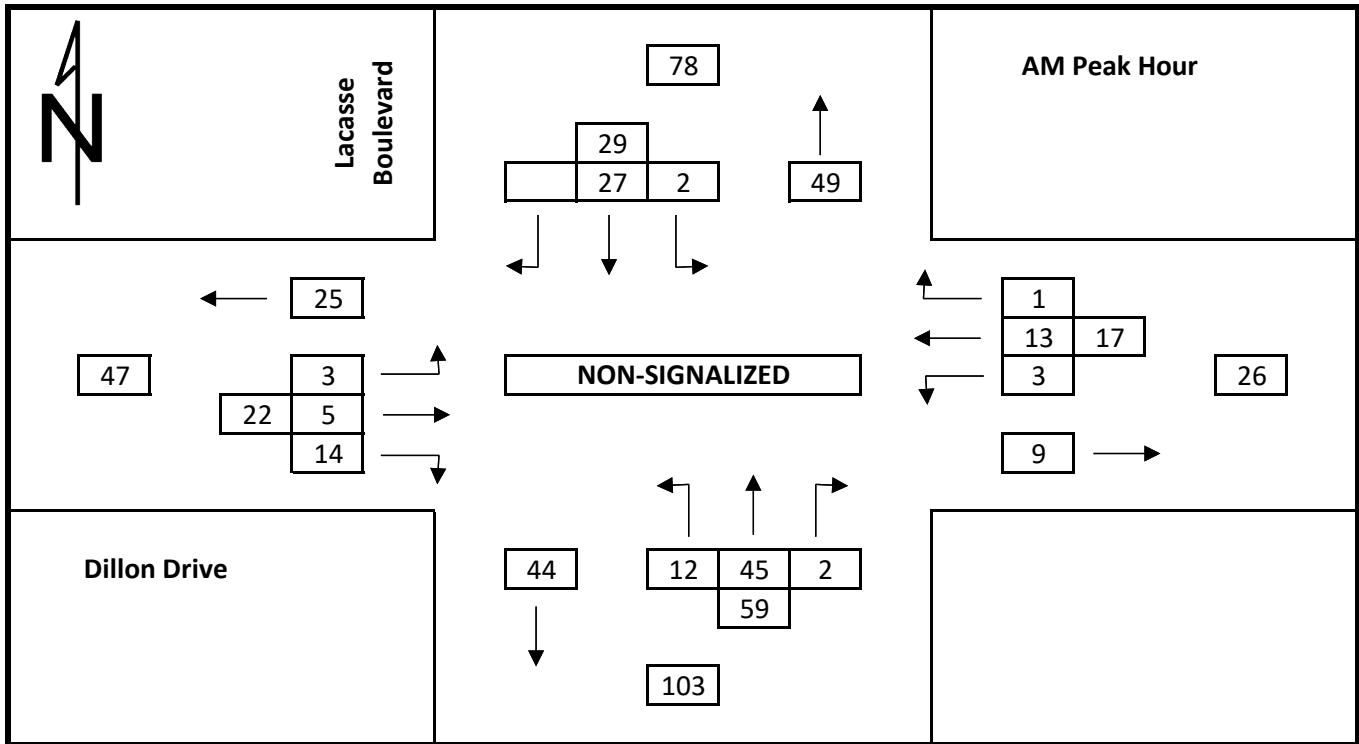
Dillon Drive at Site Access



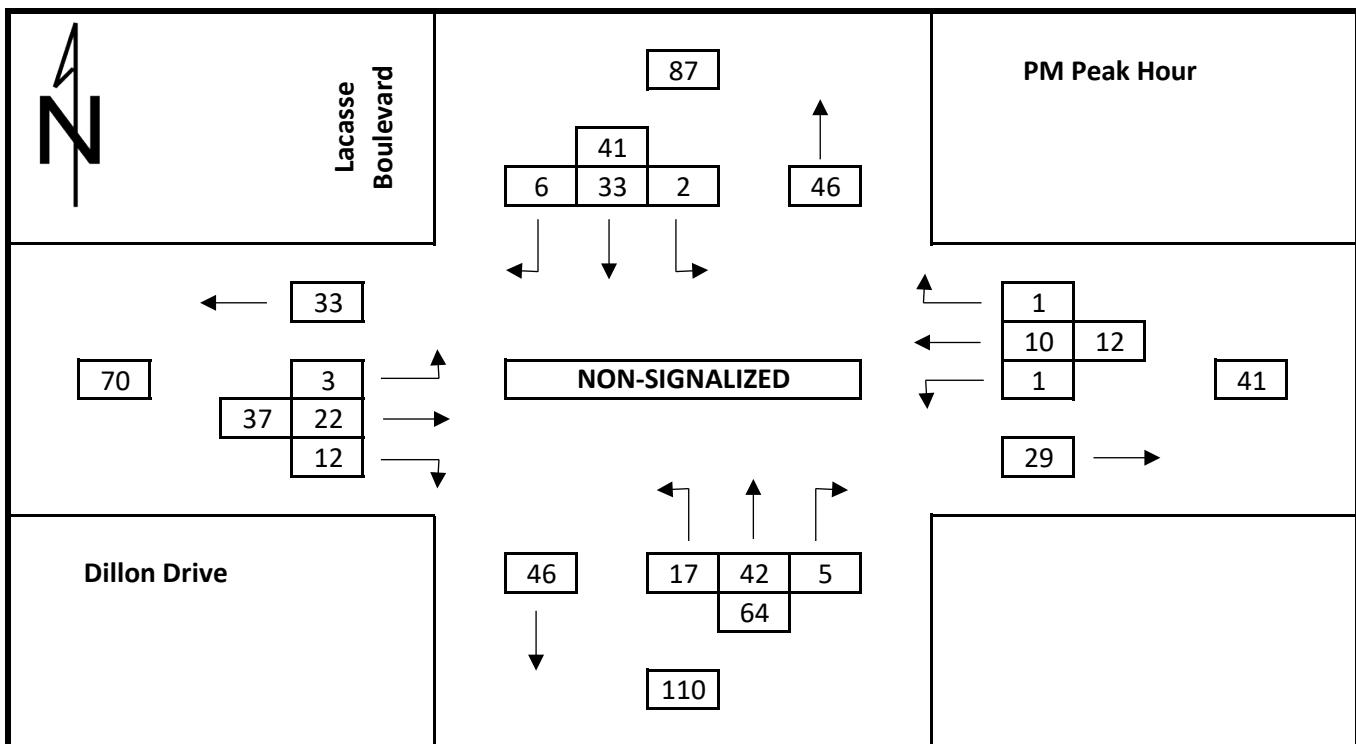
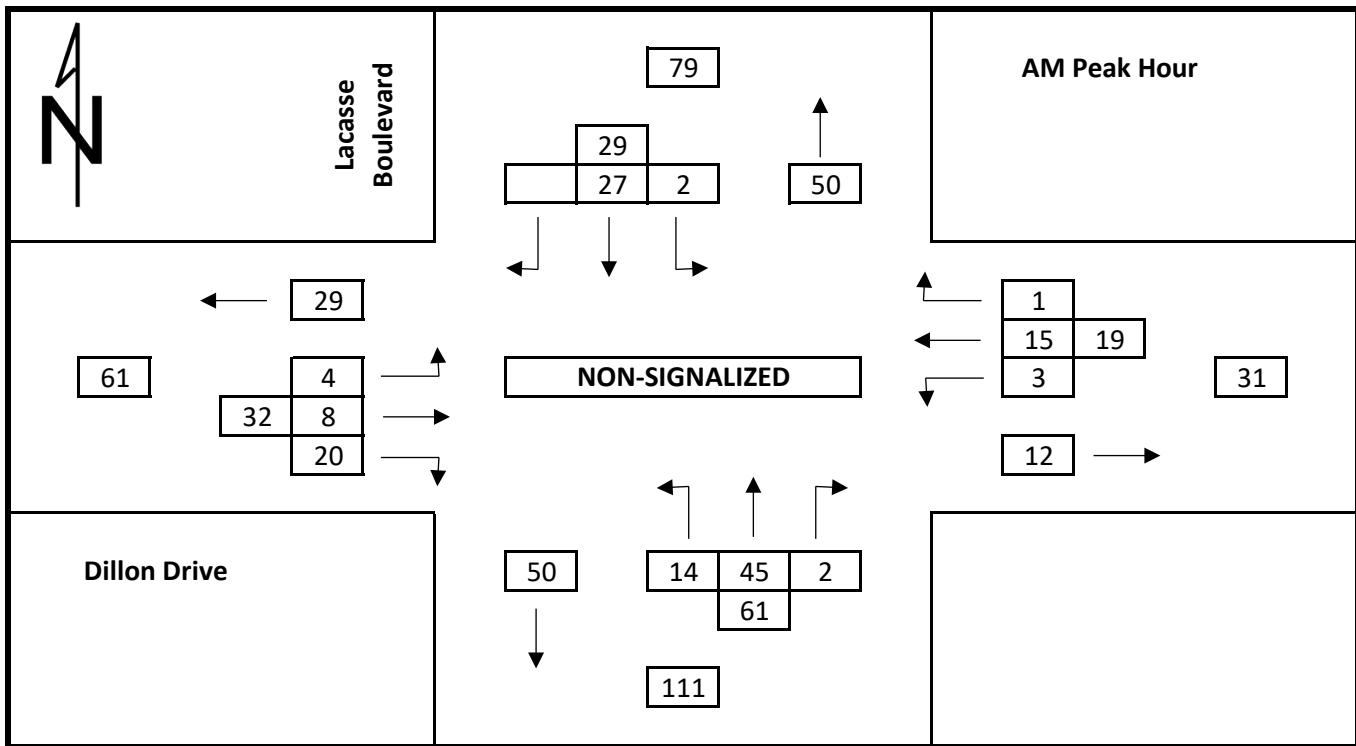
Total Traffic 2030
Dillon Drive at Site Access



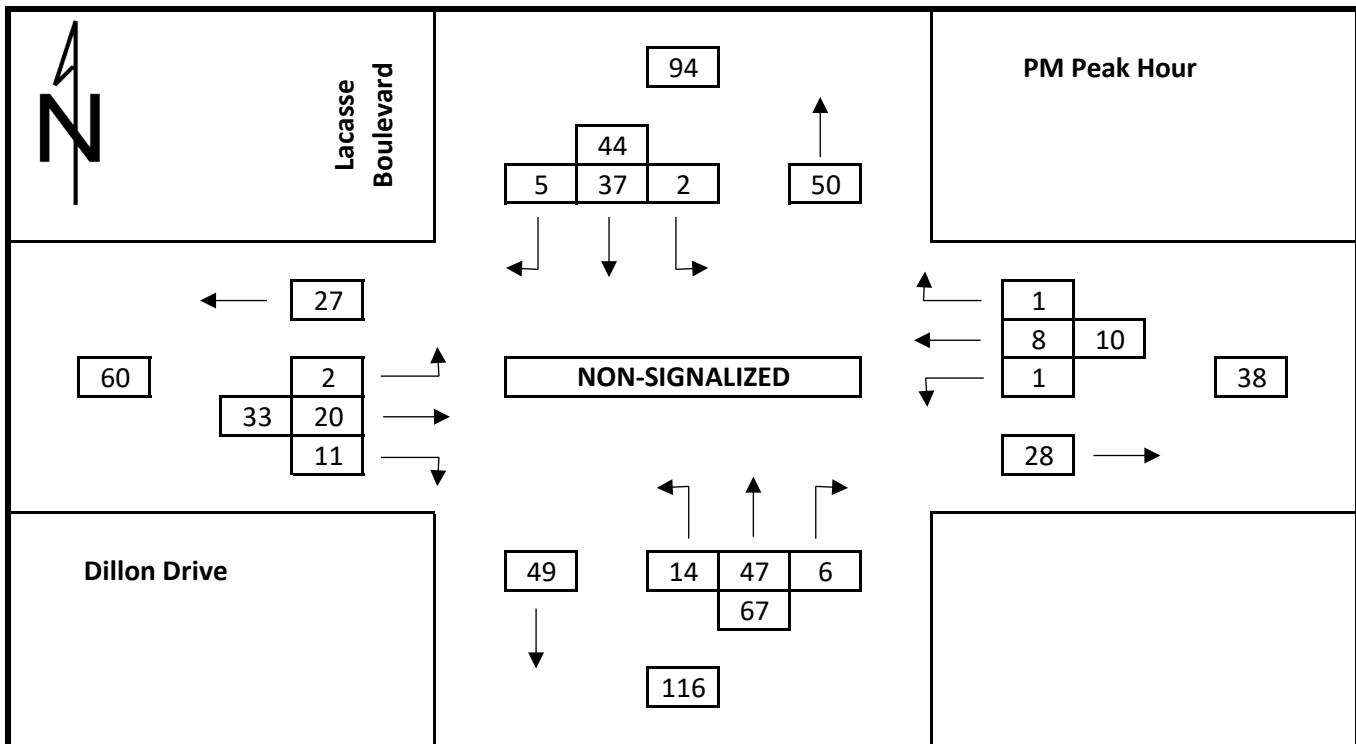
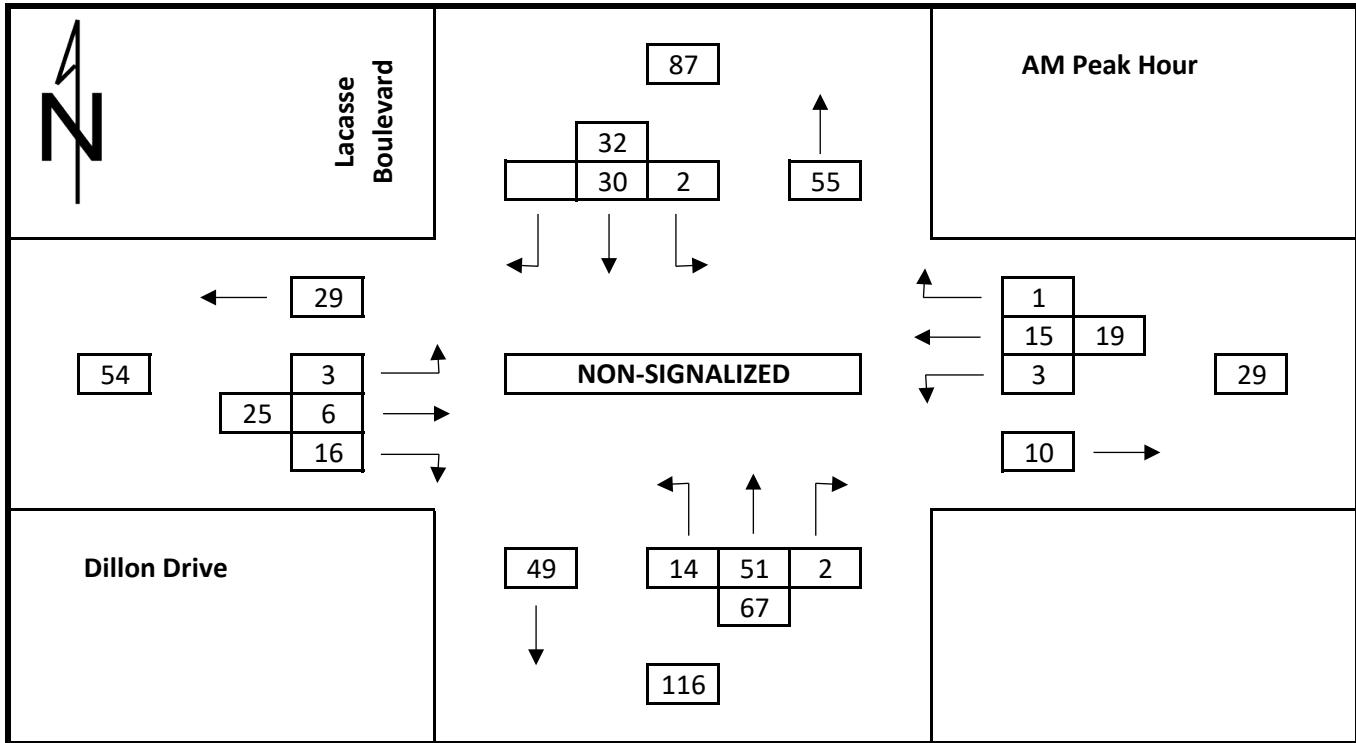
Existing Traffic Counts
Dillon Drive at Lacasse Boulevard



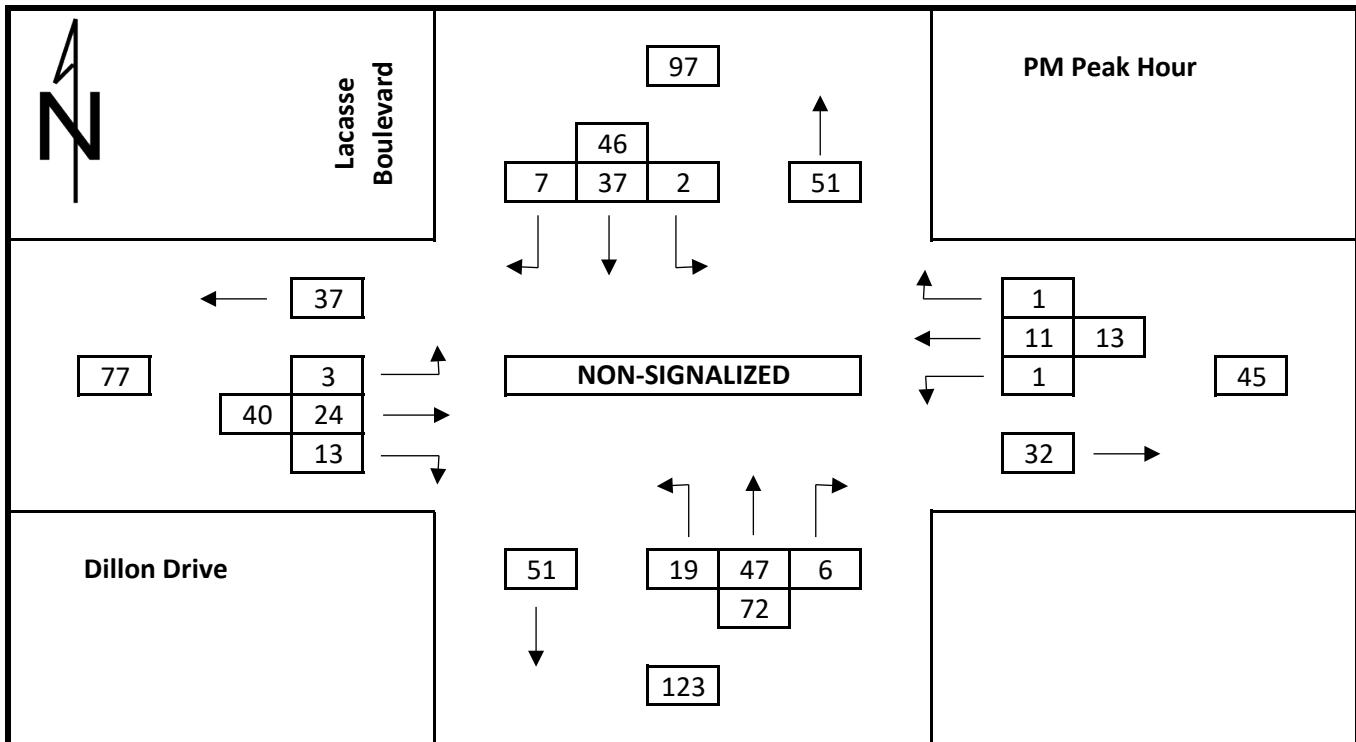
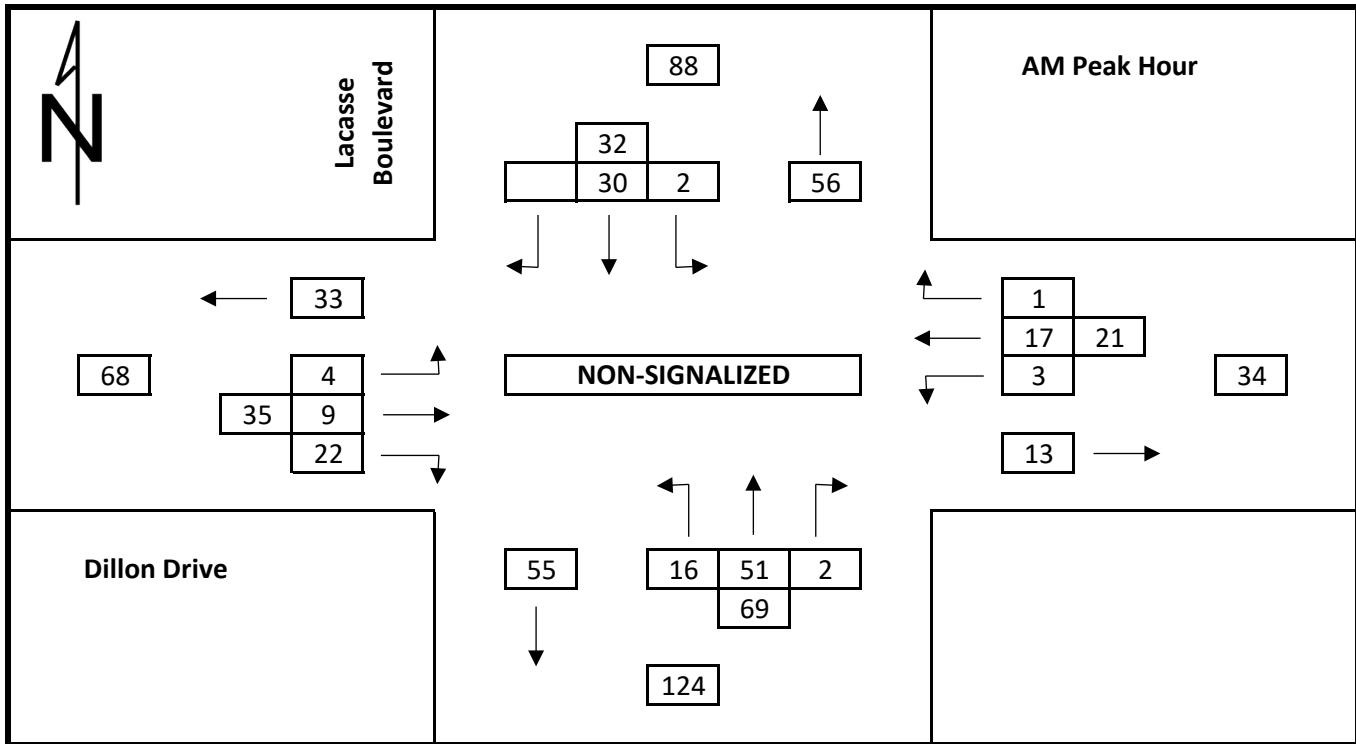
Existing + Site Generated Traffic
Dillon Drive at Lacasse Boulevard



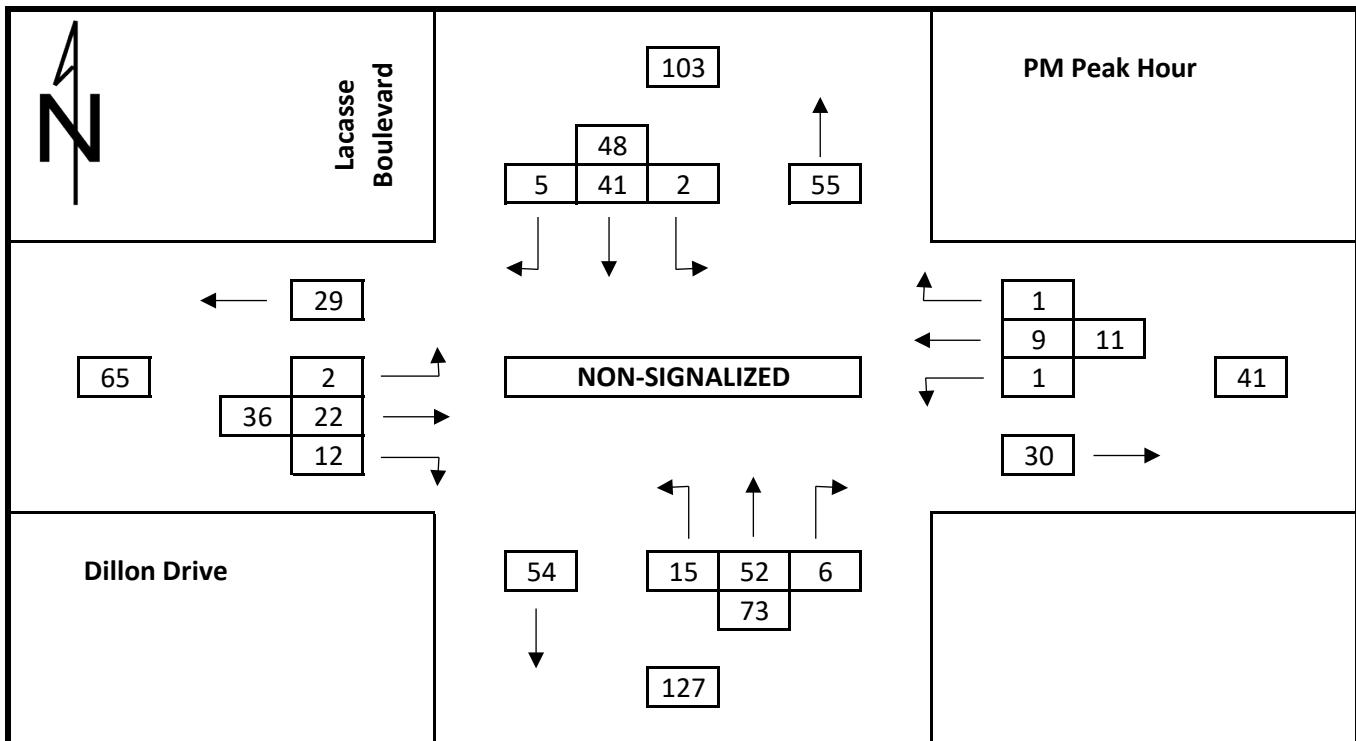
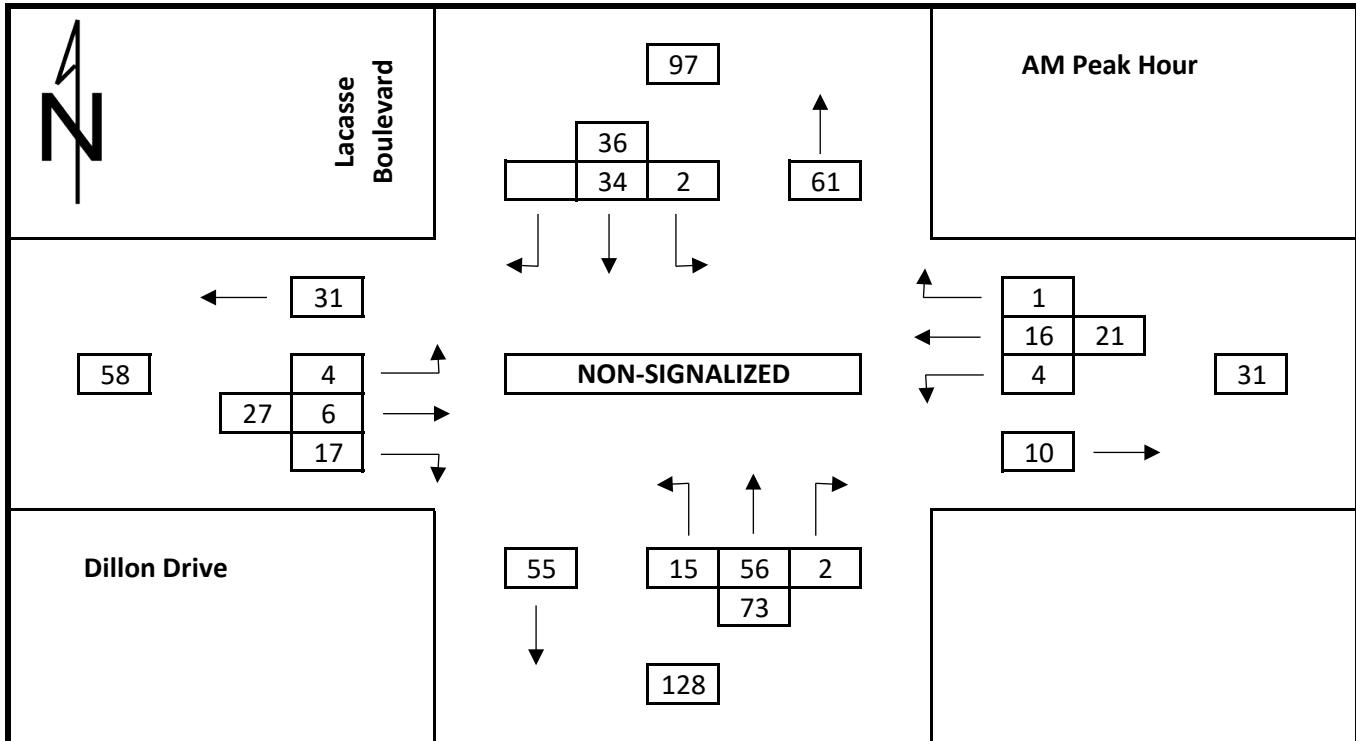
Background Traffic Year 2025
Dillon Drive at Lacasse Boulevard



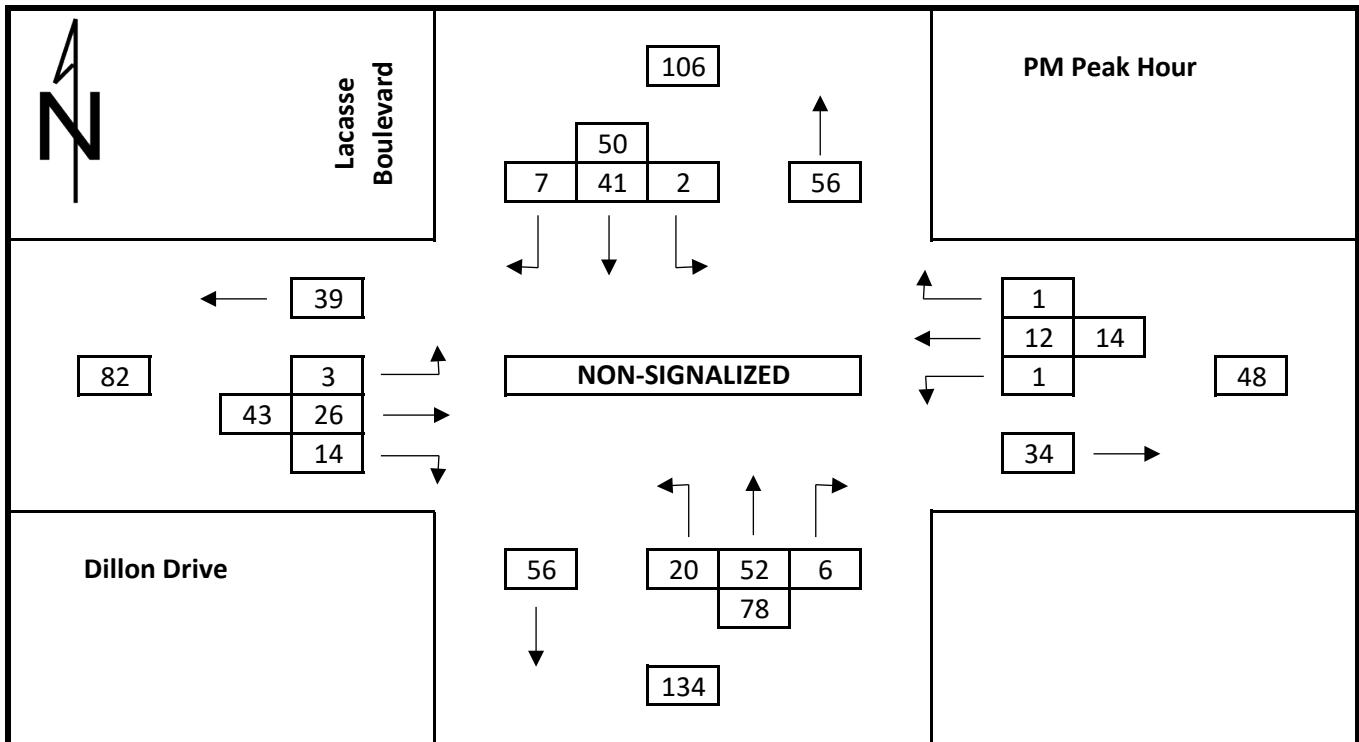
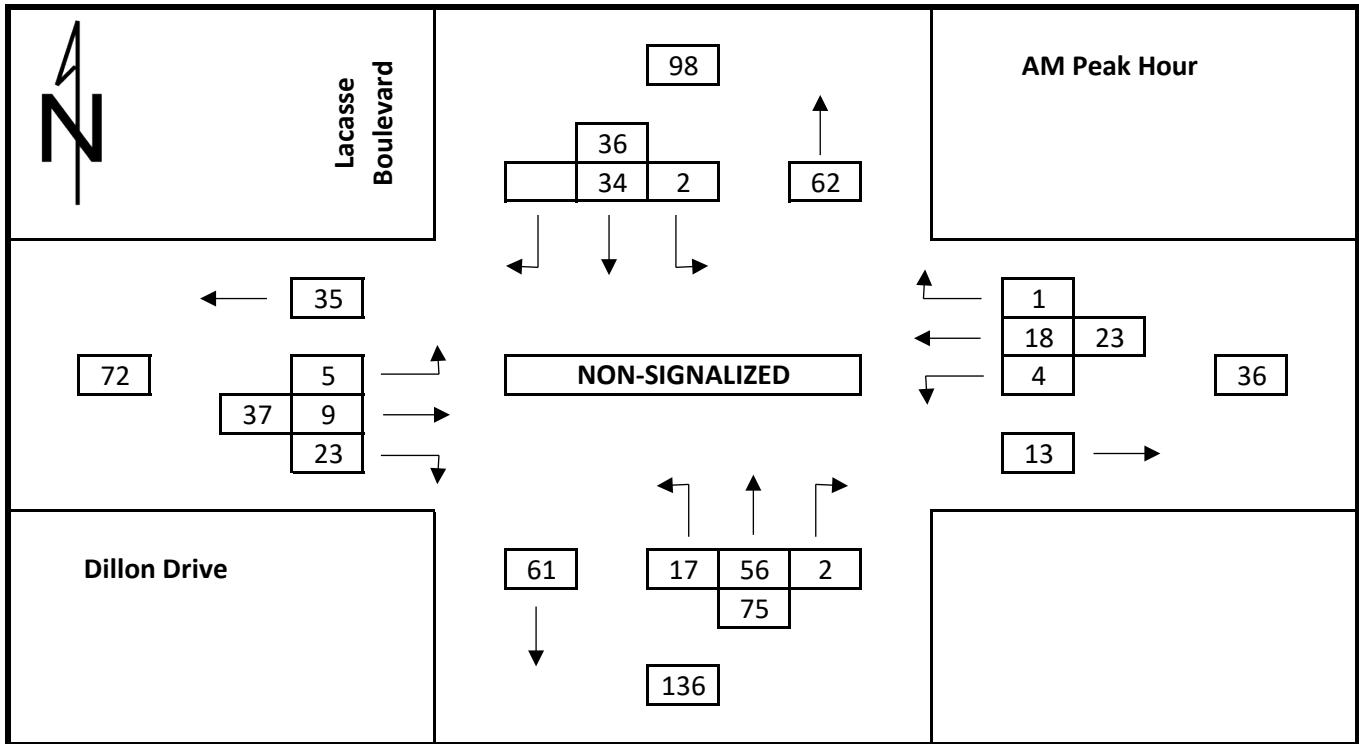
Total Traffic 2025
Dillon Drive at Lacasse Boulevard



Background Traffic Year 2030
Dillon Drive at Lacasse Boulevard



Total Traffic 2030
 Dillon Drive at Lacasse Boulevard



Appendix D

DETAILED SYNCHRO RESULTS

Dillon Drive at Lesperance Road

Dillon Drive at St. Pierre Street

Dillon Drive at Site Access

Dillon Drive at Lacasse Boulevard

Dillon Drive at Lesperance Road
Tecumseh, Ontario

Existing Traffic, AM Peak
Existing Geometric Configuration

Intersection

Int Delay, s/veh 2.5

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↔ | ↔ | | ↔ | ↔ | | ↑ | ↑ | | ↑ | ↑ | |
| Traffic Vol, veh/h | 3 | 5 | 13 | 26 | 2 | 15 | 3 | 102 | 13 | 4 | 88 | 3 |
| Future Vol, veh/h | 3 | 5 | 13 | 26 | 2 | 15 | 3 | 102 | 13 | 4 | 88 | 3 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | 450 | - | - | 100 | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 0 | 0 | 6 | 9 | 0 | 2 | 0 | 2 | 2 | 0 | 4 | 0 |
| Mvmt Flow | 3 | 5 | 14 | 28 | 2 | 16 | 3 | 111 | 14 | 4 | 96 | 3 |

| Major/Minor | Minor2 | Minor1 | | | Major1 | | | Major2 | | | | |
|----------------------|--------|--------|-------|-------|--------|-------|------|--------|---|------|---|---|
| Conflicting Flow All | 241 | 239 | 100 | 241 | 233 | 120 | 100 | 0 | 0 | 126 | 0 | 0 |
| Stage 1 | 107 | 107 | - | 125 | 125 | - | - | - | - | - | - | - |
| Stage 2 | 134 | 132 | - | 116 | 108 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.26 | 7.19 | 6.5 | 6.22 | 4.1 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.354 | 3.581 | 4 | 3.318 | 2.2 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 717 | 666 | 945 | 699 | 671 | 931 | 1505 | - | - | 1473 | - | - |
| Stage 1 | 903 | 811 | - | 862 | 796 | - | - | - | - | - | - | - |
| Stage 2 | 874 | 791 | - | 872 | 810 | - | - | - | - | - | - | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 699 | 661 | 943 | 681 | 666 | 929 | 1504 | - | - | 1472 | - | - |
| Mov Cap-2 Maneuver | 699 | 661 | - | 681 | 666 | - | - | - | - | - | - | - |
| Stage 1 | 900 | 808 | - | 859 | 794 | - | - | - | - | - | - | - |
| Stage 2 | 854 | 789 | - | 850 | 807 | - | - | - | - | - | - | - |

| Approach | EB | WB | | | NB | | | SB | | |
|-----------------------|-------|------|-----|-------|-------|-------|-----|-----|--|--|
| HCM Control Delay, s | 9.5 | 10.1 | | | 0.2 | | | 0.3 | | |
| HCM LOS | A | B | | | | | | | | |
| <hr/> | | | | | | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | WBLn1 | SBL | SBT | SBR | | |
| Capacity (veh/h) | 1504 | - | - | 819 | 750 | 1472 | - | - | | |
| HCM Lane V/C Ratio | 0.002 | - | - | 0.028 | 0.062 | 0.003 | - | - | | |
| HCM Control Delay (s) | 7.4 | - | - | 9.5 | 10.1 | 7.5 | - | - | | |
| HCM Lane LOS | A | - | - | A | B | A | - | - | | |
| HCM 95th %tile Q(veh) | 0 | - | - | 0.1 | 0.2 | 0 | - | - | | |

Dillon Drive at Lesperance Road
Tecumseh, Ontario

Existing Traffic, PM Peak
Existing Geometric Configuration

Intersection

Int Delay, s/veh 2.4

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 3 | 8 | 17 | 15 | 9 | 8 | 19 | 145 | 21 | 8 | 124 | 2 |
| Future Vol, veh/h | 3 | 8 | 17 | 15 | 9 | 8 | 19 | 145 | 21 | 8 | 124 | 2 |
| Conflicting Peds, #/hr | 2 | 0 | 2 | 10 | 0 | 10 | 12 | 0 | 12 | 6 | 0 | 6 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | 450 | - | - | 100 | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 |
| Heavy Vehicles, % | 0 | 0 | 6 | 9 | 0 | 2 | 0 | 2 | 2 | 0 | 4 | 0 |
| Mvmt Flow | 4 | 10 | 20 | 18 | 11 | 10 | 23 | 175 | 25 | 10 | 149 | 2 |

| Major/Minor | Minor2 | Minor1 | | | Major1 | | | Major2 | | | | |
|----------------------|--------|--------|-------|-------|--------|-------|------|--------|---|------|---|---|
| Conflicting Flow All | 436 | 440 | 172 | 441 | 429 | 210 | 163 | 0 | 0 | 212 | 0 | 0 |
| Stage 1 | 182 | 182 | - | 246 | 246 | - | - | - | - | - | - | - |
| Stage 2 | 254 | 258 | - | 195 | 183 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.26 | 7.19 | 6.5 | 6.22 | 4.1 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.354 | 3.581 | 4 | 3.318 | 2.2 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 534 | 514 | 861 | 515 | 521 | 830 | 1428 | - | - | 1370 | - | - |
| Stage 1 | 824 | 753 | - | 742 | 706 | - | - | - | - | - | - | - |
| Stage 2 | 755 | 698 | - | 791 | 752 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | - | - | - |
| Mov Cap-1 Maneuver | 500 | 492 | 845 | 477 | 499 | 815 | 1413 | - | - | 1356 | - | - |
| Mov Cap-2 Maneuver | 500 | 492 | - | 477 | 499 | - | - | - | - | - | - | - |
| Stage 1 | 803 | 740 | - | 723 | 688 | - | - | - | - | - | - | - |
| Stage 2 | 716 | 680 | - | 750 | 739 | - | - | - | - | - | - | - |

| Approach | EB | WB | | | NB | | | SB | | | | |
|-----------------------|-------|------|-----|-------|-------|-------|-----|-----|--|--|--|--|
| HCM Control Delay, s | 10.7 | 12.2 | | | 0.8 | | | 0.5 | | | | |
| HCM LOS | B | B | | | | | | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | WBLn1 | SBL | SBT | SBR | | | | |
| Capacity (veh/h) | 1413 | - | - | 661 | 540 | 1356 | - | - | | | | |
| HCM Lane V/C Ratio | 0.016 | - | - | 0.051 | 0.071 | 0.007 | - | - | | | | |
| HCM Control Delay (s) | 7.6 | - | - | 10.7 | 12.2 | 7.7 | - | - | | | | |
| HCM Lane LOS | A | - | - | B | B | A | - | - | | | | |
| HCM 95th %tile Q(veh) | 0 | - | - | 0.2 | 0.2 | 0 | - | - | | | | |

Intersection

Int Delay, s/veh 2.8

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 3 | 6 | 13 | 33 | 3 | 19 | 3 | 102 | 15 | 4 | 88 | 3 |
| Future Vol, veh/h | 3 | 6 | 13 | 33 | 3 | 19 | 3 | 102 | 15 | 4 | 88 | 3 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | 450 | - | - | 100 | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 0 | 0 | 6 | 9 | 0 | 2 | 0 | 2 | 2 | 0 | 4 | 0 |
| Mvmt Flow | 3 | 7 | 14 | 36 | 3 | 21 | 3 | 111 | 16 | 4 | 96 | 3 |

| Major/Minor | Minor2 | Minor1 | | | Major1 | | Major2 | | | | | |
|----------------------|--------|--------|-------|-------|--------|-------|--------|---|---|------|---|---|
| Conflicting Flow All | 245 | 241 | 100 | 243 | 234 | 121 | 100 | 0 | 0 | 128 | 0 | 0 |
| Stage 1 | 107 | 107 | - | 126 | 126 | - | - | - | - | - | - | - |
| Stage 2 | 138 | 134 | - | 117 | 108 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.26 | 7.19 | 6.5 | 6.22 | 4.1 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.354 | 3.581 | 4 | 3.318 | 2.2 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 713 | 664 | 945 | 697 | 670 | 930 | 1505 | - | - | 1470 | - | - |
| Stage 1 | 903 | 811 | - | 861 | 796 | - | - | - | - | - | - | - |
| Stage 2 | 870 | 789 | - | 871 | 810 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 691 | 659 | 943 | 677 | 665 | 928 | 1504 | - | - | 1469 | - | - |
| Mov Cap-2 Maneuver | 691 | 659 | - | 677 | 665 | - | - | - | - | - | - | - |
| Stage 1 | 900 | 808 | - | 858 | 794 | - | - | - | - | - | - | - |
| Stage 2 | 845 | 787 | - | 848 | 807 | - | - | - | - | - | - | - |

| Approach | EB | WB | | | NB | | SB | | |
|-----------------------|-------|------|-----|-------|-------|-------|-----|-----|--|
| HCM Control Delay, s | 9.6 | 10.2 | | | 0.2 | | 0.3 | | |
| HCM LOS | A | B | | | | | | | |
| <hr/> | | | | | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | WBLn1 | SBL | SBT | SBR | |
| Capacity (veh/h) | 1504 | - | - | 808 | 746 | 1469 | - | - | |
| HCM Lane V/C Ratio | 0.002 | - | - | 0.03 | 0.08 | 0.003 | - | - | |
| HCM Control Delay (s) | 7.4 | - | - | 9.6 | 10.2 | 7.5 | - | - | |
| HCM Lane LOS | A | - | - | A | B | A | - | - | |
| HCM 95th %tile Q(veh) | 0 | - | - | 0.1 | 0.3 | 0 | - | - | |

Dillon Drive at Lesperance Road
Tecumseh, Ontario

Existing + Site Generated Traffic, PM Peak

Existing Geometric Configuration

Intersection

Int Delay, s/veh 2.6

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 3 | 10 | 17 | 18 | 11 | 9 | 19 | 145 | 28 | 10 | 124 | 2 |
| Future Vol, veh/h | 3 | 10 | 17 | 18 | 11 | 9 | 19 | 145 | 28 | 10 | 124 | 2 |
| Conflicting Peds, #/hr | 2 | 0 | 2 | 10 | 0 | 10 | 12 | 0 | 12 | 6 | 0 | 6 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | 450 | - | - | 100 | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 |
| Heavy Vehicles, % | 0 | 0 | 6 | 9 | 0 | 2 | 0 | 2 | 2 | 0 | 4 | 0 |
| Mvmt Flow | 4 | 12 | 20 | 22 | 13 | 11 | 23 | 175 | 34 | 12 | 149 | 2 |

| Major/Minor | Minor2 | Minor1 | | | Major1 | | | Major2 | | | | |
|----------------------|--------|--------|-------|-------|--------|-------|------|--------|---|------|---|---|
| Conflicting Flow All | 446 | 453 | 172 | 450 | 437 | 214 | 163 | 0 | 0 | 221 | 0 | 0 |
| Stage 1 | 186 | 186 | - | 250 | 250 | - | - | - | - | - | - | - |
| Stage 2 | 260 | 267 | - | 200 | 187 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.26 | 7.19 | 6.5 | 6.22 | 4.1 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.354 | 3.581 | 4 | 3.318 | 2.2 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 526 | 506 | 861 | 508 | 516 | 826 | 1428 | - | - | 1360 | - | - |
| Stage 1 | 820 | 750 | - | 739 | 704 | - | - | - | - | - | - | - |
| Stage 2 | 749 | 692 | - | 786 | 749 | - | - | - | - | - | - | - |
| Platoon blocked, % | - | - | - | - | - | - | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | 489 | 484 | 845 | 468 | 493 | 811 | 1413 | - | - | 1346 | - | - |
| Mov Cap-2 Maneuver | 489 | 484 | - | 468 | 493 | - | - | - | - | - | - | - |
| Stage 1 | 799 | 736 | - | 720 | 686 | - | - | - | - | - | - | - |
| Stage 2 | 707 | 674 | - | 741 | 735 | - | - | - | - | - | - | - |

| Approach | EB | WB | | | NB | | | SB | | | | |
|-----------------------|-------|------|-----|-------|-------|-------|-----|-----|--|--|--|--|
| HCM Control Delay, s | 11 | 12.4 | | | 0.8 | | | 0.6 | | | | |
| HCM LOS | B | B | | | | | | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | WBLn1 | SBL | SBT | SBR | | | | |
| Capacity (veh/h) | 1413 | - | - | 639 | 529 | 1346 | - | - | | | | |
| HCM Lane V/C Ratio | 0.016 | - | - | 0.057 | 0.087 | 0.009 | - | - | | | | |
| HCM Control Delay (s) | 7.6 | - | - | 11 | 12.4 | 7.7 | - | - | | | | |
| HCM Lane LOS | A | - | - | B | B | A | - | - | | | | |
| HCM 95th %tile Q(veh) | 0 | - | - | 0.2 | 0.3 | 0 | - | - | | | | |

| Intersection | | | | | | | | | | | | | |
|--------------------------|-------|--------|-------|-------|--------|-------|-------|--------|------|------|------|------|--|
| Int Delay, s/veh | 2.5 | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | ↔ | | | ↔ | | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | |
| Traffic Vol, veh/h | 3 | 6 | 15 | 29 | 2 | 17 | 3 | 115 | 15 | 5 | 99 | 3 | |
| Future Vol, veh/h | 3 | 6 | 15 | 29 | 2 | 17 | 3 | 115 | 15 | 5 | 99 | 3 | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free | |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None | |
| Storage Length | - | - | - | - | - | - | 450 | - | - | 100 | - | - | |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | |
| Heavy Vehicles, % | 0 | 0 | 6 | 9 | 0 | 2 | 0 | 2 | 2 | 0 | 4 | 0 | |
| Mvmt Flow | 3 | 7 | 16 | 32 | 2 | 18 | 3 | 125 | 16 | 5 | 108 | 3 | |
| Major/Minor | | | | | | | | | | | | | |
| Minor2 | | Minor1 | | | Major1 | | | Major2 | | | | | |
| Conflicting Flow All | 271 | 269 | 112 | 272 | 262 | 135 | 112 | 0 | 0 | 142 | 0 | 0 | |
| Stage 1 | 121 | 121 | - | 140 | 140 | - | - | - | - | - | - | - | |
| Stage 2 | 150 | 148 | - | 132 | 122 | - | - | - | - | - | - | - | |
| Critical Hdwy | 7.1 | 6.5 | 6.26 | 7.19 | 6.5 | 6.22 | 4.1 | - | - | 4.1 | - | - | |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - | |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - | |
| Follow-up Hdwy | 3.5 | 4 | 3.354 | 3.581 | 4 | 3.318 | 2.2 | - | - | 2.2 | - | - | |
| Pot Cap-1 Maneuver | 686 | 641 | 930 | 666 | 646 | 914 | 1490 | - | - | 1453 | - | - | |
| Stage 1 | 888 | 800 | - | 847 | 785 | - | - | - | - | - | - | - | |
| Stage 2 | 857 | 779 | - | 855 | 799 | - | - | - | - | - | - | - | |
| Platoon blocked, % | | | | | | | | - | - | - | - | - | |
| Mov Cap-1 Maneuver | 666 | 637 | 928 | 645 | 641 | 912 | 1489 | - | - | 1452 | - | - | |
| Mov Cap-2 Maneuver | 666 | 637 | - | 645 | 641 | - | - | - | - | - | - | - | |
| Stage 1 | 885 | 797 | - | 844 | 783 | - | - | - | - | - | - | - | |
| Stage 2 | 835 | 777 | - | 830 | 796 | - | - | - | - | - | - | - | |
| Approach | | | | | | | | | | | | | |
| EB | | | WB | | | NB | | | SB | | | | |
| HCM Control Delay, s | 9.7 | | 10.4 | | | 0.2 | | | 0.3 | | | | |
| HCM LOS | A | | B | | | | | | | | | | |
| Minor Lane/Major Mvmt | | NBL | NBT | NBR | EBLn1 | WBLn1 | SBL | SBT | SBR | | | | |
| Capacity (veh/h) | 1489 | | - | - | 798 | 719 | 1452 | - | - | | | | |
| HCM Lane V/C Ratio | 0.002 | | - | - | 0.033 | 0.073 | 0.004 | - | - | | | | |
| HCM Control Delay (s) | 7.4 | | - | - | 9.7 | 10.4 | 7.5 | - | - | | | | |
| HCM Lane LOS | A | | - | - | A | B | A | - | - | | | | |
| HCM 95th %tile Q(veh) | 0 | | - | - | 0.1 | 0.2 | 0 | - | - | | | | |

Dillon Drive at Lesperance Road
Tecumseh, Ontario

Background Traffic 2025, PM Peak
Existing Geometric Configuration

Intersection

Int Delay, s/veh 2.5

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↔ | | | ↔ | | ↑ | ↔ | ↑ | | ↑ | ↔ | ↑ |
| Traffic Vol, veh/h | 3 | 9 | 19 | 17 | 10 | 9 | 21 | 163 | 24 | 9 | 140 | 2 |
| Future Vol, veh/h | 3 | 9 | 19 | 17 | 10 | 9 | 21 | 163 | 24 | 9 | 140 | 2 |
| Conflicting Peds, #/hr | 2 | 0 | 2 | 10 | 0 | 10 | 12 | 0 | 12 | 6 | 0 | 6 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | 450 | - | - | 100 | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 |
| Heavy Vehicles, % | 0 | 0 | 6 | 9 | 0 | 2 | 0 | 2 | 2 | 0 | 4 | 0 |
| Mvmt Flow | 4 | 11 | 23 | 20 | 12 | 11 | 25 | 196 | 29 | 11 | 169 | 2 |

| Major/Minor | Minor2 | Minor1 | | Major1 | | Major2 | |
|----------------------|--------|--------|-------|--------|-----|--------|------|
| Conflicting Flow All | 486 | 491 | 192 | 492 | 478 | 233 | 183 |
| Stage 1 | 204 | 204 | - | 273 | 273 | - | - |
| Stage 2 | 282 | 287 | - | 219 | 205 | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.26 | 7.19 | 6.5 | 6.22 | 4.1 |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.354 | 3.581 | 4 | 3.318 | 2.2 |
| Pot Cap-1 Maneuver | 495 | 481 | 839 | 476 | 489 | 806 | 1404 |
| Stage 1 | 803 | 737 | - | 718 | 688 | - | - |
| Stage 2 | 729 | 678 | - | 768 | 736 | - | - |
| Platoon blocked, % | | | | | | - | - |
| Mov Cap-1 Maneuver | 460 | 459 | 823 | 437 | 467 | 791 | 1390 |
| Mov Cap-2 Maneuver | 460 | 459 | - | 437 | 467 | - | - |
| Stage 1 | 781 | 724 | - | 698 | 669 | - | - |
| Stage 2 | 687 | 659 | - | 723 | 723 | - | - |

| Approach | EB | WB | | NB | | SB | | |
|-----------------------|-------|------|-----|-------|-------|-------|-----|-----|
| HCM Control Delay, s | 11.1 | 12.8 | | 0.8 | | 0.5 | | |
| HCM LOS | B | B | | | | | | |
| <hr/> | | | | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBln1 | WBln1 | SBL | SBT | SBR |
| Capacity (veh/h) | 1390 | - | - | 630 | 502 | 1328 | - | - |
| HCM Lane V/C Ratio | 0.018 | - | - | 0.059 | 0.086 | 0.008 | - | - |
| HCM Control Delay (s) | 7.6 | - | - | 11.1 | 12.8 | 7.7 | - | - |
| HCM Lane LOS | A | - | - | B | B | A | - | - |
| HCM 95th %tile Q(veh) | 0.1 | - | - | 0.2 | 0.3 | 0 | - | - |

Dillon Drive at Lesperance Road
Tecumseh, Ontario

Total Traffic 2025, AM Peak
Existing Geometric Configuration

Intersection

Int Delay, s/veh 2.9

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|----------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

| | | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|--|
| Lane Configurations | | | | | | | | | | | | | |
| Traffic Vol, veh/h | 3 | 7 | 15 | 36 | 3 | 21 | 3 | 115 | 17 | 5 | 99 | 3 | |
| Future Vol, veh/h | 3 | 7 | 15 | 36 | 3 | 21 | 3 | 115 | 17 | 5 | 99 | 3 | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free | |
| RT Channelized | - | - | None | |
| Storage Length | - | - | - | - | - | - | 450 | - | - | 100 | - | - | |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | |
| Heavy Vehicles, % | 0 | 0 | 6 | 9 | 0 | 2 | 0 | 2 | 2 | 0 | 4 | 0 | |
| Mvmt Flow | 3 | 8 | 16 | 39 | 3 | 23 | 3 | 125 | 18 | 5 | 108 | 3 | |

| Major/Minor | Minor2 | Minor1 | | | Major1 | | | Major2 | | | | |
|----------------------|--------|--------|-------|-------|--------|-------|------|--------|---|------|---|---|
| Conflicting Flow All | 275 | 271 | 112 | 274 | 263 | 136 | 112 | 0 | 0 | 144 | 0 | 0 |
| Stage 1 | 121 | 121 | - | 141 | 141 | - | - | - | - | - | - | - |
| Stage 2 | 154 | 150 | - | 133 | 122 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.26 | 7.19 | 6.5 | 6.22 | 4.1 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.354 | 3.581 | 4 | 3.318 | 2.2 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 681 | 639 | 930 | 664 | 646 | 913 | 1490 | - | - | 1451 | - | - |
| Stage 1 | 888 | 800 | - | 845 | 784 | - | - | - | - | - | - | - |
| Stage 2 | 853 | 777 | - | 854 | 799 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | - | - | - |
| Mov Cap-1 Maneuver | 657 | 635 | 928 | 643 | 641 | 911 | 1489 | - | - | 1450 | - | - |
| Mov Cap-2 Maneuver | 657 | 635 | - | 643 | 641 | - | - | - | - | - | - | - |
| Stage 1 | 885 | 797 | - | 842 | 782 | - | - | - | - | - | - | - |
| Stage 2 | 826 | 775 | - | 827 | 796 | - | - | - | - | - | - | - |

| Approach | EB | WB | | | NB | | | SB | | |
|-----------------------|-------|------|-----|-------|-------|-------|-----|-----|--|--|
| HCM Control Delay, s | 9.7 | 10.5 | | | 0.2 | | | 0.4 | | |
| HCM LOS | A | B | | | | | | | | |
| <hr/> | | | | | | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | WBLn1 | SBL | SBT | SBR | | |
| Capacity (veh/h) | 1489 | - | - | 787 | 717 | 1450 | - | - | | |
| HCM Lane V/C Ratio | 0.002 | - | - | 0.035 | 0.091 | 0.004 | - | - | | |
| HCM Control Delay (s) | 7.4 | - | - | 9.7 | 10.5 | 7.5 | - | - | | |
| HCM Lane LOS | A | - | - | A | B | A | - | - | | |
| HCM 95th %tile Q(veh) | 0 | - | - | 0.1 | 0.3 | 0 | - | - | | |

Dillon Drive at Lesperance Road
Tecumseh, Ontario

Total Traffic 2025, PM Peak
Existing Geometric Configuration

Intersection

Int Delay, s/veh 2.6

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 3 | 11 | 19 | 20 | 12 | 10 | 21 | 163 | 31 | 11 | 140 | 2 |
| Future Vol, veh/h | 3 | 11 | 19 | 20 | 12 | 10 | 21 | 163 | 31 | 11 | 140 | 2 |
| Conflicting Peds, #/hr | 2 | 0 | 2 | 10 | 0 | 10 | 12 | 0 | 12 | 6 | 0 | 6 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | 450 | - | - | 100 | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 |
| Heavy Vehicles, % | 0 | 0 | 6 | 9 | 0 | 2 | 0 | 2 | 2 | 0 | 4 | 0 |
| Mvmt Flow | 4 | 13 | 23 | 24 | 14 | 12 | 25 | 196 | 37 | 13 | 169 | 2 |

| Major/Minor | Minor2 | Minor1 | | | Major1 | | | Major2 | | | | |
|----------------------|--------|--------|-------|-------|--------|-------|------|--------|---|------|---|---|
| Conflicting Flow All | 496 | 503 | 192 | 501 | 486 | 237 | 183 | 0 | 0 | 245 | 0 | 0 |
| Stage 1 | 208 | 208 | - | 277 | 277 | - | - | - | - | - | - | - |
| Stage 2 | 288 | 295 | - | 224 | 209 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.26 | 7.19 | 6.5 | 6.22 | 4.1 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.354 | 3.581 | 4 | 3.318 | 2.2 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 487 | 474 | 839 | 469 | 484 | 802 | 1404 | - | - | 1333 | - | - |
| Stage 1 | 799 | 734 | - | 714 | 685 | - | - | - | - | - | - | - |
| Stage 2 | 724 | 673 | - | 763 | 733 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | - | - | - |
| Mov Cap-1 Maneuver | 450 | 452 | 823 | 428 | 461 | 787 | 1390 | - | - | 1319 | - | - |
| Mov Cap-2 Maneuver | 450 | 452 | - | 428 | 461 | - | - | - | - | - | - | - |
| Stage 1 | 777 | 719 | - | 694 | 666 | - | - | - | - | - | - | - |
| Stage 2 | 679 | 654 | - | 715 | 718 | - | - | - | - | - | - | - |

| Approach | EB | WB | | | NB | | | SB | | | | |
|-----------------------|-------|------|-----|-------|-------|------|-----|-----|--|--|--|--|
| HCM Control Delay, s | 11.3 | 13.2 | | | 0.7 | | | 0.6 | | | | |
| HCM LOS | B | B | | | | | | | | | | |
| <hr/> | | | | | | | | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | WBLn1 | SBL | SBT | SBR | | | | |
| Capacity (veh/h) | 1390 | - | - | 610 | 491 | 1319 | - | - | | | | |
| HCM Lane V/C Ratio | 0.018 | - | - | 0.065 | 0.103 | 0.01 | - | - | | | | |
| HCM Control Delay (s) | 7.6 | - | - | 11.3 | 13.2 | 7.8 | - | - | | | | |
| HCM Lane LOS | A | - | - | B | B | A | - | - | | | | |
| HCM 95th %tile Q(veh) | 0.1 | - | - | 0.2 | 0.3 | 0 | - | - | | | | |

Intersection

Int Delay, s/veh 2.6

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↔ | | | ↔ | | | ↑ | ↑ | | ↑ | ↑ | |
| Traffic Vol, veh/h | 4 | 6 | 16 | 32 | 2 | 19 | 4 | 127 | 16 | 5 | 109 | 4 |
| Future Vol, veh/h | 4 | 6 | 16 | 32 | 2 | 19 | 4 | 127 | 16 | 5 | 109 | 4 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | 450 | - | - | 100 | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 0 | 0 | 6 | 9 | 0 | 2 | 0 | 2 | 2 | 0 | 4 | 0 |
| Mvmt Flow | 4 | 7 | 17 | 35 | 2 | 21 | 4 | 138 | 17 | 5 | 118 | 4 |

| Major/Minor | Minor2 | Minor1 | | | Major1 | | | Major2 | | | | |
|----------------------|--------|--------|-------|-------|--------|-------|------|--------|---|------|---|---|
| Conflicting Flow All | 298 | 295 | 122 | 299 | 289 | 149 | 123 | 0 | 0 | 156 | 0 | 0 |
| Stage 1 | 131 | 131 | - | 156 | 156 | - | - | - | - | - | - | - |
| Stage 2 | 167 | 164 | - | 143 | 133 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.26 | 7.19 | 6.5 | 6.22 | 4.1 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.354 | 3.581 | 4 | 3.318 | 2.2 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 658 | 620 | 918 | 640 | 624 | 898 | 1477 | - | - | 1436 | - | - |
| Stage 1 | 877 | 792 | - | 830 | 772 | - | - | - | - | - | - | - |
| Stage 2 | 840 | 766 | - | 843 | 790 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | - | - | - |
| Mov Cap-1 Maneuver | 637 | 615 | 916 | 619 | 619 | 896 | 1476 | - | - | 1435 | - | - |
| Mov Cap-2 Maneuver | 637 | 615 | - | 619 | 619 | - | - | - | - | - | - | - |
| Stage 1 | 873 | 789 | - | 827 | 769 | - | - | - | - | - | - | - |
| Stage 2 | 815 | 763 | - | 817 | 787 | - | - | - | - | - | - | - |

| Approach | EB | WB | | | NB | | SB | |
|-----------------------|-------|------|-----|-------|-------|-------|-----|-----|
| HCM Control Delay, s | 9.8 | 10.6 | | | 0.2 | | 0.3 | |
| HCM LOS | A | B | | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | WBLn1 | SBL | SBT | SBR |
| Capacity (veh/h) | 1476 | - | - | 776 | 696 | 1435 | - | - |
| HCM Lane V/C Ratio | 0.003 | - | - | 0.036 | 0.083 | 0.004 | - | - |
| HCM Control Delay (s) | 7.4 | - | - | 9.8 | 10.6 | 7.5 | - | - |
| HCM Lane LOS | A | - | - | A | B | A | - | - |
| HCM 95th %tile Q(veh) | 0 | - | - | 0.1 | 0.3 | 0 | - | - |

| Intersection | | | | | | | | | | | | |
|--------------------------|--------|--------|-------|--------|-------|--------|------|------|------|------|------|------|
| Int Delay, s/veh | 2.6 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ |
| Traffic Vol, veh/h | 4 | 10 | 21 | 19 | 11 | 10 | 24 | 180 | 26 | 10 | 154 | 2 |
| Future Vol, veh/h | 4 | 10 | 21 | 19 | 11 | 10 | 24 | 180 | 26 | 10 | 154 | 2 |
| Conflicting Peds, #/hr | 2 | 0 | 2 | 10 | 0 | 10 | 12 | 0 | 12 | 6 | 0 | 6 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | 450 | - | - | 100 | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 |
| Heavy Vehicles, % | 0 | 0 | 6 | 9 | 0 | 2 | 0 | 2 | 2 | 0 | 4 | 0 |
| Mvmt Flow | 5 | 12 | 25 | 23 | 13 | 12 | 29 | 217 | 31 | 12 | 186 | 2 |
| Major/Minor | Minor2 | Minor1 | | Major1 | | Major2 | | | | | | |
| Conflicting Flow All | 536 | 541 | 209 | 543 | 527 | 255 | 200 | 0 | 0 | 260 | 0 | 0 |
| Stage 1 | 223 | 223 | - | 303 | 303 | - | - | - | - | - | - | - |
| Stage 2 | 313 | 318 | - | 240 | 224 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.26 | 7.19 | 6.5 | 6.22 | 4.1 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.354 | 3.581 | 4 | 3.318 | 2.2 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 459 | 451 | 821 | 440 | 459 | 784 | 1384 | - | - | 1316 | - | - |
| Stage 1 | 784 | 723 | - | 692 | 667 | - | - | - | - | - | - | - |
| Stage 2 | 702 | 657 | - | 748 | 722 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | - | - | - |
| Mov Cap-1 Maneuver | 423 | 429 | 806 | 400 | 437 | 769 | 1370 | - | - | 1303 | - | - |
| Mov Cap-2 Maneuver | 423 | 429 | - | 400 | 437 | - | - | - | - | - | - | - |
| Stage 1 | 760 | 709 | - | 671 | 646 | - | - | - | - | - | - | - |
| Stage 2 | 657 | 637 | - | 700 | 708 | - | - | - | - | - | - | - |
| Approach | EB | WB | | NB | | SB | | | | | | |
| HCM Control Delay, s | 11.5 | 13.6 | | 0.8 | | 0.5 | | | | | | |
| HCM LOS | B | B | | | | | | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | WBLn1 | SBL | SBT | SBR | | | | |
| Capacity (veh/h) | 1370 | - | - | 595 | 467 | 1303 | - | - | | | | |
| HCM Lane V/C Ratio | 0.021 | - | - | 0.071 | 0.103 | 0.009 | - | - | | | | |
| HCM Control Delay (s) | 7.7 | - | - | 11.5 | 13.6 | 7.8 | - | - | | | | |
| HCM Lane LOS | A | - | - | B | B | A | - | - | | | | |
| HCM 95th %tile Q(veh) | 0.1 | - | - | 0.2 | 0.3 | 0 | - | - | | | | |

Dillon Drive at Lesperance Road
Tecumseh, Ontario

Total Traffic 2030, AM Peak
Existing Geometric Configuration

Intersection

Int Delay, s/veh 2.9

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↔ | | | ↔ | | | ↑ | ↑ | | ↑ | ↑ | |
| Traffic Vol, veh/h | 4 | 7 | 16 | 39 | 3 | 23 | 4 | 127 | 18 | 5 | 109 | 4 |
| Future Vol, veh/h | 4 | 7 | 16 | 39 | 3 | 23 | 4 | 127 | 18 | 5 | 109 | 4 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | 450 | - | - | 100 | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 0 | 0 | 6 | 9 | 0 | 2 | 0 | 2 | 2 | 0 | 4 | 0 |
| Mvmt Flow | 4 | 8 | 17 | 42 | 3 | 25 | 4 | 138 | 20 | 5 | 118 | 4 |

| Major/Minor | Minor2 | Minor1 | | | Major1 | | | Major2 | | | | |
|----------------------|--------|--------|-------|-------|--------|-------|------|--------|---|------|---|---|
| Conflicting Flow All | 302 | 298 | 122 | 301 | 290 | 150 | 123 | 0 | 0 | 159 | 0 | 0 |
| Stage 1 | 131 | 131 | - | 157 | 157 | - | - | - | - | - | - | - |
| Stage 2 | 171 | 167 | - | 144 | 133 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.26 | 7.19 | 6.5 | 6.22 | 4.1 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.354 | 3.581 | 4 | 3.318 | 2.2 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 654 | 617 | 918 | 638 | 624 | 896 | 1477 | - | - | 1433 | - | - |
| Stage 1 | 877 | 792 | - | 829 | 772 | - | - | - | - | - | - | - |
| Stage 2 | 836 | 764 | - | 842 | 790 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | - | - | - |
| Mov Cap-1 Maneuver | 629 | 612 | 916 | 616 | 619 | 894 | 1476 | - | - | 1432 | - | - |
| Mov Cap-2 Maneuver | 629 | 612 | - | 616 | 619 | - | - | - | - | - | - | - |
| Stage 1 | 873 | 789 | - | 826 | 769 | - | - | - | - | - | - | - |
| Stage 2 | 806 | 761 | - | 815 | 787 | - | - | - | - | - | - | - |

| Approach | EB | WB | | | NB | | | SB | | | | |
|-----------------------|-------|------|-----|-------|-------|-------|-----|-----|--|--|--|--|
| HCM Control Delay, s | 9.9 | 10.8 | | | 0.2 | | | 0.3 | | | | |
| HCM LOS | A | B | | | | | | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | WBLn1 | SBL | SBT | SBR | | | | |
| Capacity (veh/h) | 1476 | - | - | 766 | 692 | 1432 | - | - | | | | |
| HCM Lane V/C Ratio | 0.003 | - | - | 0.038 | 0.102 | 0.004 | - | - | | | | |
| HCM Control Delay (s) | 7.4 | - | - | 9.9 | 10.8 | 7.5 | - | - | | | | |
| HCM Lane LOS | A | - | - | A | B | A | - | - | | | | |
| HCM 95th %tile Q(veh) | 0 | - | - | 0.1 | 0.3 | 0 | - | - | | | | |

Dillon Drive at Lesperance Road
Tecumseh, Ontario

Total Traffic 2030, PM Peak
Existing Geometric Configuration

Intersection

Int Delay, s/veh 2.8

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 4 | 12 | 21 | 22 | 13 | 11 | 24 | 180 | 33 | 12 | 154 | 2 |
| Future Vol, veh/h | 4 | 12 | 21 | 22 | 13 | 11 | 24 | 180 | 33 | 12 | 154 | 2 |
| Conflicting Peds, #/hr | 2 | 0 | 2 | 10 | 0 | 10 | 12 | 0 | 12 | 6 | 0 | 6 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None |
| Storage Length | - | - | - | - | - | - | 450 | - | - | 100 | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 | 83 |
| Heavy Vehicles, % | 0 | 0 | 6 | 9 | 0 | 2 | 0 | 2 | 2 | 0 | 4 | 0 |
| Mvmt Flow | 5 | 14 | 25 | 27 | 16 | 13 | 29 | 217 | 40 | 14 | 186 | 2 |

| Major/Minor | Minor2 | Minor1 | | | Major1 | | | Major2 | | | | |
|----------------------|--------|--------|-------|-------|--------|-------|------|--------|---|------|---|---|
| Conflicting Flow All | 547 | 554 | 209 | 552 | 535 | 259 | 200 | 0 | 0 | 269 | 0 | 0 |
| Stage 1 | 227 | 227 | - | 307 | 307 | - | - | - | - | - | - | - |
| Stage 2 | 320 | 327 | - | 245 | 228 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.26 | 7.19 | 6.5 | 6.22 | 4.1 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.19 | 5.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.354 | 3.581 | 4 | 3.318 | 2.2 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 451 | 443 | 821 | 434 | 454 | 780 | 1384 | - | - | 1306 | - | - |
| Stage 1 | 780 | 720 | - | 688 | 665 | - | - | - | - | - | - | - |
| Stage 2 | 696 | 651 | - | 743 | 719 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | - | - | - |
| Mov Cap-1 Maneuver | 413 | 420 | 806 | 392 | 431 | 766 | 1370 | - | - | 1293 | - | - |
| Mov Cap-2 Maneuver | 413 | 420 | - | 392 | 431 | - | - | - | - | - | - | - |
| Stage 1 | 756 | 705 | - | 667 | 644 | - | - | - | - | - | - | - |
| Stage 2 | 648 | 631 | - | 691 | 704 | - | - | - | - | - | - | - |

| Approach | EB | WB | | | NB | | SB | |
|-----------------------|-------|-----|-----|-------|-------|-------|-----|-----|
| HCM Control Delay, s | 11.8 | 14 | | | 0.8 | | 0.6 | |
| HCM LOS | B | B | | | | | | |
| <hr/> | | | | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | WBLn1 | SBL | SBT | SBR |
| Capacity (veh/h) | 1370 | - | - | 575 | 457 | 1293 | - | - |
| HCM Lane V/C Ratio | 0.021 | - | - | 0.078 | 0.121 | 0.011 | - | - |
| HCM Control Delay (s) | 7.7 | - | - | 11.8 | 14 | 7.8 | - | - |
| HCM Lane LOS | A | - | - | B | B | A | - | - |
| HCM 95th %tile Q(veh) | 0.1 | - | - | 0.3 | 0.4 | 0 | - | - |

Dillon Drive at St. Pierre Street
Tecumseh, Ontario

Existing Traffic, AM Peak
Existing Geometric Configuration

Intersection

Intersection Delay, s/veh 7.2
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | | | ↔ | | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 2 | 22 | 4 | 1 | 28 | 0 | 8 | 5 | 1 | 1 | 8 | 5 |
| Future Vol, veh/h | 2 | 22 | 4 | 1 | 28 | 0 | 8 | 5 | 1 | 1 | 8 | 5 |
| Peak Hour Factor | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 22 | 40 | 0 | 4 | 0 |
| Mvmt Flow | 3 | 30 | 5 | 1 | 38 | 0 | 11 | 7 | 1 | 1 | 11 | 7 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 7.1 | | | 7.2 | | | 7.3 | | | 7 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 57% | 7% | 3% | 7% |
| Vol Thru, % | 36% | 79% | 97% | 57% |
| Vol Right, % | 7% | 14% | 0% | 36% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 14 | 28 | 29 | 14 |
| LT Vol | 8 | 2 | 1 | 1 |
| Through Vol | 5 | 22 | 28 | 8 |
| RT Vol | 1 | 4 | 0 | 5 |
| Lane Flow Rate | 19 | 38 | 40 | 19 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.022 | 0.042 | 0.044 | 0.021 |
| Departure Headway (Hd) | 4.121 | 3.925 | 4.002 | 3.849 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 866 | 912 | 895 | 927 |
| Service Time | 2.157 | 1.95 | 2.027 | 1.886 |
| HCM Lane V/C Ratio | 0.022 | 0.042 | 0.045 | 0.02 |
| HCM Control Delay | 7.3 | 7.1 | 7.2 | 7 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0.1 | 0.1 | 0.1 |

Dillon Drive at St. Pierre Street
Tecumseh, Ontario

Existing Traffic, PM Peak
Existing Geometric Configuration

Intersection

Intersection Delay, s/veh 7.2
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | | | ↔ | | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 5 | 30 | 2 | 2 | 24 | 2 | 7 | 4 | 4 | 1 | 5 | 3 |
| Future Vol, veh/h | 5 | 30 | 2 | 2 | 24 | 2 | 7 | 4 | 4 | 1 | 5 | 3 |
| Peak Hour Factor | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 22 | 40 | 0 | 4 | 0 |
| Mvmt Flow | 7 | 41 | 3 | 3 | 32 | 3 | 9 | 5 | 5 | 1 | 7 | 4 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 7.2 | | | 7.2 | | | 7.1 | | | 7 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 47% | 14% | 7% | 11% |
| Vol Thru, % | 27% | 81% | 86% | 56% |
| Vol Right, % | 27% | 5% | 7% | 33% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 15 | 37 | 28 | 9 |
| LT Vol | 7 | 5 | 2 | 1 |
| Through Vol | 4 | 30 | 24 | 5 |
| RT Vol | 4 | 2 | 2 | 3 |
| Lane Flow Rate | 20 | 50 | 38 | 12 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.022 | 0.055 | 0.042 | 0.013 |
| Departure Headway (Hd) | 3.995 | 3.98 | 3.965 | 3.889 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 893 | 901 | 904 | 916 |
| Service Time | 2.033 | 1.999 | 1.986 | 1.93 |
| HCM Lane V/C Ratio | 0.022 | 0.055 | 0.042 | 0.013 |
| HCM Control Delay | 7.1 | 7.2 | 7.2 | 7 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0.2 | 0.1 | 0 |

Dillon Drive at St. Pierre Street
Tecumseh, Ontario

Existing + Site Generated Traffic, AM Peak
Existing Geometric Configuration

Intersection

Intersection Delay, s/veh 7.2
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | | | ↔ | | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 2 | 25 | 4 | 1 | 40 | 0 | 8 | 5 | 1 | 1 | 8 | 5 |
| Future Vol, veh/h | 2 | 25 | 4 | 1 | 40 | 0 | 8 | 5 | 1 | 1 | 8 | 5 |
| Peak Hour Factor | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 22 | 40 | 0 | 4 | 0 |
| Mvmt Flow | 3 | 34 | 5 | 1 | 55 | 0 | 11 | 7 | 1 | 1 | 11 | 7 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 7.2 | | | 7.3 | | | 7.3 | | | 7 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 57% | 6% | 2% | 7% |
| Vol Thru, % | 36% | 81% | 98% | 57% |
| Vol Right, % | 7% | 13% | 0% | 36% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 14 | 31 | 41 | 14 |
| LT Vol | 8 | 2 | 1 | 1 |
| Through Vol | 5 | 25 | 40 | 8 |
| RT Vol | 1 | 4 | 0 | 5 |
| Lane Flow Rate | 19 | 42 | 56 | 19 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.022 | 0.047 | 0.062 | 0.021 |
| Departure Headway (Hd) | 4.158 | 3.944 | 4.004 | 3.886 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 857 | 907 | 894 | 916 |
| Service Time | 2.202 | 1.972 | 2.029 | 1.931 |
| HCM Lane V/C Ratio | 0.022 | 0.046 | 0.063 | 0.021 |
| HCM Control Delay | 7.3 | 7.2 | 7.3 | 7 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0.1 | 0.2 | 0.1 |

Intersection

Intersection Delay, s/veh 7.2
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↖ | | | ↖ | | | ↖ | | | ↖ | |
| Traffic Vol, veh/h | 5 | 41 | 2 | 2 | 30 | 2 | 7 | 4 | 4 | 1 | 5 | 3 |
| Future Vol, veh/h | 5 | 41 | 2 | 2 | 30 | 2 | 7 | 4 | 4 | 1 | 5 | 3 |
| Peak Hour Factor | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 22 | 40 | 0 | 4 | 0 |
| Mvmt Flow | 7 | 55 | 3 | 3 | 41 | 3 | 9 | 5 | 5 | 1 | 7 | 4 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 7.3 | | | 7.2 | | | 7.2 | | | 7 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 47% | 10% | 6% | 11% |
| Vol Thru, % | 27% | 85% | 88% | 56% |
| Vol Right, % | 27% | 4% | 6% | 33% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 15 | 48 | 34 | 9 |
| LT Vol | 7 | 5 | 2 | 1 |
| Through Vol | 4 | 41 | 30 | 5 |
| RT Vol | 4 | 2 | 2 | 3 |
| Lane Flow Rate | 20 | 65 | 46 | 12 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.023 | 0.072 | 0.051 | 0.013 |
| Departure Headway (Hd) | 4.035 | 3.987 | 3.982 | 3.93 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 882 | 899 | 899 | 905 |
| Service Time | 2.083 | 2.009 | 2.008 | 1.981 |
| HCM Lane V/C Ratio | 0.023 | 0.072 | 0.051 | 0.013 |
| HCM Control Delay | 7.2 | 7.3 | 7.2 | 7 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0.2 | 0.2 | 0 |

Intersection

Intersection Delay, s/veh 7.2
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | | | ↔ | | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 2 | 25 | 5 | 1 | 32 | 0 | 9 | 6 | 1 | 1 | 9 | 6 |
| Future Vol, veh/h | 2 | 25 | 5 | 1 | 32 | 0 | 9 | 6 | 1 | 1 | 9 | 6 |
| Peak Hour Factor | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 22 | 40 | 0 | 4 | 0 |
| Mvmt Flow | 3 | 34 | 7 | 1 | 44 | 0 | 12 | 8 | 1 | 1 | 12 | 8 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 7.2 | | | 7.3 | | | 7.3 | | | 7 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 56% | 6% | 3% | 6% |
| Vol Thru, % | 38% | 78% | 97% | 56% |
| Vol Right, % | 6% | 16% | 0% | 38% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 16 | 32 | 33 | 16 |
| LT Vol | 9 | 2 | 1 | 1 |
| Through Vol | 6 | 25 | 32 | 9 |
| RT Vol | 1 | 5 | 0 | 6 |
| Lane Flow Rate | 22 | 44 | 45 | 22 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.025 | 0.048 | 0.05 | 0.023 |
| Departure Headway (Hd) | 4.145 | 3.927 | 4.013 | 3.857 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 860 | 911 | 891 | 924 |
| Service Time | 2.186 | 1.955 | 2.041 | 1.899 |
| HCM Lane V/C Ratio | 0.026 | 0.048 | 0.051 | 0.024 |
| HCM Control Delay | 7.3 | 7.2 | 7.3 | 7 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0.2 | 0.2 | 0.1 |

Intersection

Intersection Delay, s/veh 7.2
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 6 | 34 | 2 | 2 | 27 | 2 | 8 | 5 | 5 | 1 | 6 | 3 |
| Future Vol, veh/h | 6 | 34 | 2 | 2 | 27 | 2 | 8 | 5 | 5 | 1 | 6 | 3 |
| Peak Hour Factor | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 22 | 40 | 0 | 4 | 0 |
| Mvmt Flow | 8 | 46 | 3 | 3 | 36 | 3 | 11 | 7 | 7 | 1 | 8 | 4 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | WB | | | NB | | | SB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 7.3 | | | 7.2 | | | 7.2 | | | 7 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 44% | 14% | 6% | 10% |
| Vol Thru, % | 28% | 81% | 87% | 60% |
| Vol Right, % | 28% | 5% | 6% | 30% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 18 | 42 | 31 | 10 |
| LT Vol | 8 | 6 | 2 | 1 |
| Through Vol | 5 | 34 | 27 | 6 |
| RT Vol | 5 | 2 | 2 | 3 |
| Lane Flow Rate | 24 | 57 | 42 | 14 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.027 | 0.063 | 0.046 | 0.015 |
| Departure Headway (Hd) | 4.002 | 3.998 | 3.983 | 3.928 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 890 | 896 | 899 | 906 |
| Service Time | 2.047 | 2.021 | 2.01 | 1.975 |
| HCM Lane V/C Ratio | 0.027 | 0.064 | 0.047 | 0.015 |
| HCM Control Delay | 7.2 | 7.3 | 7.2 | 7 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0.2 | 0.1 | 0 |

Dillon Drive at St. Pierre Street
Tecumseh, Ontario

Total Traffic 2025, AM Peak
Existing Geometric Configuration

Intersection

Intersection Delay, s/veh 7.2
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | | | ↔ | | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 2 | 28 | 5 | 1 | 44 | 0 | 9 | 6 | 1 | 1 | 9 | 6 |
| Future Vol, veh/h | 2 | 28 | 5 | 1 | 44 | 0 | 9 | 6 | 1 | 1 | 9 | 6 |
| Peak Hour Factor | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 22 | 40 | 0 | 4 | 0 |
| Mvmt Flow | 3 | 38 | 7 | 1 | 60 | 0 | 12 | 8 | 1 | 1 | 12 | 8 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | | EB | | | SB | | | NB | |
| Opposing Lanes | 1 | | | | 1 | | | 1 | | | 1 | |
| Conflicting Approach Left | SB | | | | NB | | | EB | | | WB | |
| Conflicting Lanes Left | 1 | | | | 1 | | | 1 | | | 1 | |
| Conflicting Approach Right | NB | | | | SB | | | WB | | | EB | |
| Conflicting Lanes Right | 1 | | | | 1 | | | 1 | | | 1 | |
| HCM Control Delay | 7.2 | | | | 7.3 | | | 7.3 | | | 7 | |
| HCM LOS | A | | | | A | | | A | | | A | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 56% | 6% | 2% | 6% |
| Vol Thru, % | 38% | 80% | 98% | 56% |
| Vol Right, % | 6% | 14% | 0% | 38% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 16 | 35 | 45 | 16 |
| LT Vol | 9 | 2 | 1 | 1 |
| Through Vol | 6 | 28 | 44 | 9 |
| RT Vol | 1 | 5 | 0 | 6 |
| Lane Flow Rate | 22 | 48 | 62 | 22 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.025 | 0.053 | 0.069 | 0.024 |
| Departure Headway (Hd) | 4.182 | 3.947 | 4.015 | 3.894 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 851 | 905 | 891 | 913 |
| Service Time | 2.233 | 1.98 | 2.045 | 1.946 |
| HCM Lane V/C Ratio | 0.026 | 0.053 | 0.07 | 0.024 |
| HCM Control Delay | 7.3 | 7.2 | 7.3 | 7 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0.2 | 0.2 | 0.1 |

Dillon Drive at St. Pierre Street
Tecumseh, Ontario

Total Traffic 2025, PM Peak
Existing Geometric Configuration

Intersection

Intersection Delay, s/veh 7.3
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 6 | 45 | 2 | 2 | 33 | 2 | 8 | 5 | 5 | 1 | 6 | 3 |
| Future Vol, veh/h | 6 | 45 | 2 | 2 | 33 | 2 | 8 | 5 | 5 | 1 | 6 | 3 |
| Peak Hour Factor | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 22 | 40 | 0 | 4 | 0 |
| Mvmt Flow | 8 | 61 | 3 | 3 | 45 | 3 | 11 | 7 | 7 | 1 | 8 | 4 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | WB | | | NB | | | SB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 7.4 | | | 7.3 | | | 7.2 | | | 7.1 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 44% | 11% | 5% | 10% |
| Vol Thru, % | 28% | 85% | 89% | 60% |
| Vol Right, % | 28% | 4% | 5% | 30% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 18 | 53 | 37 | 10 |
| LT Vol | 8 | 6 | 2 | 1 |
| Through Vol | 5 | 45 | 33 | 6 |
| RT Vol | 5 | 2 | 2 | 3 |
| Lane Flow Rate | 24 | 72 | 50 | 14 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.027 | 0.08 | 0.056 | 0.015 |
| Departure Headway (Hd) | 4.042 | 4.004 | 3.999 | 3.969 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 879 | 895 | 895 | 894 |
| Service Time | 2.099 | 2.03 | 2.028 | 2.027 |
| HCM Lane V/C Ratio | 0.027 | 0.08 | 0.056 | 0.016 |
| HCM Control Delay | 7.2 | 7.4 | 7.3 | 7.1 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0.3 | 0.2 | 0 |

Intersection

Intersection Delay, s/veh 7.2
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 2 | 27 | 5 | 1 | 35 | 0 | 10 | 6 | 1 | 1 | 10 | 6 |
| Future Vol, veh/h | 2 | 27 | 5 | 1 | 35 | 0 | 10 | 6 | 1 | 1 | 10 | 6 |
| Peak Hour Factor | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 22 | 40 | 0 | 4 | 0 |
| Mvmt Flow | 3 | 37 | 7 | 1 | 48 | 0 | 14 | 8 | 1 | 1 | 14 | 8 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | WB | | | NB | | | SB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 7.2 | | | 7.3 | | | 7.3 | | | 7 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 59% | 6% | 3% | 6% |
| Vol Thru, % | 35% | 79% | 97% | 59% |
| Vol Right, % | 6% | 15% | 0% | 35% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 17 | 34 | 36 | 17 |
| LT Vol | 10 | 2 | 1 | 1 |
| Through Vol | 6 | 27 | 35 | 10 |
| RT Vol | 1 | 5 | 0 | 6 |
| Lane Flow Rate | 23 | 47 | 49 | 23 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.027 | 0.051 | 0.055 | 0.025 |
| Departure Headway (Hd) | 4.166 | 3.943 | 4.022 | 3.883 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 855 | 907 | 890 | 917 |
| Service Time | 2.21 | 1.972 | 2.051 | 1.929 |
| HCM Lane V/C Ratio | 0.027 | 0.052 | 0.055 | 0.025 |
| HCM Control Delay | 7.3 | 7.2 | 7.3 | 7 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0.2 | 0.2 | 0.1 |

Intersection

Intersection Delay, s/veh 7.2
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | | | ↔ | | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 6 | 37 | 2 | 2 | 30 | 2 | 9 | 5 | 5 | 1 | 6 | 4 |
| Future Vol, veh/h | 6 | 37 | 2 | 2 | 30 | 2 | 9 | 5 | 5 | 1 | 6 | 4 |
| Peak Hour Factor | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 22 | 40 | 0 | 4 | 0 |
| Mvmt Flow | 8 | 50 | 3 | 3 | 41 | 3 | 12 | 7 | 7 | 1 | 8 | 5 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 7.3 | | | 7.2 | | | 7.2 | | | 7 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 47% | 13% | 6% | 9% |
| Vol Thru, % | 26% | 82% | 88% | 55% |
| Vol Right, % | 26% | 4% | 6% | 36% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 19 | 45 | 34 | 11 |
| LT Vol | 9 | 6 | 2 | 1 |
| Through Vol | 5 | 37 | 30 | 6 |
| RT Vol | 5 | 2 | 2 | 4 |
| Lane Flow Rate | 26 | 61 | 46 | 15 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.029 | 0.068 | 0.051 | 0.016 |
| Departure Headway (Hd) | 4.033 | 4.005 | 3.993 | 3.904 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 882 | 894 | 896 | 910 |
| Service Time | 2.082 | 2.031 | 2.022 | 1.956 |
| HCM Lane V/C Ratio | 0.029 | 0.068 | 0.051 | 0.016 |
| HCM Control Delay | 7.2 | 7.3 | 7.2 | 7 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0.2 | 0.2 | 0 |

Intersection

Intersection Delay, s/veh 7.2
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | | | ↔ | | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 2 | 30 | 5 | 1 | 47 | 0 | 10 | 6 | 1 | 1 | 10 | 6 |
| Future Vol, veh/h | 2 | 30 | 5 | 1 | 47 | 0 | 10 | 6 | 1 | 1 | 10 | 6 |
| Peak Hour Factor | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 22 | 40 | 0 | 4 | 0 |
| Mvmt Flow | 2 | 30 | 5 | 1 | 47 | 0 | 10 | 6 | 1 | 1 | 10 | 6 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 7.1 | | | 7.2 | | | 7.3 | | | 7 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 59% | 5% | 2% | 6% |
| Vol Thru, % | 35% | 81% | 98% | 59% |
| Vol Right, % | 6% | 14% | 0% | 35% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 17 | 37 | 48 | 17 |
| LT Vol | 10 | 2 | 1 | 1 |
| Through Vol | 6 | 30 | 47 | 10 |
| RT Vol | 1 | 5 | 0 | 6 |
| Lane Flow Rate | 17 | 37 | 48 | 17 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.02 | 0.04 | 0.053 | 0.018 |
| Departure Headway (Hd) | 4.143 | 3.925 | 3.991 | 3.861 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 862 | 912 | 898 | 924 |
| Service Time | 2.179 | 1.949 | 2.012 | 1.898 |
| HCM Lane V/C Ratio | 0.02 | 0.041 | 0.053 | 0.018 |
| HCM Control Delay | 7.3 | 7.1 | 7.2 | 7 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0.1 | 0.2 | 0.1 |

Intersection

Intersection Delay, s/veh 7.3
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 6 | 48 | 2 | 2 | 36 | 2 | 9 | 5 | 5 | 1 | 6 | 4 |
| Future Vol, veh/h | 6 | 48 | 2 | 2 | 36 | 2 | 9 | 5 | 5 | 1 | 6 | 4 |
| Peak Hour Factor | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 22 | 40 | 0 | 4 | 0 |
| Mvmt Flow | 8 | 65 | 3 | 3 | 49 | 3 | 12 | 7 | 7 | 1 | 8 | 5 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | WB | | | NB | | | SB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 7.4 | | | 7.3 | | | 7.3 | | | 7.1 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 47% | 11% | 5% | 9% |
| Vol Thru, % | 26% | 86% | 90% | 55% |
| Vol Right, % | 26% | 4% | 5% | 36% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 19 | 56 | 40 | 11 |
| LT Vol | 9 | 6 | 2 | 1 |
| Through Vol | 5 | 48 | 36 | 6 |
| RT Vol | 5 | 2 | 2 | 4 |
| Lane Flow Rate | 26 | 76 | 54 | 15 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.029 | 0.084 | 0.06 | 0.016 |
| Departure Headway (Hd) | 4.071 | 4.011 | 4.007 | 3.943 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 872 | 892 | 892 | 899 |
| Service Time | 2.13 | 2.039 | 2.039 | 2.004 |
| HCM Lane V/C Ratio | 0.03 | 0.085 | 0.061 | 0.017 |
| HCM Control Delay | 7.3 | 7.4 | 7.3 | 7.1 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0.3 | 0.2 | 0 |

Dillon Drive at Site Access
Tecumseh, Ontario

Existing + Site Generated Traffic, AM Peak
Proposed Geometric Configuration

Intersection

Int Delay, s/veh 2.9

| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
|--------------------------|------|------|------|------|------|------|
| Lane Configurations | ↑ | | ↔ | ↔ | | |
| Traffic Vol, veh/h | 22 | 3 | 4 | 25 | 12 | 10 |
| Future Vol, veh/h | 22 | 3 | 4 | 25 | 12 | 10 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 0 | 0 | 2 | 0 | 0 |
| Mvmt Flow | 24 | 3 | 4 | 27 | 13 | 11 |

| Major/Minor | Major1 | Major2 | Minor1 | | |
|----------------------|--------|--------|--------|---|----------|
| Conflicting Flow All | 0 | 0 | 27 | 0 | 61 26 |
| Stage 1 | - | - | - | - | 26 - |
| Stage 2 | - | - | - | - | 35 - |
| Critical Hdwy | - | - | 4.1 | - | 6.4 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 3.3 |
| Pot Cap-1 Maneuver | - | - | 1600 | - | 950 1056 |
| Stage 1 | - | - | - | - | 1002 - |
| Stage 2 | - | - | - | - | 993 - |
| Platoon blocked, % | - | - | - | - | - |
| Mov Cap-1 Maneuver | - | - | 1600 | - | 947 1056 |
| Mov Cap-2 Maneuver | - | - | - | - | 947 - |
| Stage 1 | - | - | - | - | 1002 - |
| Stage 2 | - | - | - | - | 990 - |

| Approach | EB | WB | NB |
|----------------------|----|----|-----|
| HCM Control Delay, s | 0 | 1 | 8.7 |
| HCM LOS | | | A |

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
|-----------------------|-------|-----|-----|-------|-----|
| Capacity (veh/h) | 994 | - | - | 1600 | - |
| HCM Lane V/C Ratio | 0.024 | - | - | 0.003 | - |
| HCM Control Delay (s) | 8.7 | - | - | 7.3 | 0 |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th %tile Q(veh) | 0.1 | - | - | 0 | - |

Dillon Drive at Site Access
Tecumseh, Ontario

Existing + Site Generated Traffic, PM Peak
Proposed Geometric Configuration

Intersection

Int Delay, s/veh 2.1

| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
|----------|-----|-----|-----|-----|-----|-----|
|----------|-----|-----|-----|-----|-----|-----|

| | | | | | | |
|--------------------------|------|------|------|------|------|------|
| Lane Configurations | | | | | | |
| Traffic Vol, veh/h | 30 | 12 | 10 | 23 | 6 | 7 |
| Future Vol, veh/h | 30 | 12 | 10 | 23 | 6 | 7 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 0 | 0 | 2 | 0 | 0 |
| Mvmt Flow | 33 | 13 | 11 | 25 | 7 | 8 |

| Major/Minor | Major1 | Major2 | Minor1 |
|-------------|--------|--------|--------|
|-------------|--------|--------|--------|

| | | | | | | |
|----------------------|---|---|------|---|-----|------|
| Conflicting Flow All | 0 | 0 | 46 | 0 | 87 | 40 |
| Stage 1 | - | - | - | - | 40 | - |
| Stage 2 | - | - | - | - | 47 | - |
| Critical Hdwy | - | - | 4.1 | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1575 | - | 919 | 1037 |
| Stage 1 | - | - | - | - | 988 | - |
| Stage 2 | - | - | - | - | 981 | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | - | - | 1575 | - | 913 | 1037 |
| Mov Cap-2 Maneuver | - | - | - | - | 913 | - |
| Stage 1 | - | - | - | - | 988 | - |
| Stage 2 | - | - | - | - | 974 | - |

| Approach | EB | WB | NB |
|----------|----|----|----|
|----------|----|----|----|

| | | | |
|----------------------|---|-----|-----|
| HCM Control Delay, s | 0 | 2.2 | 8.7 |
| HCM LOS | | A | |

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
|-----------------------|-------|-----|-----|-------|-----|
| Capacity (veh/h) | 976 | - | - | 1575 | - |
| HCM Lane V/C Ratio | 0.014 | - | - | 0.007 | - |
| HCM Control Delay (s) | 8.7 | - | - | 7.3 | 0 |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th %tile Q(veh) | 0 | - | - | 0 | - |

Dillon Drive at Site Access
Tecumseh, Ontario

Total Traffic 2025, AM Peak
Proposed Geometric Configuration

Intersection

Int Delay, s/veh 2.7

| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
|--------------------------|------|------|------|------|------|------|
| Lane Configurations | ↑ | | ↔ | ↔ | | |
| Traffic Vol, veh/h | 25 | 3 | 4 | 28 | 12 | 10 |
| Future Vol, veh/h | 25 | 3 | 4 | 28 | 12 | 10 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 0 | 0 | 2 | 0 | 0 |
| Mvmt Flow | 27 | 3 | 4 | 30 | 13 | 11 |

| Major/Minor | Major1 | Major2 | Minor1 | | |
|----------------------|--------|--------|--------|---|----------|
| Conflicting Flow All | 0 | 0 | 30 | 0 | 67 29 |
| Stage 1 | - | - | - | - | 29 - |
| Stage 2 | - | - | - | - | 38 - |
| Critical Hdwy | - | - | 4.1 | - | 6.4 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 3.3 |
| Pot Cap-1 Maneuver | - | - | 1596 | - | 943 1052 |
| Stage 1 | - | - | - | - | 999 - |
| Stage 2 | - | - | - | - | 990 - |
| Platoon blocked, % | - | - | - | - | - |
| Mov Cap-1 Maneuver | - | - | 1596 | - | 940 1052 |
| Mov Cap-2 Maneuver | - | - | - | - | 940 - |
| Stage 1 | - | - | - | - | 999 - |
| Stage 2 | - | - | - | - | 987 - |

| Approach | EB | WB | NB |
|----------------------|----|-----|-----|
| HCM Control Delay, s | 0 | 0.9 | 8.7 |
| HCM LOS | | | A |

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
|-----------------------|-------|-----|-----|-------|-----|
| Capacity (veh/h) | 988 | - | - | 1596 | - |
| HCM Lane V/C Ratio | 0.024 | - | - | 0.003 | - |
| HCM Control Delay (s) | 8.7 | - | - | 7.3 | 0 |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th %tile Q(veh) | 0.1 | - | - | 0 | - |

Dillon Drive at Site Access
Tecumseh, Ontario

Total Traffic 2025, PM Peak
Proposed Geometric Configuration

Intersection

Int Delay, s/veh 2

| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
|----------|-----|-----|-----|-----|-----|-----|
|----------|-----|-----|-----|-----|-----|-----|

| | | | | | | |
|--------------------------|------|------|------|------|------|------|
| Lane Configurations | | | | | | |
| Traffic Vol, veh/h | 34 | 12 | 10 | 26 | 6 | 7 |
| Future Vol, veh/h | 34 | 12 | 10 | 26 | 6 | 7 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 0 | 0 | 2 | 0 | 0 |
| Mvmt Flow | 37 | 13 | 11 | 28 | 7 | 8 |

| Major/Minor | Major1 | Major2 | Minor1 |
|-------------|--------|--------|--------|
|-------------|--------|--------|--------|

| | | | | | | |
|----------------------|---|---|------|---|-----|------|
| Conflicting Flow All | 0 | 0 | 50 | 0 | 94 | 44 |
| Stage 1 | - | - | - | - | 44 | - |
| Stage 2 | - | - | - | - | 50 | - |
| Critical Hdwy | - | - | 4.1 | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1570 | - | 911 | 1032 |
| Stage 1 | - | - | - | - | 984 | - |
| Stage 2 | - | - | - | - | 978 | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | - | - | 1570 | - | 905 | 1032 |
| Mov Cap-2 Maneuver | - | - | - | - | 905 | - |
| Stage 1 | - | - | - | - | 984 | - |
| Stage 2 | - | - | - | - | 971 | - |

| Approach | EB | WB | NB |
|----------|----|----|----|
|----------|----|----|----|

| | | | |
|----------------------|---|---|-----|
| HCM Control Delay, s | 0 | 2 | 8.8 |
| HCM LOS | | A | |

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
|-----------------------|-------|-----|-----|-----|-----|
|-----------------------|-------|-----|-----|-----|-----|

| | | | | | |
|-----------------------|-------|---|---|-------|---|
| Capacity (veh/h) | 969 | - | - | 1570 | - |
| HCM Lane V/C Ratio | 0.015 | - | - | 0.007 | - |
| HCM Control Delay (s) | 8.8 | - | - | 7.3 | 0 |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th %tile Q(veh) | 0 | - | - | 0 | - |

Dillon Drive at Site Access
Tecumseh, Ontario

Total Traffic 2030, AM Peak
Proposed Geometric Configuration

Intersection

Int Delay, s/veh 2.5

| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
|--------------------------|------|------|------|------|------|------|
| Lane Configurations | ↑ | | ↔ | ↔ | | |
| Traffic Vol, veh/h | 27 | 3 | 4 | 31 | 12 | 10 |
| Future Vol, veh/h | 27 | 3 | 4 | 31 | 12 | 10 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 0 | 0 | 2 | 0 | 0 |
| Mvmt Flow | 29 | 3 | 4 | 34 | 13 | 11 |

| Major/Minor | Major1 | Major2 | Minor1 | | | |
|----------------------|--------|--------|--------|---|-----|------|
| Conflicting Flow All | 0 | 0 | 32 | 0 | 73 | 31 |
| Stage 1 | - | - | - | - | 31 | - |
| Stage 2 | - | - | - | - | 42 | - |
| Critical Hdwy | - | - | 4.1 | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1593 | - | 936 | 1049 |
| Stage 1 | - | - | - | - | 997 | - |
| Stage 2 | - | - | - | - | 986 | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | - | - | 1593 | - | 933 | 1049 |
| Mov Cap-2 Maneuver | - | - | - | - | 933 | - |
| Stage 1 | - | - | - | - | 997 | - |
| Stage 2 | - | - | - | - | 983 | - |

| Approach | EB | WB | NB | | | |
|----------------------|----|-----|-----|--|--|--|
| HCM Control Delay, s | 0 | 0.8 | 8.8 | | | |
| HCM LOS | | | A | | | |

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT | |
|-----------------------|-------|-----|-----|-------|-----|--|
| Capacity (veh/h) | 982 | - | - | 1593 | - | |
| HCM Lane V/C Ratio | 0.024 | - | - | 0.003 | - | |
| HCM Control Delay (s) | 8.8 | - | - | 7.3 | 0 | |
| HCM Lane LOS | A | - | - | A | A | |
| HCM 95th %tile Q(veh) | 0.1 | - | - | 0 | - | |

Dillon Drive at Site Access
Tecumseh, Ontario

Total Traffic 2030, PM Peak
Proposed Geometric Configuration

Intersection

Int Delay, s/veh 1.9

| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
|----------|-----|-----|-----|-----|-----|-----|
|----------|-----|-----|-----|-----|-----|-----|

| | | | | | | |
|--------------------------|------|------|------|------|------|------|
| Lane Configurations | | | | | | |
| Traffic Vol, veh/h | 37 | 12 | 10 | 29 | 6 | 7 |
| Future Vol, veh/h | 37 | 12 | 10 | 29 | 6 | 7 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 0 | 0 | 2 | 0 | 0 |
| Mvmt Flow | 40 | 13 | 11 | 32 | 7 | 8 |

| Major/Minor | Major1 | Major2 | Minor1 | | | |
|-------------|--------|--------|--------|--|--|--|
|-------------|--------|--------|--------|--|--|--|

| | | | | | | |
|----------------------|---|---|------|---|-----|------|
| Conflicting Flow All | 0 | 0 | 53 | 0 | 101 | 47 |
| Stage 1 | - | - | - | - | 47 | - |
| Stage 2 | - | - | - | - | 54 | - |
| Critical Hdwy | - | - | 4.1 | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1566 | - | 902 | 1028 |
| Stage 1 | - | - | - | - | 981 | - |
| Stage 2 | - | - | - | - | 974 | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | - | - | 1566 | - | 896 | 1028 |
| Mov Cap-2 Maneuver | - | - | - | - | 896 | - |
| Stage 1 | - | - | - | - | 981 | - |
| Stage 2 | - | - | - | - | 967 | - |

| Approach | EB | WB | NB |
|----------|----|----|----|
|----------|----|----|----|

| | | | |
|----------------------|---|-----|-----|
| HCM Control Delay, s | 0 | 1.9 | 8.8 |
|----------------------|---|-----|-----|

| | |
|---------|---|
| HCM LOS | A |
|---------|---|

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
|-----------------------|-------|-----|-----|-------|-----|
| Capacity (veh/h) | 963 | - | - | 1566 | - |
| HCM Lane V/C Ratio | 0.015 | - | - | 0.007 | - |
| HCM Control Delay (s) | 8.8 | - | - | 7.3 | 0 |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th %tile Q(veh) | 0 | - | - | 0 | - |

Dillon Drive at Lacasse Boulevard
Tecumseh, Ontario

Existing Traffic, AM Peak
Existing Geometric Configuration

Intersection

Intersection Delay, s/veh 7.8
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↖ | | | ↖ | | | ↖ | | | ↖ | |
| Traffic Vol, veh/h | 3 | 5 | 14 | 3 | 13 | 1 | 12 | 45 | 2 | 2 | 27 | 0 |
| Future Vol, veh/h | 3 | 5 | 14 | 3 | 13 | 1 | 12 | 45 | 2 | 2 | 27 | 0 |
| Peak Hour Factor | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 |
| Heavy Vehicles, % | 60 | 0 | 0 | 25 | 5 | 0 | 8 | 1 | 29 | 0 | 0 | 0 |
| Mvmt Flow | 5 | 8 | 22 | 5 | 20 | 2 | 18 | 69 | 3 | 3 | 42 | 0 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 8.1 | | | 7.8 | | | 7.8 | | | 7.4 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 20% | 14% | 18% | 7% |
| Vol Thru, % | 76% | 23% | 76% | 93% |
| Vol Right, % | 3% | 64% | 6% | 0% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 59 | 22 | 17 | 29 |
| LT Vol | 12 | 3 | 3 | 2 |
| Through Vol | 45 | 5 | 13 | 27 |
| RT Vol | 2 | 14 | 1 | 0 |
| Lane Flow Rate | 91 | 34 | 26 | 45 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.106 | 0.045 | 0.033 | 0.051 |
| Departure Headway (Hd) | 4.194 | 4.822 | 4.588 | 4.087 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 848 | 735 | 771 | 866 |
| Service Time | 2.253 | 2.901 | 2.671 | 2.158 |
| HCM Lane V/C Ratio | 0.107 | 0.046 | 0.034 | 0.052 |
| HCM Control Delay | 7.8 | 8.1 | 7.8 | 7.4 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.4 | 0.1 | 0.1 | 0.2 |

Dillon Drive at Lacasse Boulevard
Tecumseh, Ontario

Existing Traffic, PM Peak
Existing Geometric Configuration

Intersection

| | |
|---------------------------|-----|
| Intersection Delay, s/veh | 7.6 |
| Intersection LOS | A |

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | | | ↔ | | | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 2 | 18 | 10 | 1 | 7 | 1 | 12 | 42 | 5 | 2 | 33 | 4 |
| Future Vol, veh/h | 2 | 18 | 10 | 1 | 7 | 1 | 12 | 42 | 5 | 2 | 33 | 4 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, % | 60 | 0 | 0 | 25 | 5 | 0 | 8 | 1 | 29 | 0 | 0 | 0 |
| Mvmt Flow | 2 | 20 | 11 | 1 | 8 | 1 | 13 | 46 | 5 | 2 | 36 | 4 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 8.2 | | | 7.6 | | | 7.5 | | | 7.2 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 20% | 7% | 11% | 5% |
| Vol Thru, % | 71% | 60% | 78% | 85% |
| Vol Right, % | 8% | 33% | 11% | 10% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 59 | 30 | 9 | 39 |
| LT Vol | 12 | 2 | 1 | 2 |
| Through Vol | 42 | 18 | 7 | 33 |
| RT Vol | 5 | 10 | 1 | 4 |
| Lane Flow Rate | 65 | 33 | 10 | 43 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.074 | 0.045 | 0.012 | 0.047 |
| Departure Headway (Hd) | 4.133 | 4.929 | 4.493 | 3.972 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 862 | 723 | 790 | 895 |
| Service Time | 2.178 | 2.981 | 2.556 | 2.023 |
| HCM Lane V/C Ratio | 0.075 | 0.046 | 0.013 | 0.048 |
| HCM Control Delay | 7.5 | 8.2 | 7.6 | 7.2 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.2 | 0.1 | 0 | 0.1 |

Dillon Drive at Lacasse Boulevard
Tecumseh, Ontario

Existing + Site Generated Traffic, AM Peak
Existing Geometric Configuration

Intersection

Intersection Delay, s/veh 7.6
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 4 | 8 | 20 | 3 | 15 | 1 | 14 | 45 | 2 | 2 | 27 | 0 |
| Future Vol, veh/h | 4 | 8 | 20 | 3 | 15 | 1 | 14 | 45 | 2 | 2 | 27 | 0 |
| Peak Hour Factor | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 |
| Heavy Vehicles, % | 6 | 0 | 0 | 25 | 5 | 0 | 8 | 1 | 29 | 0 | 0 | 0 |
| Mvmt Flow | 6 | 12 | 31 | 5 | 23 | 2 | 22 | 69 | 3 | 3 | 42 | 0 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 7.2 | | | 7.9 | | | 7.8 | | | 7.4 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 23% | 12% | 16% | 7% |
| Vol Thru, % | 74% | 25% | 79% | 93% |
| Vol Right, % | 3% | 62% | 5% | 0% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 61 | 32 | 19 | 29 |
| LT Vol | 14 | 4 | 3 | 2 |
| Through Vol | 45 | 8 | 15 | 27 |
| RT Vol | 2 | 20 | 1 | 0 |
| Lane Flow Rate | 94 | 49 | 29 | 45 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.11 | 0.054 | 0.037 | 0.051 |
| Departure Headway (Hd) | 4.233 | 3.913 | 4.604 | 4.122 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 842 | 901 | 768 | 861 |
| Service Time | 2.284 | 1.996 | 2.687 | 2.187 |
| HCM Lane V/C Ratio | 0.112 | 0.054 | 0.038 | 0.052 |
| HCM Control Delay | 7.8 | 7.2 | 7.9 | 7.4 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.4 | 0.2 | 0.1 | 0.2 |

Dillon Drive at Lacasse Boulevard
Tecumseh, Ontario

Existing + Site Generated Traffic, PM Peak
Existing Geometric Configuration

Intersection

Intersection Delay, s/veh 7.7
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 3 | 22 | 12 | 1 | 10 | 1 | 17 | 42 | 5 | 2 | 33 | 6 |
| Future Vol, veh/h | 3 | 22 | 12 | 1 | 10 | 1 | 17 | 42 | 5 | 2 | 33 | 6 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, % | 60 | 0 | 0 | 25 | 5 | 0 | 8 | 1 | 29 | 0 | 0 | 0 |
| Mvmt Flow | 3 | 24 | 13 | 1 | 11 | 1 | 19 | 46 | 5 | 2 | 36 | 7 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | WB | | | NB | | | SB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 8.3 | | | 7.7 | | | 7.6 | | | 7.2 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 27% | 8% | 8% | 5% |
| Vol Thru, % | 66% | 59% | 83% | 80% |
| Vol Right, % | 8% | 32% | 8% | 15% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 64 | 37 | 12 | 41 |
| LT Vol | 17 | 3 | 1 | 2 |
| Through Vol | 42 | 22 | 10 | 33 |
| RT Vol | 5 | 12 | 1 | 6 |
| Lane Flow Rate | 70 | 41 | 13 | 45 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.081 | 0.056 | 0.017 | 0.05 |
| Departure Headway (Hd) | 4.17 | 4.954 | 4.524 | 3.969 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 852 | 719 | 783 | 893 |
| Service Time | 2.228 | 3.013 | 2.597 | 2.034 |
| HCM Lane V/C Ratio | 0.082 | 0.057 | 0.017 | 0.05 |
| HCM Control Delay | 7.6 | 8.3 | 7.7 | 7.2 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.3 | 0.2 | 0.1 | 0.2 |

Intersection

Intersection Delay, s/veh 7.8
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 3 | 6 | 16 | 3 | 15 | 1 | 14 | 51 | 2 | 2 | 30 | 0 |
| Future Vol, veh/h | 3 | 6 | 16 | 3 | 15 | 1 | 14 | 51 | 2 | 2 | 30 | 0 |
| Peak Hour Factor | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 |
| Heavy Vehicles, % | 60 | 0 | 0 | 25 | 5 | 0 | 8 | 1 | 29 | 0 | 0 | 0 |
| Mvmt Flow | 5 | 9 | 25 | 5 | 23 | 2 | 22 | 78 | 3 | 3 | 46 | 0 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | WB | | | NB | | | SB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 8.2 | | | 7.9 | | | 7.9 | | | 7.4 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 21% | 12% | 16% | 6% |
| Vol Thru, % | 76% | 24% | 79% | 94% |
| Vol Right, % | 3% | 64% | 5% | 0% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 67 | 25 | 19 | 32 |
| LT Vol | 14 | 3 | 3 | 2 |
| Through Vol | 51 | 6 | 15 | 30 |
| RT Vol | 2 | 16 | 1 | 0 |
| Lane Flow Rate | 103 | 38 | 29 | 49 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.121 | 0.052 | 0.038 | 0.056 |
| Departure Headway (Hd) | 4.215 | 4.849 | 4.62 | 4.109 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 842 | 730 | 764 | 859 |
| Service Time | 2.284 | 2.939 | 2.716 | 2.193 |
| HCM Lane V/C Ratio | 0.122 | 0.052 | 0.038 | 0.057 |
| HCM Control Delay | 7.9 | 8.2 | 7.9 | 7.4 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.4 | 0.2 | 0.1 | 0.2 |

Intersection

Intersection Delay, s/veh 7.7
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 2 | 20 | 11 | 1 | 8 | 1 | 14 | 47 | 6 | 2 | 37 | 5 |
| Future Vol, veh/h | 2 | 20 | 11 | 1 | 8 | 1 | 14 | 47 | 6 | 2 | 37 | 5 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, % | 60 | 0 | 0 | 25 | 5 | 0 | 8 | 1 | 29 | 0 | 0 | 0 |
| Mvmt Flow | 2 | 22 | 12 | 1 | 9 | 1 | 15 | 52 | 7 | 2 | 41 | 5 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | WB | | | NB | | | SB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 8.3 | | | 7.7 | | | 7.6 | | | 7.3 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 21% | 6% | 10% | 5% |
| Vol Thru, % | 70% | 61% | 80% | 84% |
| Vol Right, % | 9% | 33% | 10% | 11% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 67 | 33 | 10 | 44 |
| LT Vol | 14 | 2 | 1 | 2 |
| Through Vol | 47 | 20 | 8 | 37 |
| RT Vol | 6 | 11 | 1 | 5 |
| Lane Flow Rate | 74 | 36 | 11 | 48 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.085 | 0.05 | 0.014 | 0.053 |
| Departure Headway (Hd) | 4.143 | 4.952 | 4.524 | 3.978 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 859 | 718 | 783 | 892 |
| Service Time | 2.195 | 3.014 | 2.598 | 2.039 |
| HCM Lane V/C Ratio | 0.086 | 0.05 | 0.014 | 0.054 |
| HCM Control Delay | 7.6 | 8.3 | 7.7 | 7.3 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.3 | 0.2 | 0 | 0.2 |

Dillon Drive at Lacasse Boulevard
Tecumseh, Ontario

Total Traffic 2025, AM Peak
Existing Geometric Configuration

Intersection

| | |
|---------------------------|---|
| Intersection Delay, s/veh | 8 |
| Intersection LOS | A |

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 4 | 9 | 22 | 3 | 17 | 1 | 16 | 51 | 2 | 2 | 30 | 0 |
| Future Vol, veh/h | 4 | 9 | 22 | 3 | 17 | 1 | 16 | 51 | 2 | 2 | 30 | 0 |
| Peak Hour Factor | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 |
| Heavy Vehicles, % | 60 | 0 | 0 | 25 | 5 | 0 | 8 | 1 | 29 | 0 | 0 | 0 |
| Mvmt Flow | 6 | 14 | 34 | 5 | 26 | 2 | 25 | 78 | 3 | 3 | 46 | 0 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 8.4 | | | 8 | | | 8 | | | 7.5 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 23% | 11% | 14% | 6% |
| Vol Thru, % | 74% | 26% | 81% | 94% |
| Vol Right, % | 3% | 63% | 5% | 0% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 69 | 35 | 21 | 32 |
| LT Vol | 16 | 4 | 3 | 2 |
| Through Vol | 51 | 9 | 17 | 30 |
| RT Vol | 2 | 22 | 1 | 0 |
| Lane Flow Rate | 106 | 54 | 32 | 49 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.125 | 0.074 | 0.043 | 0.058 |
| Departure Headway (Hd) | 4.253 | 4.961 | 4.745 | 4.247 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 830 | 726 | 759 | 848 |
| Service Time | 2.344 | 2.961 | 2.748 | 2.25 |
| HCM Lane V/C Ratio | 0.128 | 0.074 | 0.042 | 0.058 |
| HCM Control Delay | 8 | 8.4 | 8 | 7.5 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.4 | 0.2 | 0.1 | 0.2 |

Dillon Drive at Lacasse Boulevard
Tecumseh, Ontario

Total Traffic 2025, PM Peak
Existing Geometric Configuration

Intersection

Intersection Delay, s/veh 7.8
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 3 | 24 | 13 | 1 | 11 | 1 | 19 | 47 | 6 | 2 | 37 | 7 |
| Future Vol, veh/h | 3 | 24 | 13 | 1 | 11 | 1 | 19 | 47 | 6 | 2 | 37 | 7 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, % | 60 | 0 | 0 | 25 | 5 | 0 | 8 | 1 | 29 | 0 | 0 | 0 |
| Mvmt Flow | 3 | 26 | 14 | 1 | 12 | 1 | 21 | 52 | 7 | 2 | 41 | 8 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | WB | | | NB | | | SB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 8.4 | | | 7.7 | | | 7.7 | | | 7.3 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 26% | 7% | 8% | 4% |
| Vol Thru, % | 65% | 60% | 85% | 80% |
| Vol Right, % | 8% | 33% | 8% | 15% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 72 | 40 | 13 | 46 |
| LT Vol | 19 | 3 | 1 | 2 |
| Through Vol | 47 | 24 | 11 | 37 |
| RT Vol | 6 | 13 | 1 | 7 |
| Lane Flow Rate | 79 | 44 | 14 | 51 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.092 | 0.061 | 0.018 | 0.056 |
| Departure Headway (Hd) | 4.179 | 4.976 | 4.553 | 3.979 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 850 | 714 | 777 | 890 |
| Service Time | 2.242 | 3.045 | 2.637 | 2.051 |
| HCM Lane V/C Ratio | 0.093 | 0.062 | 0.018 | 0.057 |
| HCM Control Delay | 7.7 | 8.4 | 7.7 | 7.3 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.3 | 0.2 | 0.1 | 0.2 |

Intersection

Intersection Delay, s/veh 7.9
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 4 | 6 | 17 | 4 | 16 | 1 | 15 | 56 | 2 | 2 | 34 | 0 |
| Future Vol, veh/h | 4 | 6 | 17 | 4 | 16 | 1 | 15 | 56 | 2 | 2 | 34 | 0 |
| Peak Hour Factor | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 |
| Heavy Vehicles, % | 60 | 0 | 0 | 25 | 5 | 0 | 8 | 1 | 29 | 0 | 0 | 0 |
| Mvmt Flow | 6 | 9 | 26 | 6 | 25 | 2 | 23 | 86 | 3 | 3 | 52 | 0 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | WB | | | NB | | | SB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 8.3 | | | 8 | | | 8 | | | 7.5 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 21% | 15% | 19% | 6% |
| Vol Thru, % | 77% | 22% | 76% | 94% |
| Vol Right, % | 3% | 63% | 5% | 0% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 73 | 27 | 21 | 36 |
| LT Vol | 15 | 4 | 4 | 2 |
| Through Vol | 56 | 6 | 16 | 34 |
| RT Vol | 2 | 17 | 1 | 0 |
| Lane Flow Rate | 112 | 42 | 32 | 55 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.132 | 0.058 | 0.043 | 0.063 |
| Departure Headway (Hd) | 4.232 | 4.99 | 4.764 | 4.126 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 837 | 722 | 756 | 853 |
| Service Time | 2.313 | 2.991 | 2.766 | 2.223 |
| HCM Lane V/C Ratio | 0.134 | 0.058 | 0.042 | 0.064 |
| HCM Control Delay | 8 | 8.3 | 8 | 7.5 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.5 | 0.2 | 0.1 | 0.2 |

Intersection

Intersection Delay, s/veh 7.7
Intersection LOS A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↖ | | | ↖ | | | ↖ | | | ↖ | |
| Traffic Vol, veh/h | 2 | 22 | 12 | 1 | 9 | 1 | 15 | 52 | 6 | 2 | 41 | 5 |
| Future Vol, veh/h | 2 | 22 | 12 | 1 | 9 | 1 | 15 | 52 | 6 | 2 | 41 | 5 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, % | 60 | 0 | 0 | 25 | 5 | 0 | 8 | 1 | 29 | 0 | 0 | 0 |
| Mvmt Flow | 2 | 24 | 13 | 1 | 10 | 1 | 16 | 57 | 7 | 2 | 45 | 5 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 8.3 | | | 7.7 | | | 7.6 | | | 7.3 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 21% | 6% | 9% | 4% |
| Vol Thru, % | 71% | 61% | 82% | 85% |
| Vol Right, % | 8% | 33% | 9% | 10% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 73 | 36 | 11 | 48 |
| LT Vol | 15 | 2 | 1 | 2 |
| Through Vol | 52 | 22 | 9 | 41 |
| RT Vol | 6 | 12 | 1 | 5 |
| Lane Flow Rate | 80 | 40 | 12 | 53 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.093 | 0.055 | 0.015 | 0.059 |
| Departure Headway (Hd) | 4.158 | 4.972 | 4.55 | 3.996 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 855 | 715 | 777 | 887 |
| Service Time | 2.216 | 3.041 | 2.634 | 2.063 |
| HCM Lane V/C Ratio | 0.094 | 0.056 | 0.015 | 0.06 |
| HCM Control Delay | 7.6 | 8.3 | 7.7 | 7.3 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.3 | 0.2 | 0 | 0.2 |

Dillon Drive at Lacasse Boulevard
Tecumseh, Ontario

Total Traffic 2030, AM Peak
Existing Geometric Configuration

Intersection

| | |
|---------------------------|---|
| Intersection Delay, s/veh | 8 |
| Intersection LOS | A |

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 5 | 9 | 23 | 4 | 18 | 1 | 17 | 56 | 2 | 2 | 34 | 0 |
| Future Vol, veh/h | 5 | 9 | 23 | 4 | 18 | 1 | 17 | 56 | 2 | 2 | 34 | 0 |
| Peak Hour Factor | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 |
| Heavy Vehicles, % | 60 | 0 | 0 | 25 | 5 | 0 | 8 | 1 | 29 | 0 | 0 | 0 |
| Mvmt Flow | 8 | 14 | 35 | 6 | 28 | 2 | 26 | 86 | 3 | 3 | 52 | 0 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 8.4 | | | 8 | | | 8.1 | | | 7.6 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 23% | 14% | 17% | 6% |
| Vol Thru, % | 75% | 24% | 78% | 94% |
| Vol Right, % | 3% | 62% | 4% | 0% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 75 | 37 | 23 | 36 |
| LT Vol | 17 | 5 | 4 | 2 |
| Through Vol | 56 | 9 | 18 | 34 |
| RT Vol | 2 | 23 | 1 | 0 |
| Lane Flow Rate | 115 | 57 | 35 | 55 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.14 | 0.079 | 0.047 | 0.066 |
| Departure Headway (Hd) | 4.369 | 5.007 | 4.795 | 4.272 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 826 | 718 | 749 | 842 |
| Service Time | 2.369 | 3.018 | 2.806 | 2.28 |
| HCM Lane V/C Ratio | 0.139 | 0.079 | 0.047 | 0.065 |
| HCM Control Delay | 8.1 | 8.4 | 8 | 7.6 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.5 | 0.3 | 0.1 | 0.2 |

Dillon Drive at Lacasse Boulevard
Tecumseh, Ontario

Total Traffic 2030, PM Peak
Existing Geometric Configuration

Intersection

| | |
|---------------------------|-----|
| Intersection Delay, s/veh | 7.8 |
| Intersection LOS | A |

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Vol, veh/h | 3 | 26 | 14 | 1 | 12 | 1 | 20 | 52 | 6 | 2 | 41 | 7 |
| Future Vol, veh/h | 3 | 26 | 14 | 1 | 12 | 1 | 20 | 52 | 6 | 2 | 41 | 7 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, % | 60 | 0 | 0 | 25 | 5 | 0 | 8 | 1 | 29 | 0 | 0 | 0 |
| Mvmt Flow | 3 | 29 | 15 | 1 | 13 | 1 | 22 | 57 | 7 | 2 | 45 | 8 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | | | | | | | | | | | | |
| Opposing Approach | WB | | | WB | | | NB | | | SB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay | 8.4 | | | 7.8 | | | 7.7 | | | 7.3 | | |
| HCM LOS | A | | | A | | | A | | | A | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|------------------------|-------|-------|-------|-------|
| Vol Left, % | 26% | 7% | 7% | 4% |
| Vol Thru, % | 67% | 60% | 86% | 82% |
| Vol Right, % | 8% | 33% | 7% | 14% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 78 | 43 | 14 | 50 |
| LT Vol | 20 | 3 | 1 | 2 |
| Through Vol | 52 | 26 | 12 | 41 |
| RT Vol | 6 | 14 | 1 | 7 |
| Lane Flow Rate | 86 | 47 | 15 | 55 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.1 | 0.066 | 0.02 | 0.061 |
| Departure Headway (Hd) | 4.193 | 4.995 | 4.577 | 3.998 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 846 | 711 | 771 | 884 |
| Service Time | 2.262 | 3.071 | 2.669 | 2.079 |
| HCM Lane V/C Ratio | 0.102 | 0.066 | 0.019 | 0.062 |
| HCM Control Delay | 7.7 | 8.4 | 7.8 | 7.3 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.3 | 0.2 | 0.1 | 0.2 |

Appendix E

TRAFFIC SIGNAL WARRANTS – SUMMARY OF JUSTIFICATIONS

Dillon Drive at Lesperance Road

Traffic Signal Warrants – Summary of Justifications (OTM Book 12)

Projected Total Traffic (Horizon Year 2025)

Dillon Drive at Lesperance Road

| JUSTIFICATION | DESCRIPTION | MINIMUM REQUIREMENTS FOR TWO-LANE ROADWAYS | | COMPLIANCE | |
|----------------------------------|--|--|--|-------------------|------------|
| | | FREE FLOW | RESTRICTED FLOW | | |
| | | OPERATING SPEED GREATER THAN OR EQUAL TO 70 km/h | OPERATING SPEED LESS THAN 70 km/h | SECTIONAL % | ENTIRE %** |
| 1. MINIMUM VEHICULAR VOLUME | A*. Vehicle Volume, All Approaches for Each of the Heaviest 8 Hours of an Average Day, and | 480 | 720 | 23 ⁽¹⁾ | 18 |
| | B***. Vehicle Volume, Along Minor Streets for Each of the Same 8 Hours | 120 | 170 | 18 ⁽²⁾ | |
| 2. DELAY TO CROSS TRAFFIC | A*. Vehicle Volume, Major Street for Each of the Heaviest 8 Hours of an Average Day, and | 480 | 720 | 19 ⁽³⁾ | 19 |
| | B*. Combined Vehicle and Pedestrian Volume Crossing the Major Street for Each of the Same 8 Hours. | 50 | 75 | 22 ⁽⁴⁾ | |
| 3. VOLUME/DELAY COMBINATIONS | The Above Justifications (1 and 2) Both Satisfied to the Extent of 80% or more | YES <input type="checkbox"/> | NO <input checked="" type="checkbox"/> | | 18 |
| 4. MIN. FOUR HOUR VEHICLE VOLUME | At Plotted Point Representing Hourly Volume for Minor Approach vs. Major Approach for Four Highest Hours of an Average Day Fall above the Applicable Curve | YES <input type="checkbox"/> | NO <input type="checkbox"/> | | N/A |
| 5. COLLISION EXPERIENCE | A. Total Reported Accidents of Types Susceptible to Correction by a Traffic Signal, per 12 Month Period Averaged over a 36 Month Period, and | 5 | | N/A | N/A |
| | B. Adequate Trial of Less Restrictive Remedies. Where Satisfactory Observance and Enforcement Have Failed to Reduce the Number of Collisions | YES <input type="checkbox"/> | NO <input type="checkbox"/> | | |
| 6. PEDESTRIAN VOLUME AND DELAY | A. Plotted Point Representing 8 Hour Pedestrian Volume vs. 8 Hour Vehicular Volume Fall in Justified Zone, and | YES <input type="checkbox"/> | NO <input type="checkbox"/> | | N/A |
| | B. Plotted Point Representing 8 Hour Volume of Pedestrian Experiencing Delays of 10 s or more vs. 8 Hour Pedestrian Volume Fall in Justified Zone | YES <input type="checkbox"/> | NO <input type="checkbox"/> | | |

Notes

* Vehicle Volume Warrants 1A and 2A for Roadways Having Two or More Moving Lanes in One Direction Should be 25% Higher than Values Given Above.

** The Lowest Sectional Percentage Governs the Entire Warrant.

*** For "T" Intersections, the Values for Warrant (1B) should be increased by 50%.

Justification 7 - Future Traffic Volumes

$$(1) = (282 + 384) / 4 / 720 = 23\%$$

$$(2) = (65 + 60) / 4 / 170 = 18\%$$

$$(3) = (217 + 324) / 4 / 720 = 19\%$$

$$(4) = (35 + 32) / 4 / 75 = 22\%$$

Traffic Signal Warrants – Summary of Justifications (OTM Book 12)

Projected Total Traffic (Horizon Year 2030)

Dillon Drive at Lesperance Road

| JUSTIFICATION | DESCRIPTION | MINIMUM REQUIREMENTS FOR TWO-LANE ROADWAYS | | COMPLIANCE | |
|----------------------------------|--|--|--|-------------------|------------|
| | | FREE FLOW | RESTRICTED FLOW | | |
| | | OPERATING SPEED GREATER THAN OR EQUAL TO 70 km/h | OPERATING SPEED LESS THAN 70 km/h | SECTIONAL % | ENTIRE %** |
| 1. MINIMUM VEHICULAR VOLUME | A*. Vehicle Volume, All Approaches for Each of the Heaviest 8 Hours of an Average Day, and | 480 | 720 | 24 ⁽¹⁾ | 21 |
| | B***. Vehicle Volume, Along Minor Streets for Each of the Same 8 Hours | 120 | 170 | 21 ⁽²⁾ | |
| 2. DELAY TO CROSS TRAFFIC | A*. Vehicle Volume, Major Street for Each of the Heaviest 8 Hours of an Average Day, and | 480 | 720 | 19 ⁽³⁾ | 19 |
| | B*. Combined Vehicle and Pedestrian Volume Crossing the Major Street for Each of the Same 8 Hours. | 50 | 75 | 25 ⁽⁴⁾ | |
| 3. VOLUME/DELAY COMBINATIONS | The Above Justifications (1 and 2) Both Satisfied to the Extent of 80% or more | YES <input type="checkbox"/> | NO <input checked="" type="checkbox"/> | | 19 |
| 4. MIN. FOUR HOUR VEHICLE VOLUME | At Plotted Point Representing Hourly Volume for Minor Approach vs. Major Approach for Four Highest Hours of an Average Day Fall above the Applicable Curve | YES <input type="checkbox"/> | NO <input type="checkbox"/> | | N/A |
| 5. COLLISION EXPERIENCE | A. Total Reported Accidents of Types Susceptible to Correction by a Traffic Signal, per 12 Month Period Averaged over a 36 Month Period, and | 5 | | N/A | N/A |
| | B. Adequate Trial of Less Restrictive Remedies. Where Satisfactory Observance and Enforcement Have Failed to Reduce the Number of Collisions | YES <input type="checkbox"/> | NO <input type="checkbox"/> | | |
| 6. PEDESTRIAN VOLUME AND DELAY | A. Plotted Point Representing 8 Hour Pedestrian Volume vs. 8 Hour Vehicular Volume Fall in Justified Zone, and | YES <input type="checkbox"/> | NO <input type="checkbox"/> | | N/A |
| | B. Plotted Point Representing 8 Hour Volume of Pedestrian Experiencing Delays of 10 s or more vs. 8 Hour Pedestrian Volume Fall in Justified Zone | YES <input type="checkbox"/> | NO <input type="checkbox"/> | | |

Notes

* Vehicle Volume Warrants 1A and 2A for Roadways Having Two or More Moving Lanes in One Direction Should be 25% Higher than Values Given Above.

** The Lowest Sectional Percentage Governs the Entire Warrant.

*** For "T" Intersections, the Values for Warrant (1B) should be increased by 50%.

Justification 7 - Future Traffic Volumes

$$(1) = (297 + 401) / 4 / 720 = 24\%$$

$$(2) = (78 + 68) / 4 / 170 = 21\%$$

$$(3) = (219 + 333) / 4 / 720 = 19\%$$

$$(4) = (43 + 32) / 4 / 75 = 25\%$$

Appendix F

SIGHT LINE ANALYSIS

Dillon Drive at Site Access

19-864: Victoria Development TIS - Sight Line Analysis

Design Intersection Sight Distance (TAC Geometric Design Guide for Canadian Roads)

Design Speed: 50 km/h (Posted Speed Limit = 40 km/h)

Table 9.9.3: Time Gap for Case B1, Left Turn from Stop

| Design Vehicle | Time Gap (t_g)(s) at Design Speed of Major Road |
|--------------------------------------|---|
| Passenger car | 7.5 |
| Single-unit truck | 9.5 |
| Combination truck (WB 19 and WB 20) | 11.5 |
| Longer truck | To be established by road authority |

$$\text{Intersection Stopping Distance (ISD)} = 0.278 V_{\text{major}} t_g$$

Where:

ISD = intersection sight distance (m)
(length of the leg of sight triangle along the major road)

V_{major} = design speed of the major road (km/h)

t_g = time gap for minor road vehicle to enter the major road (s)

$$\text{ISD}_{\text{passenger car}} (\text{left turn from stop}) = 0.278 \times 50 \times 7.5 = \mathbf{104 \text{ m}}$$

Table 9.9.5: Time Gap for Case B2—Right Turn from Stop and Case B3—Crossing Maneuver

| Design Vehicle | Time Gap (t_g)(s) at Design Speed of Major Road |
|--------------------------------------|---|
| Passenger car | 6.5 |
| Single-unit truck | 8.5 |
| Combination truck (WB 19 and WB 20) | 10.5 |

$$\text{ISD}_{\text{passenger car}} (\text{right turn from stop}) = 0.278 \times 50 \times 6.5 = \mathbf{90 \text{ m}}$$

Victoria Development, 12433 Dillon Drive, Tecumseh, Ontario

Traffic Impact Study (March 2021): Response Matrix

In response to the request made by Mr. John Henderson, P.Eng., in his Technical Submission Review letter, the following is a summary of how each concern was addressed in the revised March 2021 TIS:

| | |
|------------|---|
| Q.1 | Site Generated Traffic: At the intersection of Dillon Drive and Lacasse Boulevard, the AM peak hour eastbound left-turn volume is shown to be 10 vehicles per hour, where it appears it should be 1 vehicle per hour. This appears to propagate through the subsequent traffic volume figures and into the Capacity and Level of Service Analysis reports in Appendix D. This will lead to overestimation of delay at the intersection of Dillon Drive and Lacasse Boulevard. Even with this issue, the delays were acceptable, however, please review and update the report accordingly. |
| A.1 | This was a transcription error; it has since been corrected in all sections of the revised report. |
| Q.2 | Peak Hour Factors: According to the Synchro reports in Appendix D, the Capacity and Level of Service Analysis used Peak Hour Factors (PHFs) of 0.92 for all intersections in all scenarios. The counts in Appendix A showed the following PHFs (at the overall intersection level): Dillon Drive at Lesperance Road – AM: 0.92, PM: 0.83; Dillon Drive at St. Pierre Street – AM: 0.73, PM: 0.74; Dillon Drive at Lacasse Boulevard – AM: 0.65, PM: 0.91. Lower PHFs will give higher peak hour delays, so using 0.92 leads to an underestimation of delays. However, given the low volumes at the study intersections, this is unlikely to lead to any erroneous conclusions. Please confirm. |
| A.2 | All PHFs were adjusted to match the values stated above. All Synchro reports were then revised to account for this change (see Appendix D). |
| Q.3 | Heavy Vehicle Percentages: According to the Synchro reports in Appendix D, the Capacity and Level of Service Analysis used heavy vehicle percentages that are inconsistent with the values from the traffic counts in Appendix A. Appendix A provides heavy vehicle percentages for the entire count period, and not just the peak hour, so the values used in the analysis may be correct if they represent the peak hours. Given the low volumes at the study intersections, the percentage of heavy vehicle used in the assessment likely had a negligible effect of reported delays and the study conclusions remain valid. Please confirm. |
| A.3 | Heavy vehicle percentages were adjusted to match the observed percentages. The chart of percentages used in the modelling is identified on page 4 of the revised report. |
| Q.4 | Conflicting Pedestrian Volumes: According to the Synchro reports in Appendix D, the Capacity and Level of Service Analysis used overly conservative volumes of conflicting pedestrians. From the counts in Appendix A, conflicting pedestrian volumes at the intersection of Dillon Drive and Lesperance Road (the only intersection where conflicting pedestrians apply to the analysis) were: Crossing North Leg: AM: 1, PM: 3; Crossing East Leg: AM: 0, PM: 1; Crossing South Leg: AM: 2, PM: 3; Crossing West Leg: AM: 0, PM: 0. Overly conservative conflicting pedestrian volumes would cause delays to be overestimated. Even with this over-estimation, all delays |



| | |
|------|--|
| | were acceptable, so the overly conservative pedestrian volumes did not lead to any erroneous conclusions. |
| A.4 | Conflicting Pedestrian Volumes were addressed on page 4 of the revised report: "Peak hour pedestrian volumes were very low, so the impact of pedestrians on intersection operations is expected to be nominal; regardless, conservative pedestrian volumes were inputted into the Synchro 10 analysis software." |
| Q.5 | Intersection Configurations in the Report Text: Readers interested in the intersection configurations used in the analysis need to search through many pages of analysis reports in Appendix D. For clarity and readability, it would be beneficial to include an outline of the intersection geometry and traffic control used in the analyses in the report text. |
| A.5 | Geometry and traffic control for each intersection is elaborated in greater detail under the specific intersection sub-heading; see pages 4 to 8. |
| Q.6 | State Assumptions and Procedures for PHFs, Heavy Vehicle Percentages, and Conflicting Pedestrian Volumes: Like the previous point, readers looking for information on these inputs need to search through analysis reports in Appendix D. For clarity and readability, it would be beneficial to include a description of any assumptions around these inputs in the report text. |
| A.6 | Tables for the heavy vehicle percentages and the PHFs are included in the revised report on page 4; pedestrian volumes are also discussed on page 4. |
| Q.7 | Note Anticipated Changes to Transportation and Land Use: The report text should include a discussion on future external changes to land use (developments) and the transportation system that may impact conditions at the study intersections. The area around each study intersection seems fully built out, so it is unlikely that there would be significant transportation or land use changes in the near future, but if that is the case, it should still be stated in the report. |
| A.7 | This concern has been addressed in the first paragraph of the Introduction and Background section; see page 1 of the revised report. |
| Q.8 | Note the Capacity and Level of Service Analysis Methodology: Include a note about the analysis methodology used in the Capacity and Level of Service Analysis (HCM 2000, HCM 2010, HCM 6 th Edition, Synchro proprietary method, etc.) in the report text. |
| A.8 | These details are addressed in the first paragraph of the Methodology section on page 2. |
| Q.9 | Clearly List the Intersections Included in the Study: The intersections in the study can be inferred from the text in the Existing Conditions section and in the Capacity and Level of Service Analysis section, but there is not a clear list of the study intersections. It would be easier to understand the extent of the TIS if the study intersections were clearly listed near the start of the report, perhaps in the Introduction and Background section. |
| A.9 | The study intersections are bulleted on page 1 in the Introduction and Background section of the revised report. |
| Q.10 | Clearly List the Analysis Scenarios Near the Start of the Report: Analysis scenarios are clearly listed in the Capacity and Level of Service Analysis section and referred to in the Trip Generation and Distribution section. It would be easier to understand the extent of the TIS if the analysis |



| | |
|------|--|
| | scenarios were listed near the start of the report, perhaps in the Introduction and Background section. |
| A.10 | The analysis scenarios are bulleted on page 1 in the Introduction and Background section of the revised report. |
| Q.11 | Note the Time Periods for Analysis: Time periods for analysis can be inferred from the discussion in the report, but they are not stated clearly. It would be easier to understand the extent of the TIS if the time periods for analysis were stated clearly near the start of the report, perhaps in the Introduction and Background section. |
| A.11 | It is stated on page 1 in the Introduction and Background section that the AM and PM peak hours would be analyzed for the given scenarios. |
| Q.12 | Note How the Background Growth Rate Was Applied: The background traffic growth rate percentage is stated, but it is not stated that the growth rate was applied as a compound annual growth rate. Compound annual growth rates are used by default in many jurisdictions, but some jurisdictions use linear growth rates. Stating the growth rate type would resolve any lack of clarity on that point. |
| A.12 | The original May 2019 report, page 2, clearly stated that, "Background traffic was increased by 2% per year for the 2025 and 2030 horizon forecasts, which provides for very conservative increases to background traffic when compounded annually." Growth is always calculated based on a compound growth rate. |

All of which is respectfully submitted,

RC Spencer Associates Inc.



John D. Tofflemire, M.A.Sc., P.Eng.
Manager, Leamington Office



Aaron D. Blata, M.Eng., P.Eng., PTOE
Associate / Traffic Operations Project Engineer



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